

**SLOPE STABILITY AND FACTOR OF SAFETY ANALYSIS ON DIFFERENT
REGION OF SOIL BY USING GEO STUDIO SLOPE/W SOFTWARE**

MAJOR II REPORT

SUBMITTED IN PARTIAL FULFILLMENT OF THE

REQUIREMENTS

FOR THE AWARD OF DEGREE OF

MASTERS OF TECHNOLOGY

IN

GEOTECHNICAL ENGINEERING

SUBMITTED BY

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CANDIDATE'S DECLARATION

I, **VISHAL RATHORE,2K18/GTE/17** student of M tech (GEOTECHNICAL ENGINEERING), hereby declare that the dissertation entitled "**SLOPE STABILITY AND FACTOR OF SAFETY ANALYSIS ON DIFFERENT REGION OF SOIL BY USING GEO STUDIO SLOPE/W SOFTWARE**" which is submitted by me to department of Civil Engineering ,Delhi Technological University, Delhi In Partial fulfillment of the requirement of the award of the degree of Master Of Technology , is original and not copied from any source without proper citation .This work has not previously formed the basis for the award of any Degree, Diploma Associate ship, Fellowship or other similar title or recognition.



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CERTIFICATE

I hereby certify that the dissertation entitled "**SLOPE STABILITY AND FACTOR OF SAFETY ANALYSIS ON DIFFERENT REGION OF SOIL BY USING GEO STUDIO SLOPE/W SOFTWARE**" which is submitted by (**VISHALRATHORE ,2K18/GTE/17**) to department of Civil Engineering, Delhi Technological University, Delhi In Partial fulfillment of the requirement of the award of the degree of Master Of Technology, is record of the project work carried by the Student under my supervision . To the best of my knowledge this work has no been submitted in part or full for any Degree to this University or elsewhere.



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ACKNOWLEDGEMENT

I thank my parents and God almighty for bestowing their blessings and grace in completion of minor project 2.

I express my sincere thanks to the respective V.C. of DTU and respective HOD of Civil Engineering Department and to the University Management. As I write this acknowledgement , I must clarify that this is not just a formal acknowledgement but also a sincere note of thanks and regards from my side . I feel a deep sense of gratitude and affection for those who associated with the project and without whose co-operation and guidance this project could not have been conducted properly.

Words fail me to express my regards towards my project guide, **Prof. A.K. Sahu**, Department of Civil Engineering ,Delhi Technological University , Delhi for giving me an opportunity to work under his guidance , which really instilled in me the requisite confidence.

I also express my deep gratitude to all the Faculty members of Department of Civil Engineering . Last but not the least , I would like to thank my family and friends who stimulated me to bring this work to a successful close.



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LIST OF ABBREVIATION

MDD : Maximum Dry Density

C : Cohesion

Φ : Internal friction angle

C_c : Coefficient of compression

C_u : Coefficient of Uniformity

D_{10} : Size of grain at which 10% finer by weight (Effective Particle size)

D_{30} : Size of grain at which 30% finer by weight

D_{60} : Size of grain at which 60% finer by weight

F.O.S : Factor of safety

ABSTRACT

The one of the main trouble in the industry of construction is on account of topography nature and the weather conditions is Slope stability . Excavations, hill roads, railway lines, embankments, earth dams, open-cut mines, reservoirs and coastal slope stability these type of applications can come under the consideration of slope engineering. One of the frequent disaster is Slope failure which can generate great loss in property and life. The project namely “Slope Stability and Factor of safety analysis” gives analysis of Four region soil (Himalaya, Jammu and Punjab and on DTU, Delhi) using Geo Studio Slope/w software. The analysis for stability of earth structures can be get from a general software tool Slope/W which is design and develop accordingly. The main essential thing that must be taking care of in the slope stability is in order to undergo the mountainous region project. The study is focus on slope stability analysis for Himachal Jammu and Punjab State and Delhi soil slope using Slope/w. Slope failure has become one of the most frequent geological disaster along the road network in the hilly terrain of Himalayan Jammu , Punjab and Delhi regions that lead to huge loss of life, property and above all the environment. The process of slope stability is very important to defence of the slopes from failure and minimize the likelihood of failure of slopes. By helping Geo Studio(Slope/w) software, the factor of safety and slope stability slope stability will be analyzed.

1. INTRODUCTION

India 2020 population is estimated about 1.38 billion people at mid year according to UN data . The population of india is approx 17.7% of the total population of the world . India ranks second in the list of countries which is by the number of population. The density of population in India is 464per square kilometer . As the population growth, we will need more land which mean that more civil engineering project work will be carried out in mountainous or hilly regions. In order to undergo the hilly region project, Slope stability is the most important thing that must be taking care of.

Due to the nature of the topography and weather conditions, Slope stability issue becomes one of the main problems in construction industry. Excavations, hill roads, railway lines, embankments, earth dams, open-cut mines, reservoirs and coastal slope stability these type of applications can come under the consideration of slope engineering. The most frequent natural disaster that can lead to great loss in property and life is acknowledged as Slope Failure. The stability of slope depends more on the driving force and resisting force because the driving force is greater than the resisting force which actually causes slope failures.

The main purpose of this study is to analyze slope stability by using Geo Studio Slope/w software. The stability analysis of earth structures can be obtained from a general software tool Slope/W which is design and develop accordingly. The sliding stability of a gravity retaining wall can be access by Slope/W, and for find out active earth forces on the wall. The stability of a wedge of soil that has been reinforced with a structural component such as a soil nail, geo-fabric, a pre-stressed anchor or some other material can ne analyzed by slope/W. By inserting the data to the software the software will analyze data in order to get slope stability. The data of the slope, which used in analyzing the slope stability using Slope/w, For Himachal , Jammu and Punjab soil was obtained from the research paper (vivek et al. 2015)“Slope stability Analysis” which was published in IJCEM (International journal core engineering and management) Volume 2, Issue 3, June 2015. Data used for DTU soil, analyzed in DTU laboratory itself.

1.1. Objective of the study

The analysis on slope stability using Geo Studio Slope/w software has two specific objectives which are:

1. To produce slope stability analysis for Himachal, Jammu, Punjab and DTU, Delhi soil slope using Slope/w.
2. To determine the factor of safety of slope stability of Himachal, Jammu, Punjab and DTU, Delhi soil slope using Slope/w.

2. Literature Reviews

This literature review of the project consists of titles such as research work , parameter and result of different research works on change in various attributes of Slope Stability.

Ravi Chandra , Bahnali Ghosh , S. B. Prasad , August 2016, “Stability Analysis of Slopes and Seismic Analysis of Earthen Dams using GeoStudio” Evaluation of Slope Stability and Seismic Analysis of Earthen Dams for different conditions by using the software slope/W .In this report under recorded earthquake the behavior of Earthen Dams analysed by using Finite Element Based Geostudio Qwake/W .Geotechnical software simulation were concerned on the effect of water pressure and the seismic response of earthdams to a recorded earthquake. At the three conditions first,middleand end times of the earthquake ,the earthquake behavior of the dams during the earthquake loading obtained as the results of the Numerical Analysis.

Shanmugapriya Dewdree and Siti Norafida Jusoh , 2019, “Slope stability analysis under different soil nailing parameters using the SLOPE/W software” For determining the most appropriate value for stabilization of soil slope using software Slope/W ,Soil nailing system was studied in terms of inclination of soil nailing . The best factor of safety found at (60° , 50° and 40° respectively) with the horizontal . Soil nailing FOS varies very minute where the soil nails varies (5° - 20°) respectively.

D. Durga Naga Laxmi Devi and R. Anbalagan , 2017 , “Study on Slope Stability of Earthen Dams by using Geostudio Software” By using the Slope/W and Seep/W software tools of Geostudio for sudden drawdown conditions and Steady State Seepage , FOS analysed . Seepage analysis and study stage seepage are essential for homogenous earthdams on downstreamside , Providing of drain on the Downstream side increases the FOS.

Imran Arshad and Muhammad Muneer , 2017, ‘Numerical Analysis of Seepage and Slope Stability in an Earthen Dam by using Geo slope software’ Bishap, Janbu , Ordinary Method of Slice and Morgenstern Price method these four analysis used for finding out the slope stability. It revealed that both side (Upstreamside and Downstreamside) of the dam section has a direct effect of FOS.

Michael Peter Serra , oct 2013 , University of Southern Queensland , Fculty of Engineering Science (Geotechnical Stability Analysis using student versions of FLAC, PLAXIS and SLOPE/W) By using FLAC and Plaxis , mesh can be generated in Finite Difference(FD) and Finite Element(FE) , gives best results . In FLAC student version it allows only coarse mess so it gives less accurate FOS compare to PLAXIS and SLOPE/W. Each software has its own limitations and benefits , user uses the software according to their model requirements.

Sarper Demirdogen , oct.2018, “Numerical Analysis of Leakage through Defective Geomembrane Liners in Embankment Dams” In this report a 2D numerical analysis conducted by using Seep/W for evaluating the leakage through geomembrane liner within an earthen dam. This study gives the appropriate idea which gives better understanding of how the parameters of geomembrane will affect the FOS of the downstream slope.

Marwah Qaddoori and Marwah Kamil Hussein , November 2019 , “Slope Stability Prediction of Homogeneous Earth dam caused by fluid particles seeps by using artificial neural networks” C, Φ , Υ are used as input parameter of dam and find out the FOS by using entry and exit method , Here time series method used for analysis . Slip surfaces eliminated in Upstream and Downstream side of the dam to find out the FOS.

Ahnad Amirul Bin Mohd Zaki, july 2015, “Comparison of factor of safety using different method of analysis for slope stability” Margenstern Price , Jonbu, Ordinary and Bishop methods used in Slope/W and FOS analysed for each case . FOS of each type with the help of Slop/W calculated and compared with conventional analysis.

Yue Yan and Yahui Zhang , 2014 , “Impact of Balasting Vibration on Soil Slope Stability” Studies the stress-strain relationship of soil mass for finding out FOS in natural conditions as well as with vibration of blasting for finding out the most endangered slidy surfaces . The deformation , Stability and stress field of slope summarize the varying pattern of slope stability under the vibration of blasting.

Amin Pourkhosravani ,January 2011, “A review of current method for slope stability evaluation” In this report author discuss the different method of analysis of slope stability (Limit Equilibrium, Numerical Analysis method) L.E method has less accuracy than other methods . The method of analysis can be based on two things :Location of slope and probable slip surface.

Guangjin Wang et al. ,2011, “ Research on slope stability analysis of super high dumping site based on cellular automation” The most important characteristics of super high jumping site is the size grading of particle . FLAC 3D software was used to analyze the stability of slope for various pilling up pattern slope based on the model. On site survey data obtained for granular size distribution and geological data. A model generated with the properties of particle size grading.

Digvijay et al. , 2017, “An overview on methods for slope stability analysis” For different soil type and slope condition the FOS find out with the principle of L.E. and F.E.M. . The various factor of safety and various parameters used by the author and reviewed and disscess . Ass s suggestion , same mathematical tools are suggested for analysis of slope.

Yu Zhoa and Zhi-Yi tong , 2014, “Slope Stability analysis using slice wise factor of safety” , In this report it is taken that the interslice force ratio is equal between the two slices and the slice weight is also taken into account for eccentric moment. Equilibrium forces and moments and the forces of interslice taken into consideration for calculating the FOS.

Xu ejun Zhou et al, 2018 , “Analysis of Slope stability with Imprecise soil properties using Uncertain sets” Due to variation of mineral composition and stress behavior of the soil. The uncertainty starts from the starting errors on account of sampling disturbance and human activities . The Unit weight, C and Φ expresses the uncertain sets of methodology.

An-Juili et al. , August 2018, “Seismic slope stability evaluation considering Rock Mass Disturbance varying in the slope” . In this analysis Finite Element and Limit Equilibrium approach is used for Seismic slope stability behavior . Same investigation performs for

Earthquake and Check out the Slope Failure During Earthquake , The generalized Hoek –Brown Failure Criterion is taken into account.

Yongtao Zhang , 2015, “The study methods and the New Progress of slope Stability” Two type of methods used (Limit Equilibrium and Numerical Analysis) most disadvantages introduce the 3D dynamic stability of slope on the research. It can concluded through that software . it is not exactly explained that all the very accurate results but it gives the mature and effective results.

Shuren Wang et al. , January 2019 , “Stability of step shaped Dump. Slope and reinforcement –Optimization analysis of Anti-Slide Piles” , By using FLAC 3D Software a three Dimentional numerical calculation done. Software made of dumping slope constructed and by the loading process the step shaped dumping slope analyzed,

Aizhang Lu, Ning Zhang , May 2015, “Analytical method of calculating slope stability by elasticity theory and limit equilibrium method” By explicit expressions Hmax can be calculated with the help of γ and ϕ . By Non linear equation of γ , C and ϕ , Φ_{max} can be calculated.

Chunyuan Liu et al. , June 2018, “Analysis of Road Embankment slope stability” For different height and slopes different method of slope stability solved.

Katsahiki Arai and Keijchi Jagyo, March 1985, “Determination of Non circular slip surface giving the minimum factor of safety in slope stability analysis” Different shapes of slip surfaces like slice has been taken into consideration, each method have its own surface of slip here in this report non circular slip surface taken into consideration which gives the least value of FOS.

2.1. Type of Slope

Topography, Characteristics of soils and geography are the various factors which taken into account for analyzing the slope stability .Type of the soil is one of the main factor for analyzing any information. Infinite slope and Finite slope are the two types of slopes . and according to Murthy 2003 , Slopes has been also classified as natural slope and man made slope.

2.1.1. Infinite slope

A parallel surface considers from the surface of the original slope for too long slope failure. According to the balance of forces acting on slices “abcd” in figure, infinite slope stability analysis can made. Equation for FOS for infinite slope surface is show as:

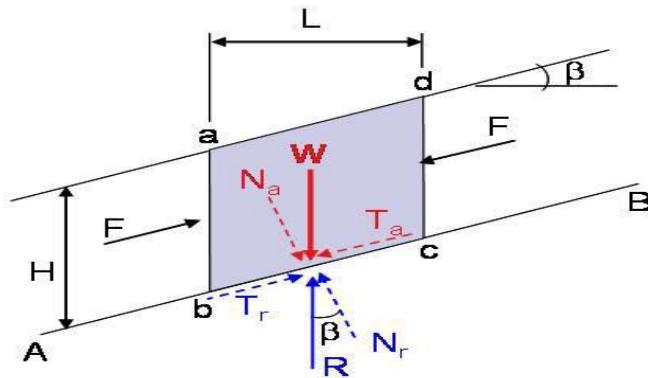


Figure1.1 : Analysis of infinite slope

Source: Winniyarti , 2010

$$FOS = c / (\gamma H \cos^2 \beta \tan \beta) + (\tan \Phi / \tan \beta)$$

Where

FOS = factor of safety

c' = effective cohesion of soil (kN/ m²)

γ = unit weight of soil (kN/m³)

W = weight slice (= $\gamma \times$ slices area (kN/m)

α = inclination of slip surface (degree)

ϕ' = effective friction angle of the soil

β = inclination angle of slope.

If ground water level is below the plane of failure so $c'=0$

$$FOS = 9 = (\tan \Phi / \tan \beta)$$

2.1.2. Finite slope

The slopes generally considered as finite slope when the critical height approaches the height of slopes. The general shape of the surface of potential failure have to take into consideration for the analysis of finite slope. According to Culmann (1875) slope failures usually occurs on the curved failure surface. According to Swedish , Geotechnical commission recommended that actual failure surface may be to be circularly cylindrical . After this assumption in most of the stability analysis of slopes slopes is considered as arc of a circle.

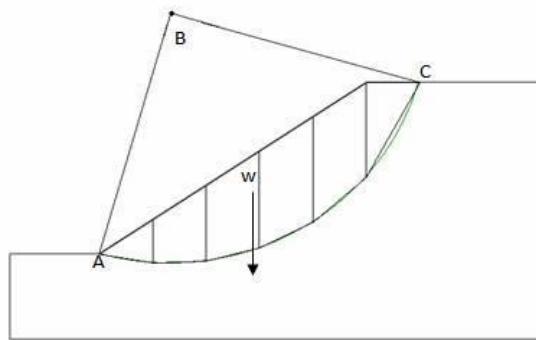


Figure1.2 : Circular slip surface

Source: Winniyarti , 2010

2.1.3. Natural Slopes

In hilly areas natural slopes can be obtain, in hill areas formation processes take a long time without disturbance process. The movement of the earth's core and earthquake may influenced th slope formation. This type of slopes are strong and stable as long as no human activities suh as mining and logging that effect the stability of slope .

2.1.4.Man-made slope

Man cut the slope or embankment for providing ground level to facilitate construction , mam made slopes are those slopes which are generated for desired construction . the stability of these type of slopes monitored time to time to prevent landslides. Itt can be classified into two categories :

1: Cut Slopes

2: Fill Slopes

1. Cut Slopes

Cut slope is one of the type of man -made slope which is generated for the construction of roads and other infrastructures. By changing the height and angle the geometry of the slope construction influenced . Each country has its own guidelines for construction of cut slopes.

2. Fill slopes

Fill slope is one of the type of man made slope, It can be generated by reclamation of land from other areas.This type of slope can be seen easily in Highway construction.Each country has its own guidelines for construction of fill slope.

2.2. Types of slope failure

In response to gravitational stresses the movement of rock debris and soil can lead to the slope failure.The several types of the failures are obtained through the study of ground movement.

1. Topples
2. Flowage
3. Sliding
4. Lateral spread

1. Topple

About a point or axis below the centre of gravity of the displaced mass, Topples is the forward rotation out of the slope of rock mass or soil mass. It is sometimes driven by gravity exerted by material upslope of the displaced mass and sometimes by water or ice in cracks in the soil mass. These type of slope failures occurs due to human activity such as cutting slopes , quarrying which are not in prescribed standards .



Figure1.3 : Topple

Source : Idaho Geological Survey , 2008

2.Flowage

The main mechanism for this process depends on the water content .When the material is in the liquid state, flow can be defined as unconsolidated material. In this type of slope failure the several categories are:

1. Debris flow
2. Mudflow

Debris flow :

The combination of rock, loose soil, organic matter, air and water mobilize as slurry in the form of rapid mass movement that flows down slope. Debris flow is due to intense surface water flow, On account of heavy rain or rapid snowmelt erodes and mobilizes loose soils or rock on steep slopes.

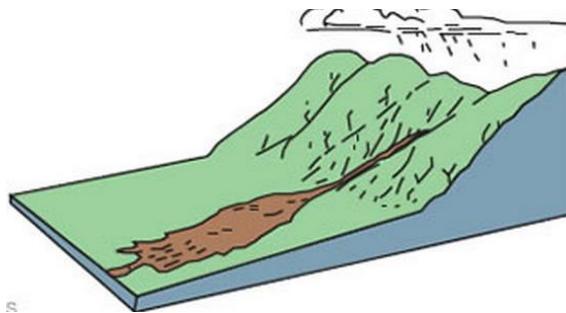


Figure1.4: Debris flow

Source : Idaho Geological Survey , 2008.

2. Mudflow :

Those type of materials that are wet enough to flow rapidly and contains atleast 50% sand , silt and clay size particles comes in the mud flow .Those countries have high heavy rainfall mudflow is one of the main kind of slope failure that occurs frequently. Mudflows and the Debris flow are referred as “mudslides”.

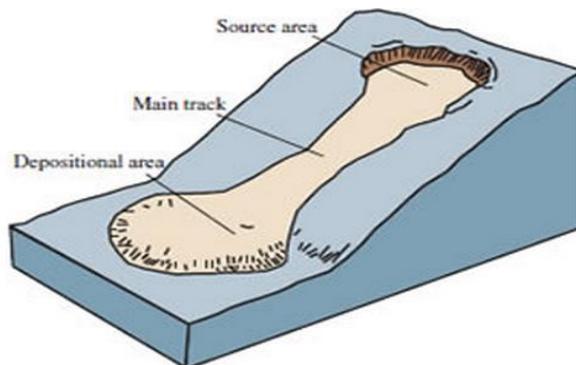


Figure1.5 : Mudflow

Source : Idaho Geological Survey , 2008.

3. Sliding

It can be defined as Continuous and uniform movements in a smooth surface, It can be classified as:

1. Translational slide
2. Rotational slide

1. Translational slide :

In the translational slide landslides occurs when the slide downwards and outwards translationally . When the base is stronger than the upper layer slip plane influenced . landslides of this type contains a greater failure. This is due to the fault plane , which extends for some distance and it is very difficult for expected failure.

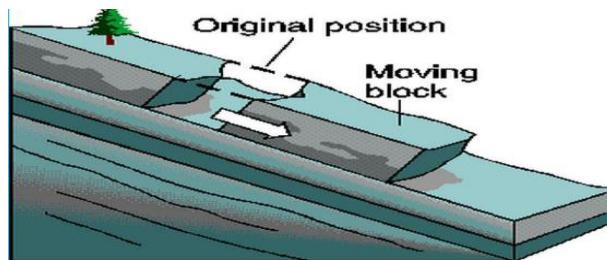


Figure1.6 : Translational Slide

Source : Idaho Geological Survey , 2008.

2. Rotational Slide

It is also known as slump , It is described as the sliding of the material along the curved surface. due to the erosion at the base of the slope this slide occurs. It slides downward or outwards that gives the backward tilt to the slipping mass.

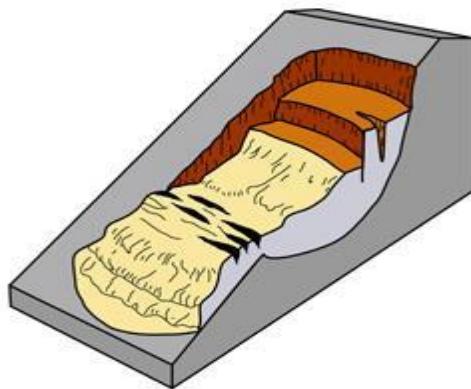


Figure1.7 : Rotational slide

Source ;Idaho Geological Survey , 2008.

4. Lateral spread:

This type of the slope failure occurs at a very wavy or gentle slope. By shear or tensile fractures lateral extension accompanied . By rapid movement of the soil failure occurs, such as by the earthquake effect. Lateral spreading in fine grained materials on low slopes is progressive, the failure starts in a small area and spreads rapidly.

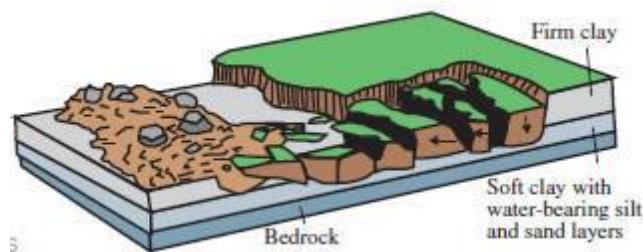


Figure1.8 : Lateral spread

Source : Idaho Geological Survey , 2008.

3.Methodology

In this report we have taken soil sample of Himachal, Jammu, Punjab and DTU, Delhi region and study of slope stability done with the help of geotechnical software code Slope/w (Geo-slope). By using the limit equilibrium within the Morgenstern–Price method, Bishop, Janbu and Ordinary Method along with Mohr-Coulomb expression Factor of safety determined. We have taken laboratory test results on soil to get the Cohesion, Unit weight and Phi value of all Four sample of soil. **The Lab results for Himachal, Jammu and Punjab soil obtained from the research paper “Slope stability Analysis” which was published in IJCEM (International journal core engineering and management) Volume 2, Issue 3, June 2015.** For DTU, Delhi soil sample the following laboratory test has been conducted in the DTU laboratory:

- Modified Proctor Test (IS 2720(1986) Part-13)
- Direct Shear Test (IS 2720(1983) Part-8)
- Sieve Analysis (IS 2720(1985) Part-4)

3.1. Software Package and the respective method Used

GEO-SLOPE International Ltd. , Slope/W 2018 R2 version 9.1.1.16749 (Student License), Operative system Microsoft windows 7 used for performing the analysis.

A software tool Slope/W uses Limit Equilibrium method for computing the FOS OF earth slopes and rock slopes. The users should know about the geotechnical principles which involved in the analysis and the final judgment is necessary to ensure that actual soil properties are used to find the FOS. γ (Unit weight), C (Cohesion) and Φ (Internal friction angle) of soil requires for this analysis.

3.1.1. Limit Equilibrium Method (LE)

The most widely used approach is Limit Equilibrium for solving geotechnical engineering problems like slope stability failures . The limit Equilibrium method requires criteria of Mohr coulomb where the material failure is on account of the combination of the maximum normal stress and maximum shear stress With the help of the soil properties Limit Equilibrium works . The working principle of Mohr column criteria is slope stability by comparison of the forces causing failure against resisting forces .With the help of static equilibrium equation FOS can be analyzed. The basic assumption of the failure is that failure occurs by sliding of mass or block along the slip surface.

3.1.2. Morgenstern-Price Method

This method was generated by N.R. Morgenstern, E. Spencer, which consider not only the normal and tangential equilibrium but also the moment equilibrium for each slice in circular and non-circular slip surfaces. It is solved for the factor of safety using the summation of forces

tangential and normal to the base of a slice and the summation of moments about the center of the base of each slice. The equations were written for a slice of infinitesimal thickness. The Combination of Moment and Force equilibrium and a modified numerical technique of Newton-Raphson was used to solve for the factor of safety satisfying force and moment equilibrium. The requirement of solution an self made assumption regarding the direction of the resultant of the interslice shear and normal forces.

4. Results and Discussion

Modified Proctor test , Direct Shear test and Sieve analysis perform on all the three types of soil , MDD obtained from Modified Proctor test, and by plotting the curve between Normal stress and Shear stress in Direct shear test Φ and C value obtained , And with the help of sieve analysis obtained the classification of soil sample and Cu and Cc. Here in this report we are taking the data from the research paper “Slope stability Analysis” which was published in International Journal of Core Engineering & management (IJCEM) Volume 2, Issue 3, June 2015.

4.1.1. Laboratory Test Results of Himachal Soil (Vivek et al. 2015)

MDD = $2.13\text{g/cm}^3 = 19.31\text{kN/m}^3$ (By modified Proctor test)

Value Of $\phi = 48^\circ$ and $C = 0.0514 \text{ N/mm}^2 = 51.4 \text{ kPa}$ (By Direct Shear test)

Well Graded Soil D10 = 0.081 D30 = 0.18 D60 = 0.52 CU = 0.642 % Gravel = 8.4 % Fines = 8.8 CC = 0.77 % Sand = 82.8% Unified Classification of Soil: SW (By sieve analysis)

4.1.2. Laboratory Test Results of Jammu Soil (Vivek et al. 2015)

MDD = $1.85\text{g/cm}^3 = 16.77\text{kN/m}^3$ (By modified Proctor test)

Value Of $\phi = 64.66^\circ$ Value Of $C = 0.0319 \text{ N/mm}^2 = 31.9 \text{ kPa}$ (By Direct Shear test)

Well Graded Soil D10 = 0.18 D30 = 0.45 D60 = 1.39 CU = 7.72 % Gravel = 3.2 % Fines = 0.4 CC = 0.81 % Sand = 96.4% Unified Classification of Soil: SW (By sieve analysis)

4.1.3. Laboratory Test Result of Punjab Soil (Vivek et al. 2015)

MDD = $1.86\text{g/cm}^3 = 18.24\text{kN/m}^3$ (By modified Proctor test)

Value Of $\phi = 36.86^\circ$ Value Of C= $0.053 \text{ N/mm}^2 = 53 \text{ kPa}$ (By Direct Shear test)

Well Graded Soil D10 = 0.081 D30 = 0.18 D60 = 0.52 CU = 0.642 % Gravel = 8.4 % Fines = 8.8 CC = 0.77 % Sand = 82.8 Unified Classification of Soil: SW (By sieve analysis)

4.1.4 Laboratory Test Result of DTU, Delhi Soil (By Lab tests conducted in DTU Lab)

MDD = $1.69\text{g/cm}^3 = 16.57\text{kN/m}^3$ (By modified Proctor test)

Value Of $\phi = 41.78^\circ$ Value Of C= $0.004 \text{ N/mm}^2 = 4.05 \text{ kPa}$ (By Direct Shear test)

Well Graded Soil D10 = 0.15 D30 = 0.21 D60 = 0.4 CU = 2.67 CC = 0.735

Unified Classification of Soil: SP (By sieve analysis)

4.2. Slope/W analysis

4.2.1. Slope/W analysis of Himachal Soil with Morgenstern-Price Method

File Information

File Version: [9.01](#)

Revision Number: [1](#)

Date: [05/03/2020](#)

Time: [05:24:15 PM](#)

Tool Version: [9.1.1.16749](#)

File Name: [SLOPE W HIMACHAL SOIL.gsz](#)

Directory: [C:\Users\Sys\Documents\](#)

Last Solved Date: [05/03/2020](#)

Last Solved Time: [05:24:18 PM](#)

Project Settings

Unit System: [International System of Units \(SI\)](#)

Analysis Settings

SLOPE/W Analysis on Himachal soil

Kind: [SLOPE/W](#)

Method: [Morgenstern-Price](#)

Settings

Side Function

Interslice force function option: [Half-Sine](#)

PWP Conditions from: [Piezometric Line](#)

Apply Phreatic Correction: [No](#)

Use Staged Rapid Drawdown: [No](#)

Unit Weight of Water: [9.807 kN/m³](#)

Piezometric Line 1

Slip Surface

Direction of movement: [Left to Right](#)

Use Passive Mode: [No](#)

Slip Surface Option: [Entry and Exit](#)

Critical slip surfaces saved: [1](#)

Optimize Critical Slip Surface Location: [No](#)

Tension Crack Option: [\(none\)](#)

Table1.1: Coordinates

| X(m) | Y(m) |
|------|------|
| 0 | 10 |
| 22.8 | 6 |

Distribution

F of S Calculation Option: [Constant](#)

Advanced

Geometry Settings

Minimum Slip Surface Depth: [0.1 m](#)

Number of Slices: [30](#)

Factor of Safety Convergence Settings

Maximum Number of Iterations: [2,000](#)

Tolerable difference in F of S: [0.01](#)

Solution Settings

Search Method: [Root Finder](#)

Tolerable difference between starting and converged F of S: [3](#)

Maximum iterations to calculate converged lambda: [20](#)

Max Absolute Lambda: [2](#)

Materials

Soil layer

Model: [Mohr-Coulomb](#)

Unit Weight: [19.31 kN/m³](#)

Cohesion': [51.4 kPa](#)

Phi': [48 °](#)

Phi-B: [0 °](#)

Pore Water Pressure

Piezometric Line: [1](#)

Table1.2: Region

| | Materials | Points | Area |
|----------|------------|-------------|--------------------|
| Region 1 | Soil layer | 1,2,3,4,5,6 | 316 m ² |

Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (0.96, 14) m

Left-Zone Right Coordinate: (1, 14) m

Left-Zone Increment: 4

Right Type: Range

Right-Zone Left Coordinate: (32.82, 4) m

Right-Zone Right Coordinate: (33, 4) m

Right-Zone Increment: 8

Radius Increments: 4

Table1.3: Points

| | X(m) | Y(m) |
|---------|------|------|
| Point 1 | 0 | 14 |
| Point 2 | 10 | 14 |
| Point 3 | 26 | 4 |

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 4) m

Slip Results

Slip Surfaces Analysed: 180 of 225 converged

Current Slip Surface

Slip Surface: 183

Factor of Safety: 4.552

Volume: 150.40423 m³

Weight: 2,904.3056 kN

Resisting Moment: 107,789.91 kN·m

Activating Moment: 23,679.525 kN·m

Resisting Force: 3,709.4992 kN

Activating Force: 815.09665 kN

Slip Rank: 1 of 225 slip surfaces

Exit: (32.82, 4) m

Entry: (1, 14) m

Radius: 25.782497 m

Center: (22.804997, 27.75788) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength (kPa) | Base Material |
|---------|-----------|-----------|------------|-------------------------|--------------------------|-------------------------|------------------------|---------------|
| Slice 1 | 1.498052 | 13.267647 | -34.623251 | -1.5532061 | -1.7250101 | 51.4 | 0 | Soil layer |
| Slice 2 | 2.4941561 | 11.897488 | -22.899923 | 19.816231 | 22.008154 | 51.4 | 0 | Soil layer |
| Slice 3 | 3.4902601 | 10.695871 | -12.82949 | 38.667619 | 42.944742 | 51.4 | 0 | Soil layer |

| | | | | | | | | |
|----------|-----------|-----------|------------|-----------|-----------|------|---|------------|
| Slice 4 | 4.4863642 | 9.6288006 | -4.0785547 | 55.629565 | 61.782891 | 51.4 | 0 | Soil layer |
| Slice 5 | 5.4859746 | 8.6704509 | 3.6001247 | 71.733872 | 75.670193 | 51.4 | 0 | Soil layer |
| Slice 6 | 6.4890913 | 7.8052209 | 10.359546 | 87.034706 | 85.156392 | 51.4 | 0 | Soil layer |
| Slice 7 | 7.4922081 | 7.0246489 | 16.288727 | 101.14264 | 94.239823 | 51.4 | 0 | Soil layer |
| Slice 8 | 8.4953249 | 6.3194378 | 21.478843 | 114.34903 | 103.14279 | 51.4 | 0 | Soil layer |
| Slice 9 | 9.4984416 | 5.6823329 | 26.001042 | 126.87369 | 112.03043 | 51.4 | 0 | Soil layer |
| Slice 10 | 10.533333 | 5.0912612 | 30.017124 | 133.86605 | 115.33591 | 51.4 | 0 | Soil layer |
| Slice 11 | 11.6 | 4.5450715 | 33.538378 | 135.12763 | 112.8263 | 51.4 | 0 | Soil layer |
| Slice 12 | 12.666667 | 4.0594642 | 36.465501 | 135.57175 | 110.06864 | 51.4 | 0 | Soil layer |
| Slice 13 | 13.733333 | 3.6307704 | 38.834473 | 135.18124 | 107.00393 | 51.4 | 0 | Soil layer |
| Slice 14 | 14.8 | 3.2559949 | 40.674668 | 133.90785 | 103.54594 | 51.4 | 0 | Soil layer |
| Slice 15 | 15.866667 | 2.9326899 | 42.010093 | 131.67801 | 99.586315 | 51.4 | 0 | Soil layer |
| Slice 16 | 16.933333 | 2.6588619 | 42.860296 | 128.3987 | 95.000027 | 51.4 | 0 | Soil layer |
| Slice 17 | 18 | 2.4329027 | 43.241049 | 123.96396 | 89.651869 | 51.4 | 0 | Soil layer |
| Slice 18 | 19.066667 | 2.2535375 | 43.164856 | 118.26228 | 83.404134 | 51.4 | 0 | Soil layer |
| Slice 19 | 20.133333 | 2.1197866 | 42.641323 | 111.18513 | 76.125611 | 51.4 | 0 | Soil layer |
| Slice 20 | 21.2 | 2.0309372 | 41.677441 | 102.63631 | 67.701687 | 51.4 | 0 | Soil layer |
| Slice 21 | 22.266667 | 1.9865241 | 40.277772 | 92.541772 | 58.045052 | 51.4 | 0 | Soil layer |
| Slice 22 | 23.333333 | 1.9863172 | 39.362187 | 84.72652 | 50.382196 | 51.4 | 0 | Soil layer |
| Slice 23 | 24.4 | 2.0303154 | 38.930697 | 79.150649 | 44.668782 | 51.4 | 0 | Soil layer |
| Slice 24 | 25.466667 | 2.1187467 | 38.063451 | 71.835004 | 37.507109 | 51.4 | 0 | Soil layer |
| Slice 25 | 26.568333 | 2.2579896 | 36.697896 | 63.859635 | 30.166167 | 51.4 | 0 | Soil layer |
| Slice 26 | 27.705 | 2.4519122 | 34.796097 | 59.909744 | 27.89153 | 51.4 | 0 | Soil layer |
| Slice 27 | 28.841667 | 2.6988692 | 32.37419 | 54.461784 | 24.530758 | 51.4 | 0 | Soil layer |
| Slice 28 | 29.978333 | 3.0004513 | 29.416574 | 47.575021 | 20.166999 | 51.4 | 0 | Soil layer |
| Slice 29 | 31.115 | 3.3586889 | 25.903338 | 39.347048 | 14.930752 | 51.4 | 0 | Soil layer |
| Slice 30 | 32.251667 | 3.7761274 | 21.809519 | 29.905045 | 8.9909924 | 51.4 | 0 | Soil layer |

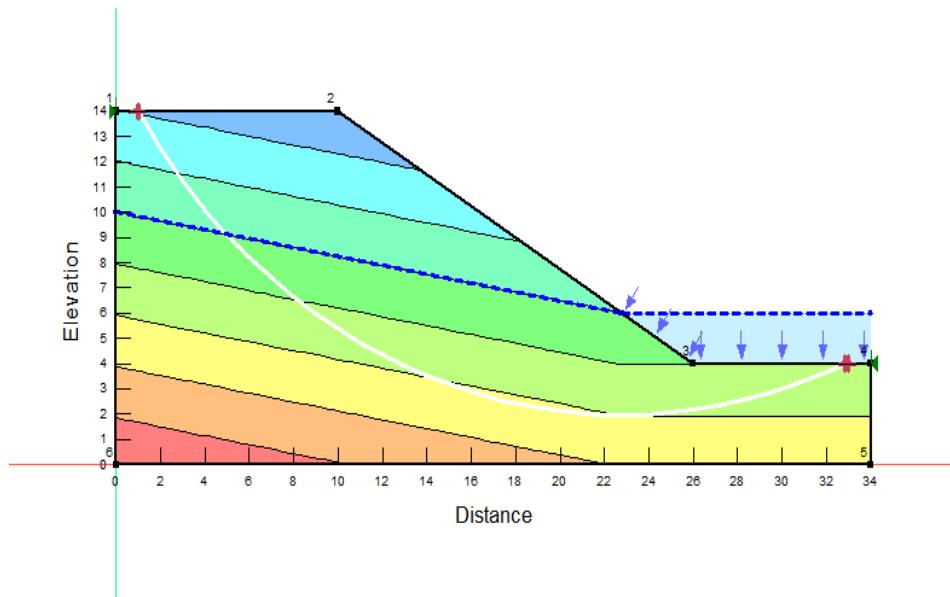


Figure2.1: Pore Pressure through Piezometric line (Himachal region sample Slope/W Analysis with Morgenstern-Price method)

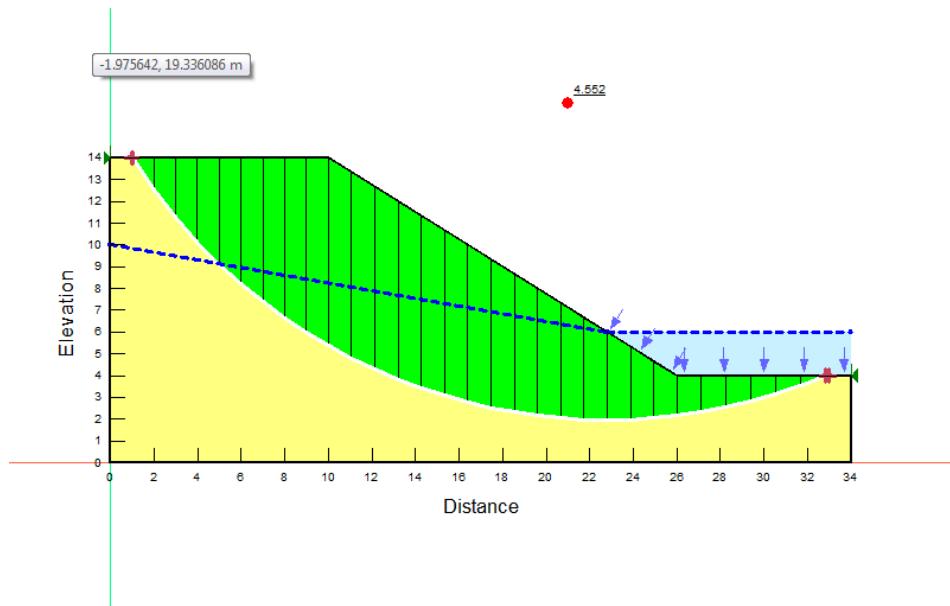


Figure2.2: Factor of safety and slip surface results of Morgenstern-Price analysis computed by SLOPE/W

4.2.2. Slope/W analysis on Himachal soil with Bishop Method

File Information

File Version: [9.01](#)
 Revision Number: [2](#)
 Date: [06/21/2020](#)
 Time: [02:15:30 AM](#)
 Tool Version: [9.1.1.16749](#)
 File Name: [SLOPE W HIMACHAL BISHOP.gsz](#)
 Directory: [C:\Users\Sys\Desktop\Major project content\Geoslope Himachal soil Content\](#)
 Last Solved Date: [06/21/2020](#)
 Last Solved Time: [02:15:34 AM](#)

Project Settings

Unit System: [International System of Units \(SI\)](#)

Analysis Settings

SLOPE W HIMACHAL SOIL BISHOP

Kind: [SLOPE/W](#)

Method: [Bishop](#)

Settings

PWP Conditions from: [Piezometric Line](#)

Apply Phreatic Correction: [Yes](#)

Use Staged Rapid Drawdown: [No](#)

Unit Weight of Water: [9.807 kN/m³](#)

Slip Surface

Direction of movement: [Left to Right](#)

Use Passive Mode: [No](#)

Slip Surface Option: [Entry and Exit](#)

Critical slip surfaces saved: [1](#)

Optimize Critical Slip Surface Location: [No](#)

Tension Crack Option: [\(none\)](#)

Distribution

F of S Calculation Option: [Constant](#)

Advanced

Geometry Settings

Minimum Slip Surface Depth: [0.1 m](#)

Number of Slices: [30](#)

Factor of Safety Convergence Settings

Maximum Number of Iterations: [30](#)

Tolerable difference in F of S: [0.01](#)

Materials

Soil Layer

Model: [Mohr-Coulomb](#)

Unit Weight: [19.31 kN/m³](#)

Cohesion': [51.4 kPa](#)

Phi': [48 °](#)

Phi-B: [0 °](#)

Pore Water Pressure

Piezometric Line: [1](#)

Slip Surface Entry and Exit

Left Type: [Range](#)

Left-Zone Left Coordinate: [\(0.96, 14\) m](#)

Left-Zone Right Coordinate: [\(1, 14\) m](#)

Left-Zone Increment: [4](#)

Right Type: [Range](#)

Right-Zone Left Coordinate: [\(32.82, 4\) m](#)

Right-Zone Right Coordinate: [\(33, 4\) m](#)

Right-Zone Increment: [4](#)

Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 4) m

Slip Results

Slip Surfaces Analysed: 100 of 125 converged

Current Slip Surface

Slip Surface: 103

Factor of Safety: 4.575

Volume: 150.40423 m³

Weight: 2,904.3056 kN

Resisting Moment: 108,326.24 kN·m

Activating Moment: 23,679.525 kN·m

Slip Rank: 1 of 125 slip surfaces

Exit: (32.82, 4) m

Entry: (1, 14) m

Radius: 25.782497 m

Center: (22.804997, 27.75788) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength(kPa) | Suction Strength (kPa) | Base Material |
|----------|-----------|-----------|------------|-------------------------|--------------------------|------------------------|------------------------|---------------|
| Slice 1 | 1.498052 | 13.267647 | -33.589413 | -1.7470058 | -1.9402465 | 51.4 | 0 | Soil Layer |
| Slice 2 | 2.4941561 | 11.897488 | -22.216139 | 20.003657 | 22.216312 | 51.4 | 0 | Soil Layer |
| Slice 3 | 3.4902601 | 10.695871 | -12.446405 | 40.081511 | 44.515027 | 51.4 | 0 | Soil Layer |
| Slice 4 | 4.4863642 | 9.6288006 | -3.9567704 | 58.67548 | 65.165723 | 51.4 | 0 | Soil Layer |
| Slice 5 | 5.4859746 | 8.6704509 | 3.4926262 | 76.624252 | 81.220899 | 51.4 | 0 | Soil Layer |
| Slice 6 | 6.4890913 | 7.8052209 | 10.050213 | 93.818148 | 93.033717 | 51.4 | 0 | Soil Layer |
| Slice 7 | 7.4922081 | 7.0246489 | 15.802351 | 109.59302 | 104.16509 | 51.4 | 0 | Soil Layer |
| Slice 8 | 8.4953249 | 6.3194378 | 20.837492 | 124.09361 | 114.67753 | 51.4 | 0 | Soil Layer |
| Slice 9 | 9.4984416 | 5.6823329 | 25.22466 | 137.43426 | 124.62139 | 51.4 | 0 | Soil Layer |
| Slice 10 | 10.533333 | 5.0912612 | 29.120823 | 144.37187 | 127.99926 | 51.4 | 0 | Soil Layer |
| Slice 11 | 11.6 | 4.5450715 | 32.536934 | 144.70664 | 124.57707 | 51.4 | 0 | Soil Layer |
| Slice 12 | 12.666667 | 4.0594642 | 35.376654 | 143.71844 | 120.32574 | 51.4 | 0 | Soil Layer |
| Slice 13 | 13.733333 | 3.6307704 | 37.674889 | 141.4808 | 115.28815 | 51.4 | 0 | Soil Layer |
| Slice 14 | 14.8 | 3.2559949 | 39.460137 | 138.05246 | 109.49787 | 51.4 | 0 | Soil Layer |
| Slice 15 | 15.866667 | 2.9326899 | 40.755686 | 133.47999 | 102.98077 | 51.4 | 0 | Soil Layer |
| Slice 16 | 16.933333 | 2.6588619 | 41.580502 | 127.79973 | 95.75615 | 51.4 | 0 | Soil Layer |

| | | | | | | | | |
|----------|-----------|-----------|-----------|-----------|-----------|------|---|------------|
| Slice 17 | 18 | 2.4329027 | 41.949886 | 121.0391 | 87.837476 | 51.4 | 0 | Soil Layer |
| Slice 18 | 19.066667 | 2.2535375 | 41.875968 | 113.21766 | 79.232978 | 51.4 | 0 | Soil Layer |
| Slice 19 | 20.133333 | 2.1197866 | 41.368068 | 104.34769 | 69.945951 | 51.4 | 0 | Soil Layer |
| Slice 20 | 21.2 | 2.0309372 | 40.432967 | 94.434626 | 59.974918 | 51.4 | 0 | Soil Layer |
| Slice 21 | 22.266667 | 1.9865241 | 39.075092 | 83.477274 | 49.31362 | 51.4 | 0 | Soil Layer |
| Slice 22 | 23.333333 | 1.9863172 | 39.362187 | 74.742749 | 39.294095 | 51.4 | 0 | Soil Layer |
| Slice 23 | 24.4 | 2.0303154 | 38.930697 | 68.289409 | 32.606153 | 51.4 | 0 | Soil Layer |
| Slice 24 | 25.466667 | 2.1187467 | 38.063451 | 60.84834 | 25.305183 | 51.4 | 0 | Soil Layer |
| Slice 25 | 26.568333 | 2.2579896 | 36.697896 | 55.585831 | 20.977177 | 51.4 | 0 | Soil Layer |
| Slice 26 | 27.705 | 2.4519122 | 34.796097 | 52.514352 | 19.678116 | 51.4 | 0 | Soil Layer |
| Slice 27 | 28.841667 | 2.6988692 | 32.37419 | 48.379484 | 17.77568 | 51.4 | 0 | Soil Layer |
| Slice 28 | 29.978333 | 3.0004513 | 29.416574 | 43.133248 | 15.23391 | 51.4 | 0 | Soil Layer |
| Slice 29 | 31.115 | 3.3586889 | 25.903338 | 36.715791 | 12.008446 | 51.4 | 0 | Soil Layer |
| Slice 30 | 32.251667 | 3.7761274 | 21.809519 | 29.052616 | 8.044275 | 51.4 | 0 | Soil Layer |

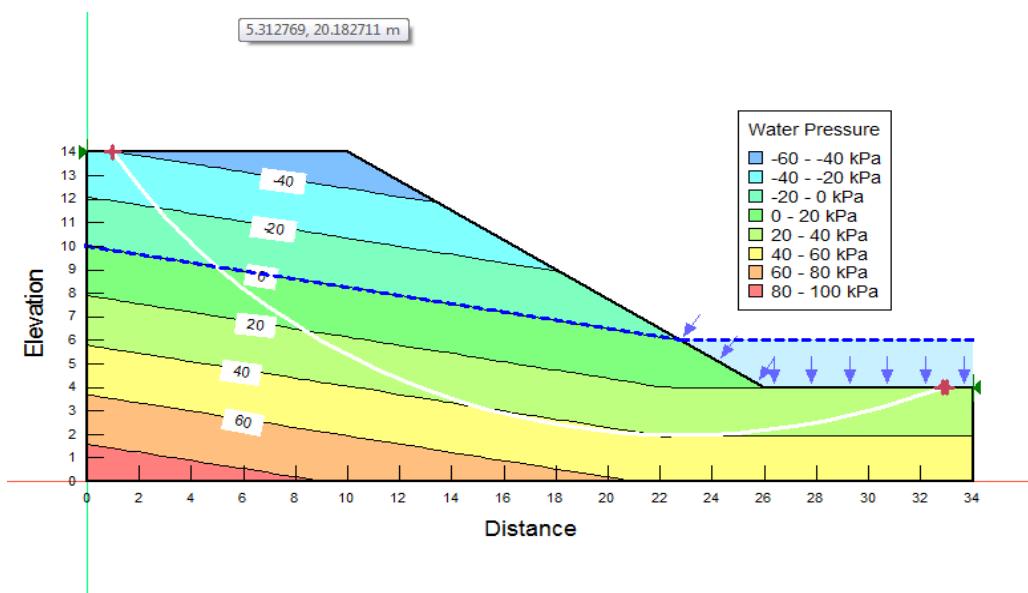


Figure2.3: Pore Pressure through Piezometric line (Himachal region sample Slope/W Analysis with Bishop method)

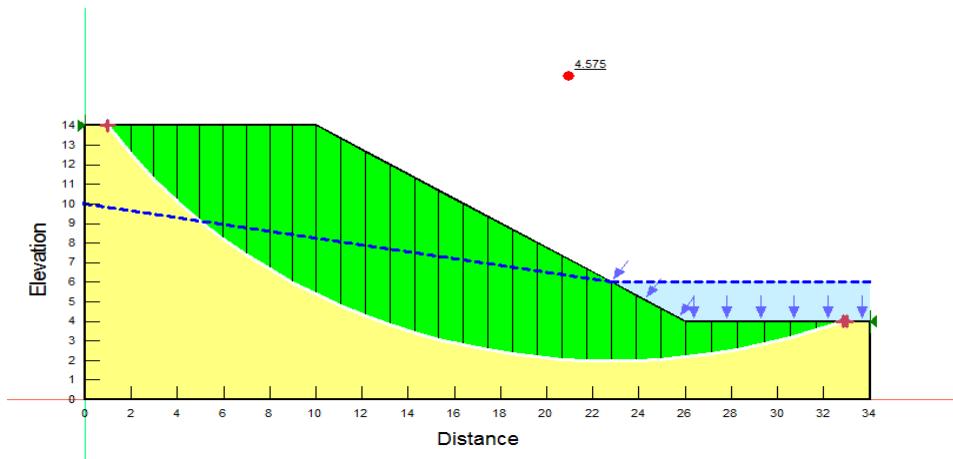


Figure 2.4: Factor of safety and slip surface results of Bishop analysis computed by SLOPE/W

4.2.3. Slope/W analysis of Himachal soil with Janbu Method

File Information

File Version: 9.01
 Revision Number: 1
 Date: 06/21/2020
 Time: 02:04:50 PM
 Tool Version: 9.1.1.16749
 File Name: SLOPE W HIMACHAL JANBU.gsz
 Directory: C:\Users\Sys\Desktop\Major project content\Geoslope Himachal soil Content\
 Last Solved Date: 06/21/2020
 Last Solved Time: 02:04:56 PM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

Slope w Himachal Janbu

Kind: SLOPE/W
 Method: Janbu
 Settings
 PWP Conditions from: Piezometric Line
 Apply Phreatic Correction: Yes
 Use Staged Rapid Drawdown: No

Unit Weight of Water: 9.807 kN/m³

Slip Surface

Direction of movement: Left to Right

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

Geometry Settings

Minimum Slip Surface Depth: 0.1 m

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

Materials

Soil Layer

Model: Mohr-Coulomb

Unit Weight: 19.31 kN/m³

Cohesion': 51.4 kPa

Phi': 48 °

Phi-B: 0 °

Pore Water Pressure

Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (0.96, 14) m

Left-Zone Right Coordinate: (1, 14) m

Left-Zone Increment: 4

Right Type: Range

Right-Zone Left Coordinate: (32.82, 4) m

Right-Zone Right Coordinate: (33, 4) m

Right-Zone Increment: 4

Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 4) m

Slip Results

Slip Surfaces Analysed: 100 of 125 converged

Current Slip Surface

Slip Surface: 104

Factor of Safety: 4.173

Volume: 216.60687 m³

Weight: 4,182.6786 kN

Resisting Force: 4,407.511 kN

Activating Force: 1,056.2541 kN

Slip Rank: 1 of 125 slip surfaces

Exit: (32.82, 4) m

Entry: (1, 14) m

Radius: 20.107733 m

Center: (20.277944, 19.716799) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength(kPa) | Base Material |
|----------|-----------|-------------|------------|-------------------------|--------------------------|-------------------------|------------------------|---------------|
| Slice 1 | 1.4929643 | 12.683382 | -28.022126 | -4.3665404 | -4.8495344 | 51.4 | 0 | Soil Layer |
| Slice 2 | 2.478893 | 10.422693 | -8.159217 | 30.134049 | 33.467252 | 51.4 | 0 | Soil Layer |
| Slice 3 | 3.4738675 | 8.7120593 | 6.4552692 | 61.09895 | 60.687955 | 51.4 | 0 | Soil Layer |
| Slice 4 | 4.4778879 | 7.306374 | 18.15333 | 89.426633 | 79.157022 | 51.4 | 0 | Soil Layer |
| Slice 5 | 5.4819083 | 6.1209262 | 27.756015 | 113.81761 | 95.581089 | 51.4 | 0 | Soil Layer |
| Slice 6 | 6.4859286 | 5.1008895 | 35.784952 | 135.24428 | 110.46077 | 51.4 | 0 | Soil Layer |
| Slice 7 | 7.489949 | 4.2131018 | 42.555649 | 154.29852 | 124.10303 | 51.4 | 0 | Soil Layer |
| Slice 8 | 8.4939694 | 3.4356803 | 48.276303 | 171.3732 | 136.71295 | 51.4 | 0 | Soil Layer |
| Slice 9 | 9.4979898 | 2.7533171 | 53.092558 | 186.74473 | 148.43577 | 51.4 | 0 | Soil Layer |
| Slice 10 | 10.527685 | 2.1415547 | 57.19425 | 195.384 | 153.47526 | 51.4 | 0 | Soil Layer |
| Slice 11 | 11.583054 | 1.5956165 | 60.626824 | 197.08914 | 151.55675 | 51.4 | 0 | Soil Layer |
| Slice 12 | 12.638424 | 1.1255865 | 63.337196 | 197.07674 | 148.53281 | 51.4 | 0 | Soil Layer |
| Slice 13 | 13.693793 | 0.72580218 | 65.379238 | 195.47265 | 144.48337 | 51.4 | 0 | Soil Layer |
| Slice 14 | 14.749163 | 0.3918861 | 66.794599 | 192.37185 | 139.46767 | 51.4 | 0 | Soil Layer |
| Slice 15 | 15.804533 | 0.12045879 | 67.615431 | 187.84524 | 133.52872 | 51.4 | 0 | Soil Layer |
| Slice 16 | 16.871199 | 0 | 66.981068 | 187.41321 | 133.75345 | 51.4 | 0 | Soil Layer |
| Slice 17 | 17.949163 | 0 | 65.181782 | 174.40354 | 121.30305 | 51.4 | 0 | Soil Layer |
| Slice 18 | 19.027127 | 0 | 63.382497 | 161.39386 | 108.85265 | 51.4 | 0 | Soil Layer |
| Slice 19 | 20.105091 | 0 | 61.583211 | 148.38419 | 96.402252 | 51.4 | 0 | Soil Layer |
| Slice 20 | 21.183054 | 0 | 59.783926 | 135.37451 | 83.951852 | 51.4 | 0 | Soil Layer |
| Slice 21 | 22.261018 | 0 | 57.984641 | 122.36484 | 71.501453 | 51.4 | 0 | Soil Layer |
| Slice 22 | 23.511836 | 0 | 58.842 | 111.63214 | 58.62939 | 51.4 | 0 | Soil Layer |
| Slice 23 | 24.667754 | 0.099372651 | 57.867452 | 108.62645 | 56.373576 | 51.4 | 0 | Soil Layer |
| Slice 24 | 25.555918 | 0.31957981 | 55.707881 | 99.869414 | 49.046352 | 51.4 | 0 | Soil Layer |
| Slice 25 | 26.568333 | 0.62769591 | 52.686186 | 92.262197 | 43.953613 | 51.4 | 0 | Soil Layer |
| Slice 26 | 27.705 | 1.0409942 | 48.63297 | 85.558072 | 41.00948 | 51.4 | 0 | Soil Layer |

| | | | | | | | | |
|----------|-----------|-----------|-----------|-----------|-----------|------|---|------------|
| Slice 27 | 28.841667 | 1.5346943 | 43.791253 | 77.208382 | 37.113482 | 51.4 | 0 | Soil Layer |
| Slice 28 | 29.978333 | 2.1155981 | 38.094329 | 67.033751 | 32.140484 | 51.4 | 0 | Soil Layer |
| Slice 29 | 31.115 | 2.7927418 | 31.453581 | 54.788976 | 25.916581 | 51.4 | 0 | Soil Layer |
| Slice 30 | 32.251667 | 3.5783326 | 23.749292 | 40.127956 | 18.190349 | 51.4 | 0 | Soil Layer |

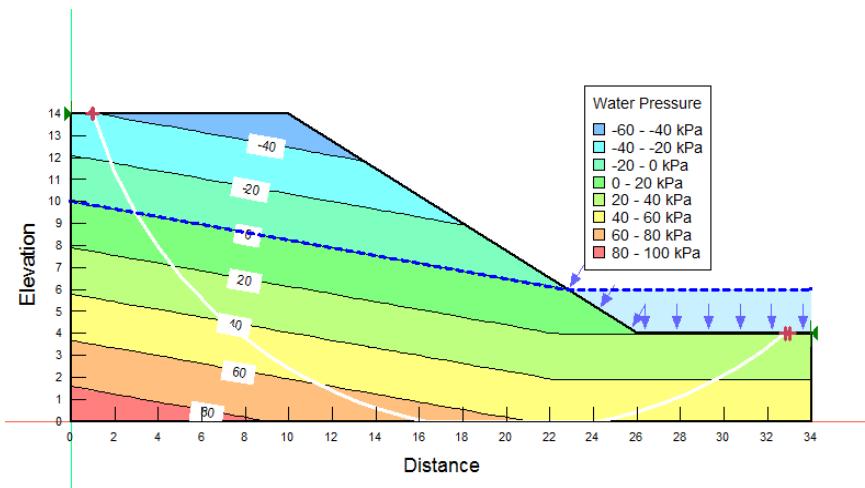


Figure2.5 : Pore Pressure through Piezometric line (Himalayan region sample Slope/W Analysis with Janbu method)

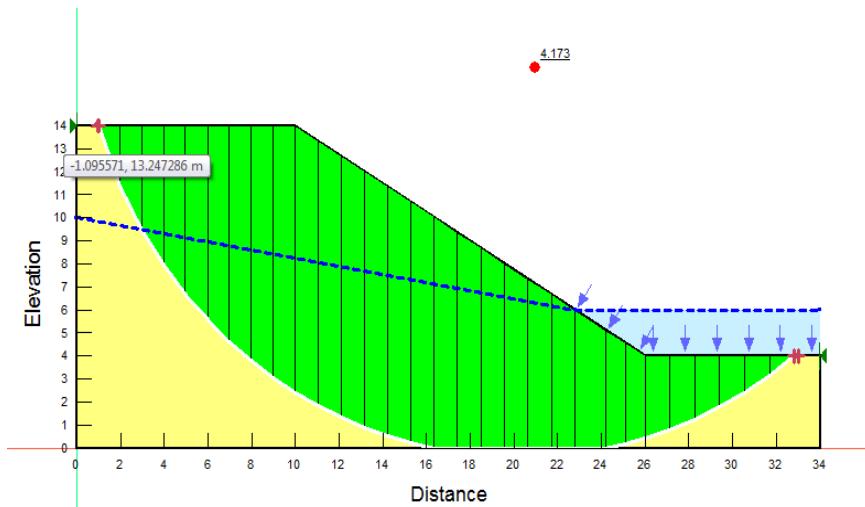


Figure2.6: Factor of safety and slip surface results of Janbu analysis computed by SLOPE/W

4.2.4. Slope/W analysis of Himachal soil by Ordinary method

File Information

File Version: 9.01

Revision Number: 1

Date: 06/21/2020

Time: 02:45:06 PM

Tool Version: 9.1.1.16749

File Name: SLOPE W HIMACHAL Ordinary.gsz

Directory: C:\Users\Sys\Desktop\Major project content\Geoslope Himachal soil Content\

Last Solved Date: 06/21/2020

Last Solved Time: 02:45:08 PM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

Slope w himachal Ordinary

Kind: SLOPE/W

Method: Ordinary

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: Yes

Use Staged Rapid Drawdown: No

Unit Weight of Water: 9.807 kN/m³

Slip Surface

Direction of movement: Left to Right

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

Geometry Settings

Minimum Slip Surface Depth: 0.1 m

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

Materials

New Material

Model: Mohr-Coulomb

Unit Weight: 19.31 kN/m³

Cohesion': 51.4 kPa

Phi': 48 °

Phi-B: 0 °

Pore Water Pressure

Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (0.96, 14) m

Left-Zone Right Coordinate: (1, 14) m

Left-Zone Increment: 4

Right Type: Range

Right-Zone Left Coordinate: (32.82, 4) m

Right-Zone Right Coordinate: (33, 4) m

Right-Zone Increment: 4

Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 4) m

Slip Results

Slip Surfaces Analysed: 100 of 125 converged

Current Slip Surface

Slip Surface: 104

Factor of Safety: 4.246

Volume: 216.60687 m³

Weight: 4,182.6786 kN

Resisting Moment: 95,053.864 kN·m

Activating Moment: 22,387.531 kN·m

Slip Rank: 1 of 125 slip surfaces

Exit: (32.82, 4) m

Entry: (1, 14) m

Radius: 20.107733 m

Center: (20.277944, 19.716799) m

Slip Slices

| | X (m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength (kPa) | Base Material |
|----------|-----------|-------------|------------|-------------------------|--------------------------|-------------------------|------------------------|---------------|
| Slice 1 | 1.4929643 | 12.683382 | -28.022126 | 3.1259131 | 3.4716782 | 51.4 | 0 | New Material |
| Slice 2 | 2.478893 | 10.422693 | -8.159217 | 14.799522 | 16.436534 | 51.4 | 0 | New Material |
| Slice 3 | 3.4738675 | 8.7120593 | 6.4552692 | 35.165932 | 31.886422 | 51.4 | 0 | New Material |
| Slice 4 | 4.4778879 | 7.306374 | 18.15333 | 60.544314 | 47.079957 | 51.4 | 0 | New Material |
| Slice 5 | 5.4819083 | 6.1209262 | 27.756015 | 84.701762 | 63.244659 | 51.4 | 0 | New Material |
| Slice 6 | 6.4859286 | 5.1008895 | 35.784952 | 107.75603 | 79.931978 | 51.4 | 0 | New Material |
| Slice 7 | 7.489949 | 4.2131018 | 42.555649 | 129.69766 | 96.781013 | 51.4 | 0 | New Material |
| Slice 8 | 8.4939694 | 3.4356803 | 48.276303 | 150.46464 | 113.49165 | 51.4 | 0 | New Material |
| Slice 9 | 9.4979898 | 2.7533171 | 53.092558 | 169.97303 | 129.80892 | 51.4 | 0 | New Material |
| Slice 10 | 10.527685 | 2.1415547 | 57.19425 | 183.68708 | 140.48453 | 51.4 | 0 | New Material |
| Slice 11 | 11.583054 | 1.5956165 | 60.626824 | 190.51863 | 144.25947 | 51.4 | 0 | New Material |
| Slice 12 | 12.638424 | 1.1255865 | 63.337196 | 194.59822 | 145.78014 | 51.4 | 0 | New Material |
| Slice 13 | 13.693793 | 0.72580218 | 65.379238 | 196.0399 | 145.11336 | 51.4 | 0 | New Material |
| Slice 14 | 14.749163 | 0.3918861 | 66.794599 | 194.96532 | 142.34801 | 51.4 | 0 | New Material |
| Slice 15 | 15.804533 | 0.12045879 | 67.615431 | 191.50453 | 137.59278 | 51.4 | 0 | New Material |
| Slice 16 | 16.871199 | 0 | 66.981068 | 187.41321 | 133.75345 | 51.4 | 0 | New Material |
| Slice 17 | 17.949163 | 0 | 65.181782 | 174.40354 | 121.30305 | 51.4 | 0 | New Material |
| Slice 18 | 19.027127 | 0 | 63.382497 | 161.39386 | 108.85265 | 51.4 | 0 | New Material |
| Slice 19 | 20.105091 | 0 | 61.583211 | 148.38419 | 96.402252 | 51.4 | 0 | New Material |
| Slice 20 | 21.183054 | 0 | 59.783926 | 135.37451 | 83.951852 | 51.4 | 0 | New Material |
| Slice 21 | 22.261018 | 0 | 57.984641 | 122.36484 | 71.501453 | 51.4 | 0 | New Material |
| Slice 22 | 23.511836 | 0 | 58.842 | 111.63214 | 58.62939 | 51.4 | 0 | New Material |
| Slice 23 | 24.667754 | 0.099372651 | 57.867452 | 99.178153 | 45.880181 | 51.4 | 0 | New Material |
| Slice 24 | 25.555918 | 0.31957981 | 55.707881 | 88.053011 | 35.922907 | 51.4 | 0 | New Material |
| Slice 25 | 26.568333 | 0.62769591 | 52.686186 | 81.594122 | 32.105515 | 51.4 | 0 | New Material |
| Slice 26 | 27.705 | 1.0409942 | 48.63297 | 72.91254 | 26.965194 | 51.4 | 0 | New Material |
| Slice 27 | 28.841667 | 1.5346943 | 43.791253 | 62.965474 | 21.295129 | 51.4 | 0 | New Material |
| Slice 28 | 29.978333 | 2.1155981 | 38.094329 | 51.829853 | 15.254844 | 51.4 | 0 | New Material |
| Slice 29 | 31.115 | 2.7927418 | 31.453581 | 39.589997 | 9.0364049 | 51.4 | 0 | New Material |
| Slice 30 | 32.251667 | 3.5783326 | 23.749292 | 26.333738 | 2.8703173 | 51.4 | 0 | New Material |

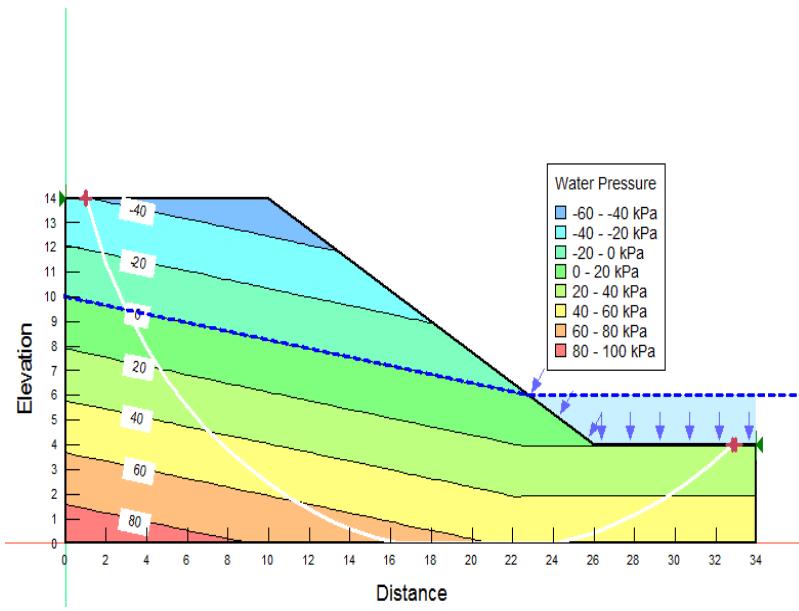


Figure2.7: Pore Pressure through Peizometric line (Himalayan region sample Slope/W Analysis with Ordinary method)

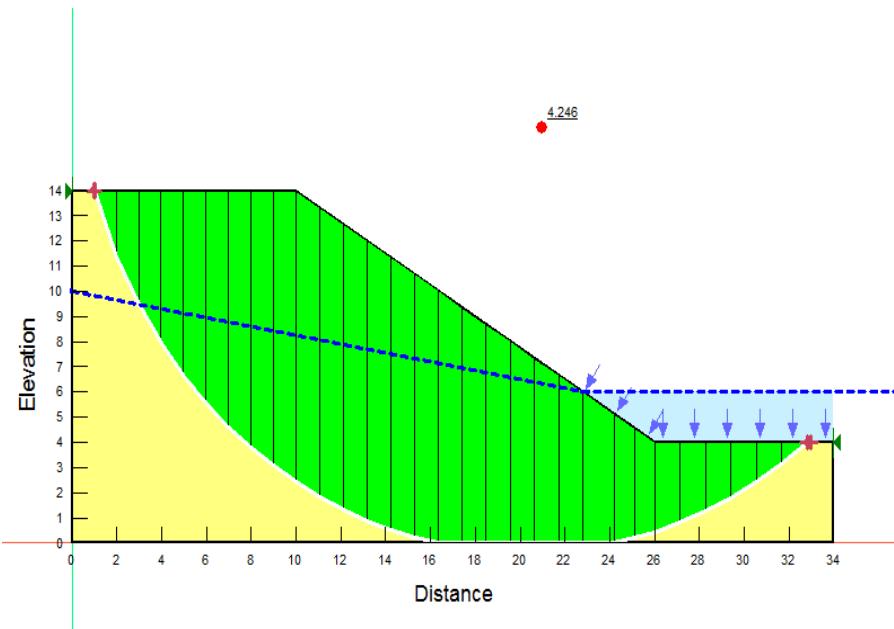


Figure2.8: Factor of safety and slip surface results of Ordinary analysis computed by SLOPE/W

4.3.1. Slope/W analysis on Jammu soil with Morgenstern-Price Method

File Information

File Version: 9.01
Revision Number: 2
Date: 05/03/2020
Time: 04:16:05 PM
Tool Version: 9.1.1.16749
File Name: SWWEP W ON JAMMU SOIL.gsz
Directory: C:\Users\Sys\Documents\
Last Solved Date: 05/03/2020
Last Solved Time: 04:17:56 PM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

SLOPE/W Analysis on Jammu soil

Description: Analysis on Jammu soil
Kind: SLOPE/W
Method: Morgenstern-Price
Settings
Side Function
Interslice force function option: Half-Sine
PWP Conditions from: Piezometric Line
Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Unit Weight of Water: 9.807 kN/m³

Slip Surface
Direction of movement: Left to Right
Use Passive Mode: No
Slip Surface Option: Entry and Exit
Critical slip surfaces saved: 1
Optimize Critical Slip Surface Location: No
Tension Crack Option: (none)

Distribution
F of S Calculation Option: Constant

Advanced
Geometry Settings
Minimum Slip Surface Depth: 0.1 m

Table2.1:Coordinate

| X(m) | Y(m) |
|----------|------|
| 0 | 10 |
| 22.44444 | 7 |

Number of Slices: 30
 Factor of Safety Convergence Settings
 Maximum Number of Iterations: 2,000
 Tolerable difference in F of S: 0.01
 Solution Settings
 Search Method: Root Finder
 Tolerable difference between starting and converged F of S: 3
 Maximum iterations to calculate converged lambda: 20
 Max Absolute Lambda: 2

Materials

Soil layer

Model: Mohr-Coulomb
 Unit Weight: 16.77 kN/m³
 Cohesion': 31.9 kPa
 Phi': 64.6 °
 Phi-B: 0 °
 Pore Water Pressure
 Piezometric Line: 1

Table 2.2: Region

| | Material | Points | Area (m ²) |
|----------|------------|-------------|------------------------|
| Region 1 | Soil Layer | 1,2,3,4,5,6 | 332 |

Slip Surface Entry and Exit

Left Type: Range
 Left-Zone Left Coordinate: (0.7, 14) m
 Left-Zone Right Coordinate: (1, 14) m
 Left-Zone Increment: 8
 Right Type: Point
 Right Coordinate: (33, 5) m
 Right-Zone Increment: 8
 Radius Increments: 4

Table 2.3: Points

| | X(m) | Y(m) |
|---------|------|------|
| Point 1 | 0 | 14 |
| Point 2 | 10 | 14 |
| Point 3 | 26 | 5 |

Slip Surface Limits

Left Coordinate: (0, 14) m
 Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 36 of 45 converged

Current Slip Surface

Slip Surface: 43

Factor of Safety: 6.624
 Volume: 152.26374 m³
 Weight: 2,553.4628 kN
 Resisting Moment: 118,289.4 kN·m
 Activating Moment: 17,853.486 kN·m
 Resisting Force: 4,207.003 kN
 Activating Force: 635.28952 kN
 Slip Rank: 1 of 45 slip surfaces
 Exit: (33, 5) m
 Entry: (1, 14) m
 Radius: 25.087975 m
 Center: (22.087975, 27.590578) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength(kPa) | Base Material |
|----------|-----------|-----------|------------|-------------------------|--------------------------|-------------------------|-----------------------|---------------|
| Slice 1 | 1.4829263 | 13.303515 | -34.341449 | 3.269557 | 6.8856711 | 31.9 | 0 | Soil layer |
| Slice 2 | 2.4487788 | 11.998745 | -22.811645 | 19.206161 | 40.448082 | 31.9 | 0 | Soil layer |
| Slice 3 | 3.4146313 | 10.851723 | -12.828867 | 33.648906 | 70.864431 | 31.9 | 0 | Soil layer |
| Slice 4 | 4.3804838 | 9.8314627 | -4.0892532 | 46.922591 | 98.818747 | 31.9 | 0 | Soil layer |
| Slice 5 | 5.3770691 | 8.8909103 | 3.8283835 | 60.341249 | 119.01582 | 31.9 | 0 | Soil layer |
| Slice 6 | 6.4043871 | 8.0202362 | 11.020438 | 73.717411 | 132.03952 | 31.9 | 0 | Soil layer |
| Slice 7 | 7.431705 | 7.2386843 | 17.338472 | 86.017695 | 144.63811 | 31.9 | 0 | Soil layer |
| Slice 8 | 8.459023 | 6.5362728 | 22.880376 | 97.500744 | 157.15013 | 31.9 | 0 | Soil layer |
| Slice 9 | 9.486341 | 5.9052746 | 27.721928 | 108.36226 | 169.82814 | 31.9 | 0 | Soil layer |
| Slice 10 | 10.518519 | 5.3372041 | 31.93998 | 114.74446 | 174.38582 | 31.9 | 0 | Soil layer |
| Slice 11 | 11.555556 | 4.8277086 | 35.577216 | 116.4667 | 170.35285 | 31.9 | 0 | Soil layer |
| Slice 12 | 12.592593 | 4.375704 | 38.650639 | 117.47305 | 165.99961 | 31.9 | 0 | Soil layer |
| Slice 13 | 13.62963 | 3.9778794 | 41.192719 | 117.7592 | 161.24863 | 31.9 | 0 | Soil layer |
| Slice 14 | 14.666666 | 3.631529 | 43.229991 | 117.29538 | 155.98134 | 31.9 | 0 | Soil layer |
| Slice 15 | 15.703703 | 3.3344427 | 44.78413 | 116.03044 | 150.04437 | 31.9 | 0 | Soil layer |
| Slice 16 | 16.740741 | 3.0848251 | 45.872744 | 113.89605 | 143.25674 | 31.9 | 0 | Soil layer |
| Slice 17 | 17.777777 | 2.8812344 | 46.509972 | 110.81133 | 135.41835 | 31.9 | 0 | Soil layer |
| Slice 18 | 18.814815 | 2.7225381 | 46.70692 | 106.68821 | 126.32031 | 31.9 | 0 | Soil layer |
| Slice 19 | 19.851851 | 2.6078791 | 46.471995 | 101.43761 | 115.75733 | 31.9 | 0 | Soil layer |
| Slice 20 | 20.888889 | 2.5366517 | 45.811136 | 94.976429 | 103.54187 | 31.9 | 0 | Soil layer |
| Slice 21 | 21.925926 | 2.5084853 | 44.727978 | 87.234997 | 89.519574 | 31.9 | 0 | Soil layer |
| Slice 22 | 23.037037 | 2.527575 | 43.861072 | 81.343497 | 78.937804 | 31.9 | 0 | Soil layer |
| Slice 23 | 24.222222 | 2.6006246 | 43.144674 | 77.050117 | 71.404696 | 31.9 | 0 | Soil layer |
| Slice 24 | 25.407407 | 2.7303598 | 41.872361 | 70.870994 | 61.070978 | 31.9 | 0 | Soil layer |
| Slice 25 | 26.5 | 2.8988272 | 40.220202 | 63.686468 | 49.41984 | 31.9 | 0 | Soil layer |
| Slice 26 | 27.5 | 3.0986552 | 38.260489 | 60.120722 | 46.037543 | 31.9 | 0 | Soil layer |
| Slice 27 | 28.5 | 3.341352 | 35.880361 | 55.468362 | 41.252235 | 31.9 | 0 | Soil layer |
| Slice 28 | 29.5 | 3.6282227 | 33.06702 | 49.754789 | 35.14436 | 31.9 | 0 | Soil layer |

| | | | | | | | | |
|----------|------|-----------|-----------|-----------|-----------|------|---|------------|
| Slice 29 | 30.5 | 3.9608794 | 29.804656 | 43.02823 | 27.848782 | 31.9 | 0 | Soil layer |
| Slice 30 | 31.5 | 4.3412916 | 26.073953 | 35.356144 | 19.548249 | 31.9 | 0 | Soil layer |
| Slice 31 | 32.5 | 4.7718535 | 21.851433 | 26.819758 | 10.463269 | 31.9 | 0 | Soil layer |

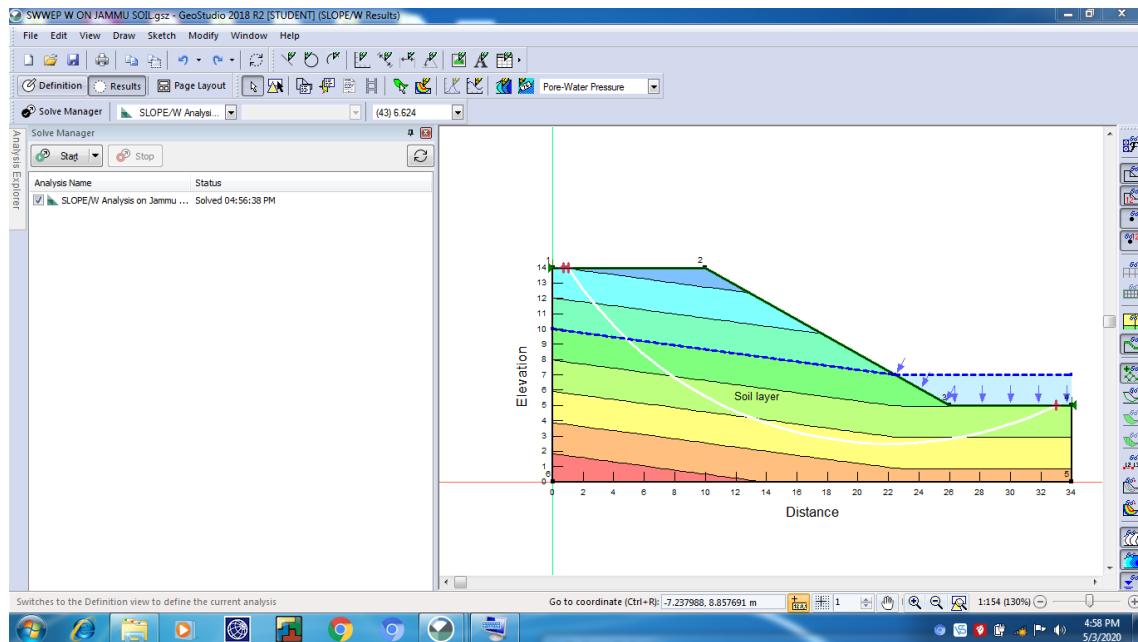


Figure3.1: Slope/W Analysis (Jammu Region Soil)

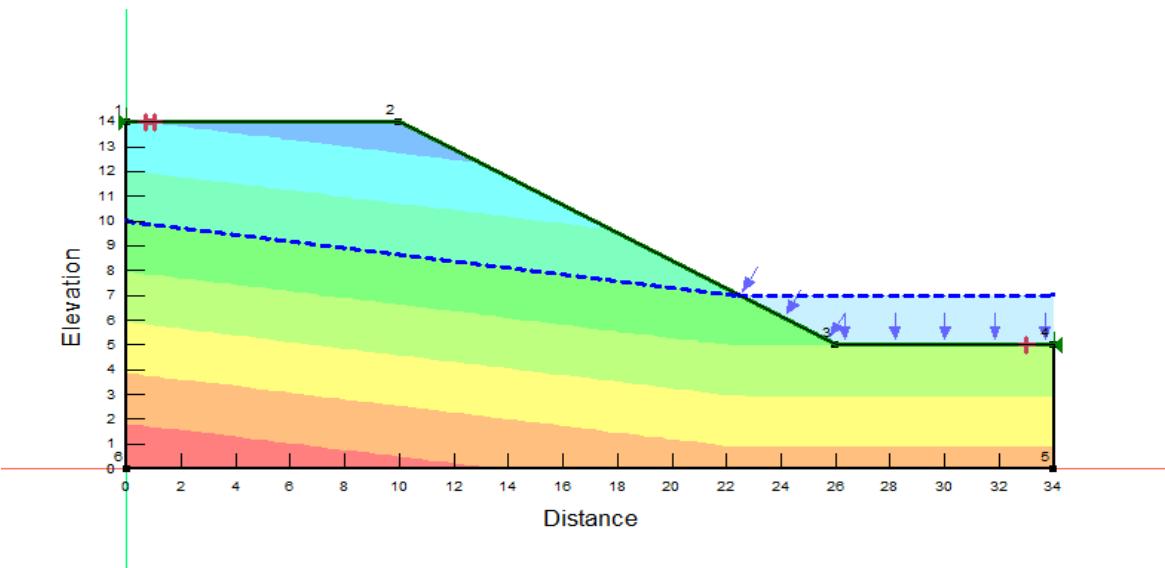


Figure3.2: Pore Pressure From Piezometric line (Jammu Region Sample Slope/W Analysis with Morgenstern–Price Method)

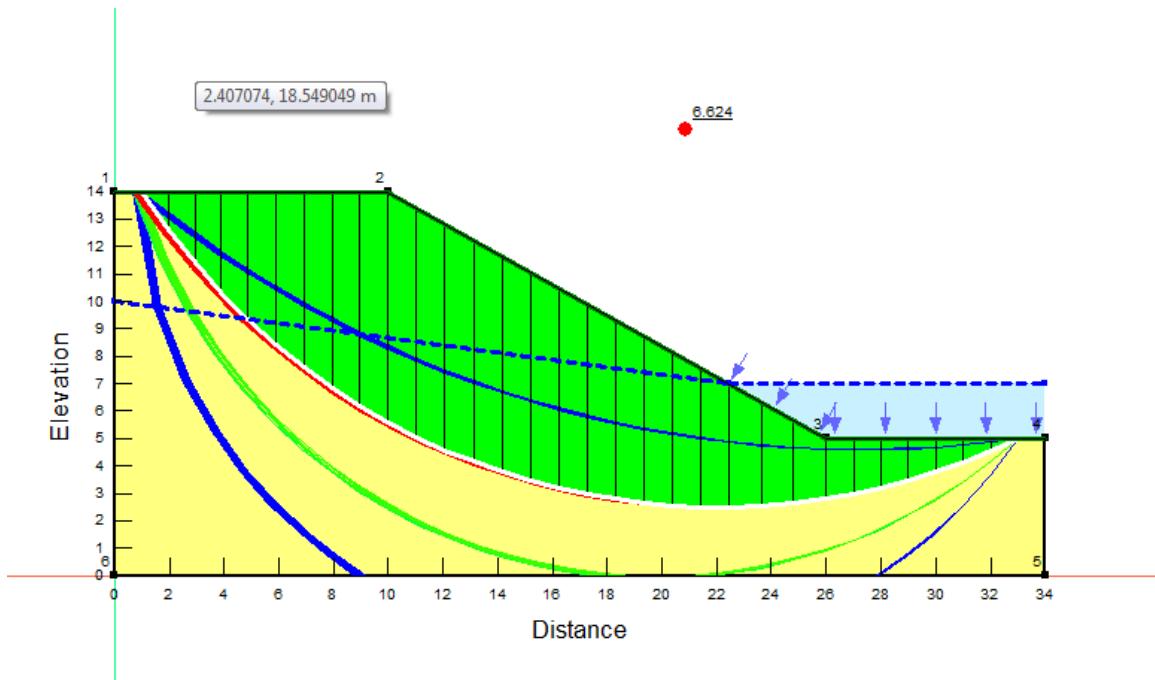


Figure3.3: Factor of safety and slip surface results of Morgenstern-Price analysis computed by SLOPE/W

4.3.2. Slope/W analysis of Jammu soil with Bishop Method

File Information

File Version: 9.01
 Revision Number: 1
 Date: 06/21/2020
 Time: 03:28:50 PM
 Tool Version: 9.1.1.16749
 File Name: SLOPE W JAMMU SOIL BISHOP.gsz
 Directory: C:\Users\Sys\Desktop\Major project content\Geoslope Jammu soil content\
 Last Solved Date: 06/21/2020
 Last Solved Time: 03:28:52 PM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

SLOPE W JAMMU SOIL BISHOP

Kind: [SLOPE/W](#)

Method: [Bishop](#)

Settings

PWP Conditions from: [Piezometric Line](#)

Apply Phreatic Correction: [Yes](#)

Use Staged Rapid Drawdown: [No](#)

Unit Weight of Water: [9.807 kN/m³](#)

Slip Surface

Direction of movement: [Left to Right](#)

Use Passive Mode: [No](#)

Slip Surface Option: [Entry and Exit](#)

Critical slip surfaces saved: [1](#)

Optimize Critical Slip Surface Location: [No](#)

Tension Crack Option: [\(none\)](#)

Distribution

F of S Calculation Option: [Constant](#)

Advanced

Geometry Settings

Minimum Slip Surface Depth: [0.1 m](#)

Number of Slices: [30](#)

Factor of Safety Convergence Settings

Maximum Number of Iterations: [2,000](#)

Tolerable difference in F of S: [0.01](#)

Materials

Soil layer

Model: [Mohr-Coulomb](#)

Unit Weight: [16.77 kN/m³](#)

Cohesion': [31.9 kPa](#)

Phi': [64.6 °](#)

Phi-B: [0 °](#)

Pore Water Pressure

Piezometric Line: [1](#)

Slip Surface Entry and Exit

Left Type: [Range](#)

Left-Zone Left Coordinate: [\(0.7, 14\) m](#)

Left-Zone Right Coordinate: [\(1, 14\) m](#)

Left-Zone Increment: [8](#)

Right Type: [Point](#)

Right Coordinate: [\(33, 5\) m](#)

Right-Zone Increment: 8

Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 36 of 45 converged

Current Slip Surface

Slip Surface: 43

Factor of Safety: 6.644

Volume: 152.26374 m³

Weight: 2,553.4628 kN

Resisting Moment: 118,612.49 kN·m

Activating Moment: 17,853.486 kN·m

Slip Rank: 1 of 45 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 25.087975 m

Center: (22.087975, 27.590578) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength (kPa) | Cohesive Strength (kPa) | Suction Strength (kPa) | Base Material |
|----------|-----------|-----------|------------|-------------------------|---------------------------|-------------------------|------------------------|---------------|
| Slice 1 | 1.4829265 | 13.303515 | -33.738677 | 3.2672189 | 6.880747 | 31.9 | 0 | Soil layer |
| Slice 2 | 2.4487794 | 11.998745 | -22.411246 | 19.669122 | 41.423076 | 31.9 | 0 | Soil layer |
| Slice 3 | 3.4146323 | 10.851721 | -12.603689 | 35.055648 | 73.827023 | 31.9 | 0 | Soil layer |
| Slice 4 | 4.3804852 | 9.8314613 | -4.0174768 | 49.490282 | 104.22629 | 31.9 | 0 | Soil layer |
| Slice 5 | 5.3770705 | 8.890909 | 3.7611832 | 64.263974 | 127.41858 | 31.9 | 0 | Soil layer |
| Slice 6 | 6.4043882 | 8.0202353 | 10.826994 | 79.102653 | 143.7882 | 31.9 | 0 | Soil layer |
| Slice 7 | 7.4317058 | 7.2386837 | 17.034126 | 92.676067 | 159.30156 | 31.9 | 0 | Soil layer |
| Slice 8 | 8.4590235 | 6.5362725 | 22.478752 | 105.11545 | 174.03248 | 31.9 | 0 | Soil layer |
| Slice 9 | 9.4863412 | 5.9052745 | 27.235319 | 116.52371 | 188.0409 | 31.9 | 0 | Soil layer |
| Slice 10 | 10.518517 | 5.337205 | 31.379324 | 122.82839 | 192.59128 | 31.9 | 0 | Soil layer |
| Slice 11 | 11.55555 | 4.8277111 | 34.952705 | 123.88965 | 187.30077 | 31.9 | 0 | Soil layer |
| Slice 12 | 12.592583 | 4.3757077 | 37.972173 | 123.85315 | 180.86491 | 31.9 | 0 | Soil layer |
| Slice 13 | 13.629617 | 3.9778839 | 40.469627 | 122.7741 | 173.33282 | 31.9 | 0 | Soil layer |
| Slice 14 | 14.66665 | 3.6315341 | 42.471137 | 120.69624 | 164.74168 | 31.9 | 0 | Soil layer |
| Slice 15 | 15.703683 | 3.334448 | 43.997997 | 117.6536 | 155.11848 | 31.9 | 0 | Soil layer |
| Slice 16 | 16.740717 | 3.0848302 | 45.067507 | 113.67227 | 144.4813 | 31.9 | 0 | Soil layer |
| Slice 17 | 17.77775 | 2.8812391 | 45.693556 | 108.77065 | 132.84005 | 31.9 | 0 | Soil layer |
| Slice 18 | 18.814783 | 2.7225422 | 45.887056 | 102.96077 | 120.19696 | 31.9 | 0 | Soil layer |

| | | | | | | | | |
|----------|-----------|-----------|-----------|-----------|-----------|------|---|------------|
| Slice 19 | 19.851817 | 2.6078822 | 45.656266 | 96.248416 | 106.54682 | 31.9 | 0 | Soil layer |
| Slice 20 | 20.88885 | 2.5366535 | 45.007021 | 88.633343 | 91.876822 | 31.9 | 0 | Soil layer |
| Slice 21 | 21.925883 | 2.5084855 | 43.94289 | 80.109303 | 76.166284 | 31.9 | 0 | Soil layer |
| Slice 22 | 23.037015 | 2.5275747 | 43.861075 | 73.215461 | 61.820193 | 31.9 | 0 | Soil layer |
| Slice 23 | 24.222222 | 2.6006247 | 43.144674 | 67.893884 | 52.121716 | 31.9 | 0 | Soil layer |
| Slice 24 | 25.407407 | 2.7303598 | 41.872361 | 61.466321 | 41.264784 | 31.9 | 0 | Soil layer |
| Slice 25 | 26.5 m | 2.8988272 | 40.220202 | 56.637302 | 34.574332 | 31.9 | 0 | Soil layer |
| Slice 26 | 27.5 | 3.0986552 | 38.260489 | 53.636112 | 32.380986 | 31.9 | 0 | Soil layer |
| Slice 27 | 28.5 | 3.341352 | 35.880361 | 49.870116 | 29.462357 | 31.9 | 0 | Soil layer |
| Slice 28 | 29.5 | 3.6282227 | 33.06702 | 45.301728 | 25.766235 | 31.9 | 0 | Soil layer |
| Slice 29 | 30.5 | 3.9608794 | 29.804656 | 39.884974 | 21.229101 | 31.9 | 0 | Soil layer |
| Slice 30 | 31.5 | 4.3412916 | 26.073953 | 33.563498 | 15.772945 | 31.9 | 0 | Soil layer |
| Slice 31 | 32.5 | 4.7718535 | 21.851433 | 26.267795 | 9.3008366 | 31.9 | 0 | Soil layer |

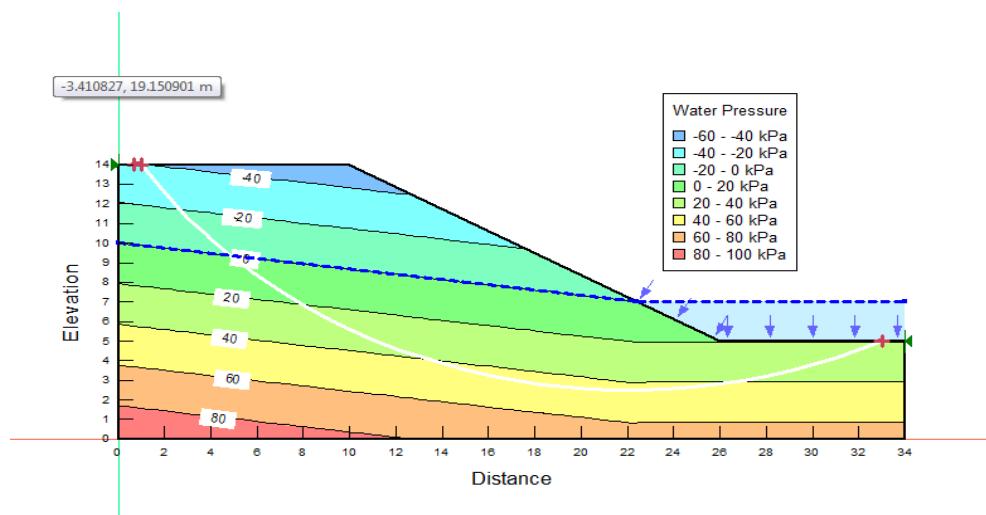


Figure3.4 : Pore Pressure From Piezometric line (Jammu Region Sample Slope/W Analysis with Bishop Method)

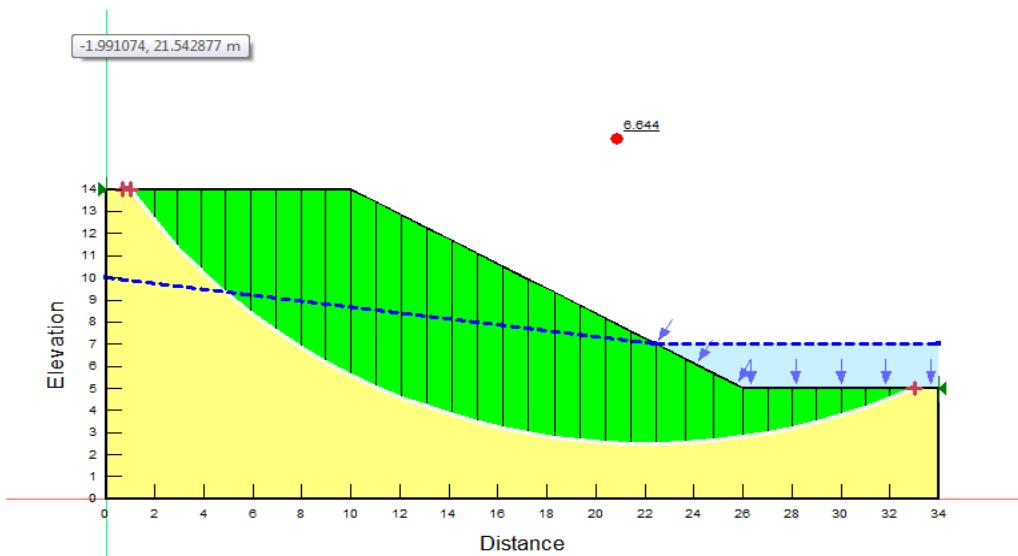


Figure3.5 : Factor of safety and slip surface results of Bishop analysis computed by SLOPE/W

4.3.3. Slope/W analysis of Jammu soil with Janbu Method

File Information

File Version: [9.01](#)
 Revision Number: [1](#)
 Date: [06/21/2020](#)
 Time: [05:44:59 PM](#)
 Tool Version: [9.1.1.16749](#)
 File Name: [SLOPE W JAMMU SOIL JANBU.gsz](#)
 Directory: [C:\Users\Sys\Desktop\Major project content\Geoslope Jammu soil content\](#)
 Last Solved Date: [06/21/2020](#)
 Last Solved Time: [05:45:02 PM](#)

Project Settings

Unit System: [International System of Units \(SI\)](#)

Analysis Settings

SLOPE W JAMMU SOIL JANBU

Kind: [SLOPE/W](#)
 Method: [Janbu](#)
 Settings
 PWP Conditions from: [Piezometric Line](#)
 Apply Phreatic Correction: [Yes](#)

Use Staged Rapid Drawdown: No
Unit Weight of Water: 9.807 kN/m³
Slip Surface
 Direction of movement: Left to Right
 Use Passive Mode: No
 Slip Surface Option: Entry and Exit
 Critical slip surfaces saved: 1
 Optimize Critical Slip Surface Location: No
 Tension Crack Option: (none)
Distribution
 F of S Calculation Option: Constant
Advanced
 Geometry Settings
 Minimum Slip Surface Depth: 0.1 m
 Number of Slices: 30
 Factor of Safety Convergence Settings
 Maximum Number of Iterations: 2,000
 Tolerable difference in F of S: 0.01

Materials

SOIL LAYER

Model: Mohr-Coulomb
Unit Weight: 16.77 kN/m³
Cohesion': 31.9 kPa
Phi': 64.6 °
Phi-B: 0 °
Pore Water Pressure
 Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range
Left-Zone Left Coordinate: (0.7, 14) m
Left-Zone Right Coordinate: (1, 14) m
Left-Zone Increment: 4
Right Type: Point
Right Coordinate: (33, 5) m
Right-Zone Increment: 8
Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m
Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 24

Factor of Safety: 6.146

Volume: 222.64535 m³

Weight: 3,733.7625 kN

Resisting Force: 5,211.6342 kN

Activating Force: 847.9557 kN

Slip Rank: 1 of 25 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 19.695433 m

Center: (19.860951, 19.672269) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength(kPa) | Base Material |
|----------|-----------|------------|------------|-------------------------|--------------------------|-------------------------|-----------------------|---------------|
| Slice 1 | 1.4827338 | 12.723295 | -28.148091 | 4.0378123 | 8.5036129 | 31.9 | 0 | SOIL LAYER |
| Slice 2 | 2.4482014 | 10.527416 | -8.2344483 | 29.274749 | 61.652479 | 31.9 | 0 | SOIL LAYER |
| Slice 3 | 3.4358683 | 8.8424331 | 6.7281822 | 54.052213 | 99.664178 | 31.9 | 0 | SOIL LAYER |
| Slice 4 | 4.4457348 | 7.4402892 | 18.937111 | 77.989846 | 124.36477 | 31.9 | 0 | SOIL LAYER |
| Slice 5 | 5.4556012 | 6.2615695 | 28.993377 | 98.601895 | 146.5952 | 31.9 | 0 | SOIL LAYER |
| Slice 6 | 6.4654676 | 5.2501951 | 37.437295 | 116.70791 | 166.94353 | 31.9 | 0 | SOIL LAYER |
| Slice 7 | 7.475334 | 4.372447 | 44.593741 | 132.80581 | 185.77418 | 31.9 | 0 | SOIL LAYER |
| Slice 8 | 8.4852004 | 3.6061675 | 50.676203 | 147.22586 | 203.33311 | 31.9 | 0 | SOIL LAYER |
| Slice 9 | 9.4950668 | 2.9359079 | 55.833525 | 160.20043 | 219.79619 | 31.9 | 0 | SOIL LAYER |
| Slice 10 | 10.556625 | 2.3246277 | 60.356019 | 167.99678 | 226.69091 | 31.9 | 0 | SOIL LAYER |
| Slice 11 | 11.669876 | 1.7713842 | 64.252767 | 170.32965 | 223.3974 | 31.9 | 0 | SOIL LAYER |
| Slice 12 | 12.783126 | 1.302221 | 67.339412 | 171.01342 | 218.33695 | 31.9 | 0 | SOIL LAYER |
| Slice 13 | 13.896377 | 0.91079783 | 69.677042 | 170.16408 | 211.62521 | 31.9 | 0 | SOIL LAYER |
| Slice 14 | 15.009627 | 0.59230863 | 71.311964 | 167.86623 | 203.34281 | 31.9 | 0 | SOIL LAYER |
| Slice 15 | 16.122877 | 0.34313347 | 72.279055 | 164.17967 | 193.54225 | 31.9 | 0 | SOIL LAYER |
| Slice 16 | 17.236128 | 0.1606069 | 72.603995 | 159.14364 | 182.25206 | 31.9 | 0 | SOIL LAYER |
| Slice 17 | 18.349378 | 0.04286321 | 72.304761 | 152.77932 | 169.47903 | 31.9 | 0 | SOIL LAYER |
| Slice 18 | 19.383477 | 0 | 71.385998 | 146.26449 | 157.69373 | 31.9 | 0 | SOIL LAYER |
| Slice 19 | 20.338424 | 0 | 70.156187 | 137.25635 | 141.31262 | 31.9 | 0 | SOIL LAYER |
| Slice 20 | 21.223023 | 0.02822915 | 68.744989 | 130.25836 | 129.54686 | 31.9 | 0 | SOIL LAYER |
| Slice 21 | 22.037274 | 0.10173232 | 66.988179 | 122.20389 | 116.28402 | 31.9 | 0 | SOIL LAYER |
| Slice 22 | 23.037015 | 0.24388432 | 66.257226 | 114.52882 | 101.65974 | 31.9 | 0 | SOIL LAYER |
| Slice 23 | 24.222222 | 0.47539134 | 63.986837 | 106.97694 | 90.53695 | 31.9 | 0 | SOIL LAYER |

| | | | | | | | | |
|----------|-----------|------------|-----------|-------------|-----------|------|---|------------|
| Slice 24 | 25.407407 | 0.78403287 | 60.95999 | 97.870707 | 77.73379 | 31.9 | 0 | SOIL LAYER |
| Slice 25 | 26.5 | 1.137139 | 57.497077 | 90.271191 | 69.022122 | 31.9 | 0 | SOIL LAYER |
| Slice 26 | 27.5 | 1.5267266 | 53.676393 | 84.484888 k | 64.88254 | 31.9 | 0 | SOIL LAYER |
| Slice 27 | 28.5 | 1.9813871 | 49.217537 | 77.497049 | 59.556515 | 31.9 | 0 | SOIL LAYER |
| Slice 28 | 29.5 | 2.5063145 | 44.069574 | 69.17127 | 52.864049 | 31.9 | 0 | SOIL LAYER |
| Slice 29 | 30.5 | 3.108224 | 38.166647 | 59.322701 | 44.554545 | 31.9 | 0 | SOIL LAYER |
| Slice 30 | 31.5 | 3.7959261 | 31.422353 | 47.6922 | 34.264219 | 31.9 | 0 | SOIL LAYER |
| Slice 31 | 32.5 | 4.5812397 | 23.720783 | 33.898778 | 21.434809 | 31.9 | 0 | SOIL LAYER |

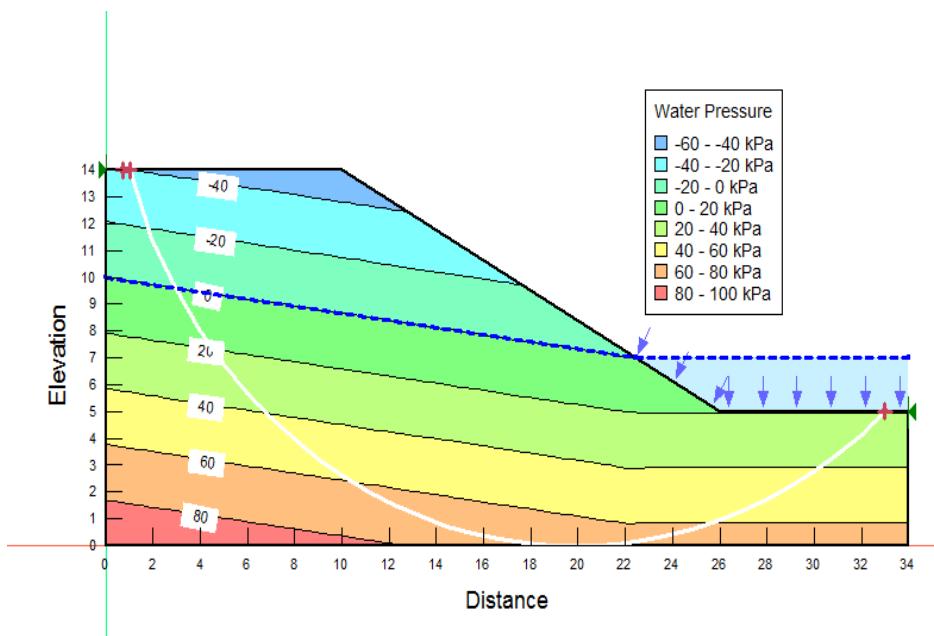


Figure3.6: Pore Pressure From Piezometric line (Jammu Region Sample Slope/W Analysis with Janbu Method)

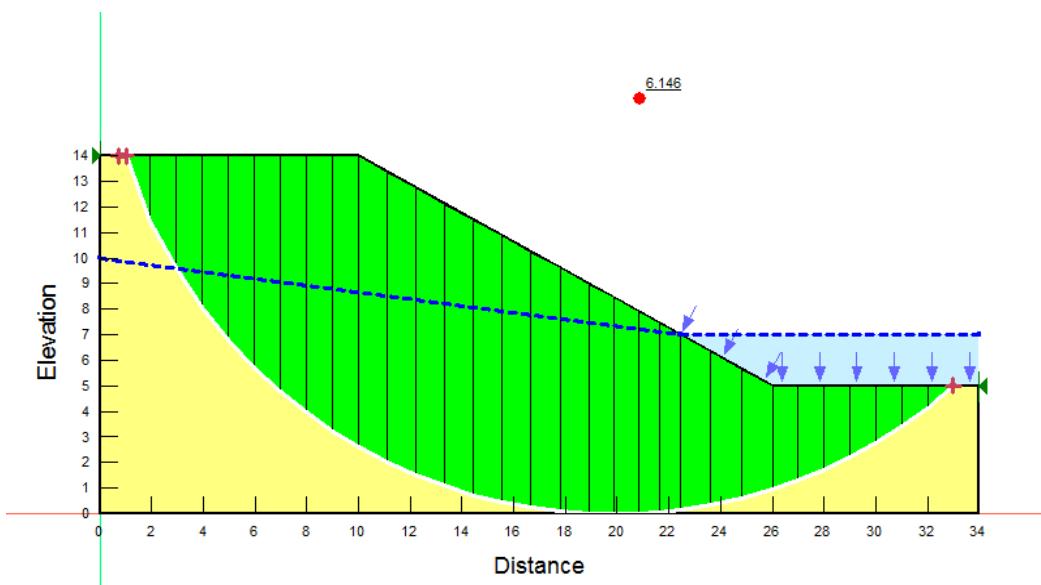


Figure3.7: Factor of safety and slip surface results of Janbu analysis computed by SLOPE/W

4.3.4. Slope/W analysis of Jammu soil with Ordinary Method

File Information

File Version: [9.01](#)
 Revision Number: [1](#)
 Date: [06/21/2020](#)
 Time: [05:58:16 PM](#)
 Tool Version: [9.1.1.16749](#)
 File Name: [SLOPE W JAMMU SOIL ORDINARY.gsz](#)
 Directory: [C:\Users\Sys\Desktop\Major project content\Geoslope Jammu soil content\](#)
 Last Solved Date: [06/21/2020](#)
 Last Solved Time: [05:58:18 PM](#)

Project Settings

Unit System: [International System of Units \(SI\)](#)

Analysis Settings

SLOPE W JAMMU SOIL ORDINARY

Kind: [SLOPE/W](#)
 Method: [Ordinary](#)
 Settings
 PWP Conditions from: [Piezometric Line](#)

Apply Phreatic Correction: Yes
Use Staged Rapid Drawdown: No
Unit Weight of Water: 9.807 kN/m³

Slip Surface
Direction of movement: Left to Right
Use Passive Mode: No
Slip Surface Option: Entry and Exit
Critical slip surfaces saved: 1
Optimize Critical Slip Surface Location: No
Tension Crack Option: (none)

Distribution
F of S Calculation Option: Constant

Advanced
Geometry Settings
Minimum Slip Surface Depth: 0.1 m
Number of Slices: 30

Factor of Safety Convergence Settings
Maximum Number of Iterations: 2,000
Tolerable difference in F of S: 0.01

Materials

SOIL LAYER

Model: Mohr-Coulomb
Unit Weight: 16.77 kN/m³
Cohesion': 31.9 kPa
Phi': 64.6 °
Phi-B: 0 °
Pore Water Pressure
Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range
Left-Zone Left Coordinate: (0.7, 14) m
Left-Zone Right Coordinate: (1, 14) m
Left-Zone Increment: 4
Right Type: Point
Right Coordinate: (33, 5) m
Right-Zone Increment: 4
Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m
Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 24

Factor of Safety: 6.149

Volume: 222.64535 m³

Weight: 3,733.7625 kN

Resisting Moment: 106,100.49 kN·m

Activating Moment: 17,254.774 kN·m

Slip Rank: 1 of 25 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 19.695433 m

Center: (19.860951, 19.672269) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength(kPa) | Suction Strength(kPa) | Base Material |
|----------|-----------|-----------------|------------|-------------------------|--------------------------|------------------------|-----------------------|---------------|
| Slice 1 | 1.4827338 | 12.723295 | -28.148091 | 2.678086 | 5.6400359 | 31. | 0 | SOIL LAYER |
| Slice 2 | 2.4482014 | 10.527416 | -8.2344483 | 12.58974 | 26.51393 | 31.9 | 0 | SOIL LAYER |
| Slice 3 | 3.4358683 | 8.8424331 | 6.7281822 | 30.897469 | 50.900399 | 31.9 | 0 | SOIL LAYER |
| Slice 4 | 4.4457348 | 7.4402892 | 18.937111 | 54.123408 | 74.102169 | 31.9 | 0 | SOIL LAYER |
| Slice 5 | 5.4556012 | 6.2615695 | 28.993377 | 75.784323 | 98.541502 | 31.9 | 0 | SOIL LAYER |
| Slice 6 | 6.4654676 | 5.2501951 | 37.437295 | 96.113816 | 123.57247 | 31.9 | 0 | SOIL LAYER |
| Slice 7 | 7.475334 | 4.372447 | 44.593741 | 115.18997 | 148.67532 | 31.9 | 0 | SOIL LAYER |
| Slice 8 | 8.4852004 | 3.6061675 | 50.676203 | 133.02113 | 173.41801 | 31.9 | 0 | SOIL LAYER |
| Slice 9 | 9.4950668 | 2.9359079 | 55.833525 | 149.58194 | 197.4337 | 31.9 | 0 | SOIL LAYER |
| Slice 10 | 10.556625 | 2.3246277 | 60.356019 | 161.46084 | 212.92625 | 31.9 | 0 | SOIL LAYER |
| Slice 11 | 11.669876 | 1.7713842 | 64.252767 | 167.66864 | 217.79333 | 31.9 | 0 | SOIL LAYER |
| Slice 12 | 12.783126 | 1.302221 | 67.339412 | 171.26105 | 218.85847 | 31.9 | 0 | SOIL LAYER |
| Slice 13 | 13.896377 | 0.91079783 | 69.677042 | 172.37152 | 216.27406 | 31.9 | 0 | SOIL LAYER |
| Slice 14 | 15.009627 | 0.59230863 | 71.311964 | 171.13691 | 210.23084 | 31.9 | 0 | SOIL LAYER |
| Slice 15 | 16.122877 | 0.34313347 | 72.279055 | 167.69908 | 200.95411 | 31.9 | 0 | SOIL LAYER |
| Slice 16 | 17.236128 | 0.1606069 | 72.603995 | 162.20578 | 188.70093 | 31.9 | 0 | SOIL LAYER |
| Slice 17 | 18.349378 | 0.04286321 | 72.304761 | 154.8112 | 173.75817 | 31.9 | 0 | SOIL LAYER |
| Slice 18 | 19.383477 | 0 | 71.385998 | 146.26449 | 157.69373 | 31.9 | 0 | SOIL LAYER |
| Slice 19 | 20.338424 | 0 | 70.156187 | 137.25635 | 141.31262 | 31.9 | 0 | SOIL LAYER |
| Slice 20 | 21.223023 | 0.02822915 1 | 68.744989 | 128.1528 | 125.11255 | 31.9 | 0 | SOIL LAYER |
| Slice 21 | 22.037274 | 0.10173232 | 66.988179 | 118.88308 | 109.29042 | 31.9 | 0 | SOIL LAYER |
| Slice 22 | 23.037015 | 0.24388432 | 66.257226 | 109.52233 | 91.116099 | 31.9 | 0 | SOIL LAYER |
| Slice 23 | 24.222222 | 0.47539134 | 63.986837 | 99.374917 | 74.527123 | 31.9 | 0 | SOIL LAYER |
| Slice 24 | 25.407407 | 0.78403287 | 60.95999 | 87.636689 | 56.180999 | 31.9 | 0 | SOIL LAYER |
| Slice 25 | 26.5 | 1.137139 | 57.497077 | 81.335723 | 50.204072 | 31.9 | 0 | SOIL LAYER |
| Slice 26 | 27.5 | 1.5267266 | 53.676393 | 74.219864 | 43.26445 | 31.9 | 0 | SOIL LAYER |

| | | | | | | | | |
|----------|------|-----------|-----------|-----------|-----------|------|---|------------|
| Slice 27 | 28.5 | 1.9813871 | 49.217537 | 66.188969 | 35.741753 | 31.9 | 0 | SOIL LAYER |
| Slice 28 | 29.5 | 2.5063145 | 44.069574 | 57.270708 | 27.801523 | 31.9 | 0 | SOIL LAYER |
| Slice 29 | 30.5 | 3.108224 | 38.166647 | 47.491959 | 19.639062 | 31.9 | 0 | SOIL LAYER |
| Slice 30 | 31.5 | 3.7959261 | 31.422353 | 36.875534 | 11.484373 | 31.9 | 0 | SOIL LAYER |
| Slice 31 | 32.5 | 4.5812397 | 23.720783 | 25.434523 | 3.6091292 | 31.9 | 0 | SOIL LAYER |

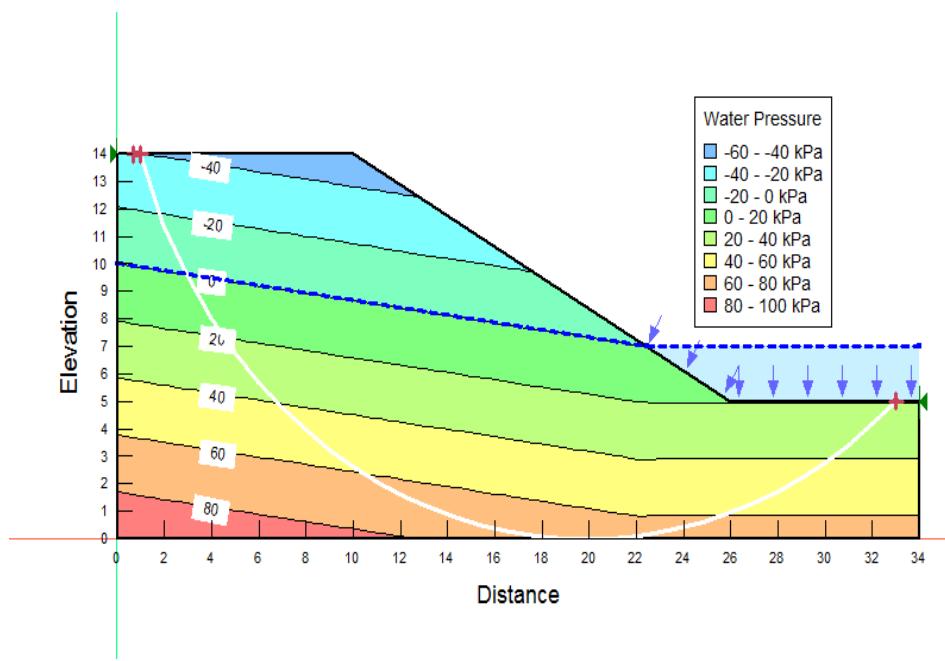


Figure3.8: Pore Pressure From Piezometric line (Jammu Region Sample Slope/W Analysis with Ordinary Method)

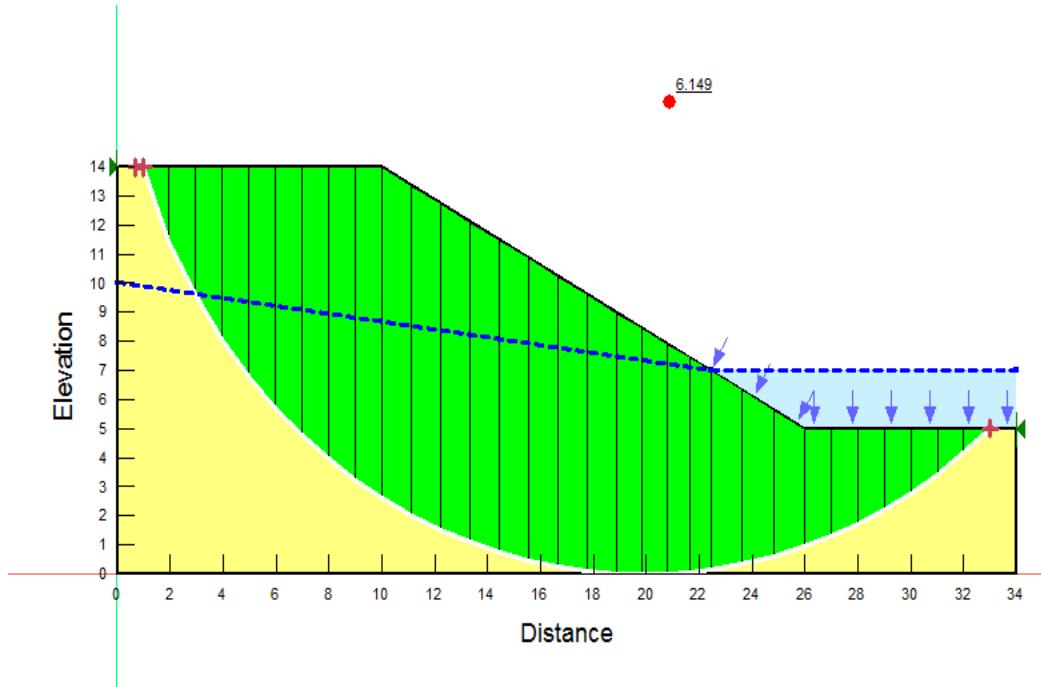


Figure3.9: Factor of safety and slip surface results of Ordinary analysis computed by SLOPE/W

4.4.1. Slope/W Analysis of Punjab Soil with Morgenstern-Price Method

File Information

File Version: 9.01
 Revision Number: 1
 Date: 05/03/2020
 Time: 06:12:38 PM
 Tool Version: 9.1.1.16749
 File Name: SLOPE W PUNJAB SOIL.gsz
 Directory: C:\Users\Sys\Desktop\PROJECT\GEOSLOPE Jammu soil content\
 Last Solved Date: 05/03/2020
 Last Solved Time: 06:12:40 PM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

SLOPE/W Analysis Punjab soil

Kind: SLOPE/W

Method: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No

Use Staged Rapid Drawdown: No

Unit Weight of Water: 9.807 kN/m³

Slip Surface

Direction of movement: Left to Right

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

Geometry Settings

Minimum Slip Surface Depth: 0.1 m

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 2,000

Tolerable difference in F of S: 0.01

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

Piezometric Line 1

Table3.1:Co ordinates

| X(m) | Y(m) |
|---------|-------|
| 0 | 10 |
| 22.4444 | 7 |

Materials

Soil Layer

Model: Mohr-Coulomb

Unit Weight: 18.24 kN/m³

Cohesion': 53 kPa

Phi': 36.86 °

Phi-B: 0 °

Pore Water Pressure

Piezometric Line: 1

Table 3.2: Region

| | Material | Points | Area (m ²) |
|----------|------------|-------------|------------------------|
| Region 1 | Soil Layer | 1,2,3,4,5,6 | 327.5 |

Table3.3 : Points

| | X(m) | Y(m) |
|---------|------|------|
| Point 1 | 0 | 14 |
| Point 2 | 9 | 14 |
| Point 3 | 26 | 5 |

Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (0.7, 14) m

Left-Zone Right Coordinate: (1, 14) m

Left-Zone Increment: 4
 Right Type: Point
 Right Coordinate: (33, 5) m
 Right-Zone Increment: 8
 Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m
 Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 24
 Factor of Safety: 4.309
 Volume: 218.13941 m³
 Weight: 3,978.8628 kN
 Resisting Moment: 79,816.887 kN·m
 Activating Moment: 18,514.155 kN·m
 Resisting Force: 3,407.927 kN
 Activating Force: 791.22266 kN
 Slip Rank: 1 of 25 slip surfaces
 Exit: (33, 5) m
 Entry: (1, 14) m
 Radius: 19.695433 m
 Center: (19.860951, 19.672269) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength (kPa) | Base Material |
|---------|-----------|-----------|------------|-------------------------|--------------------------|-------------------------|------------------------|---------------|
| Slice 1 | 1.4827337 | 12.723296 | -28.650983 | -5.9959873 | -4.4953723 | 53 | 0 | Soil Layer |
| Slice 2 | 2.448201 | 10.527416 | -8.3815647 | 29.361563 | 22.013248 | 53 | 0 | Soil Layer |
| Slice 3 | 3.4366901 | 8.8413051 | 6.8583811 | 58.245411 | 38.526404 | 53 | 0 | Soil Layer |
| Slice 4 | 4.448201 | 7.4372561 | 19.301963 | 83.276994 | 47.964007 | 53 | 0 | Soil Layer |
| Slice 5 | 5.4597119 | 6.2572085 | 29.548764 | 104.13839 | 55.922088 | 53 | 0 | Soil Layer |
| Slice 6 | 6.4712228 | 5.2448932 | 38.150615 | 122.20151 | 63.01549 | 53 | 0 | Soil Layer |
| Slice 7 | 7.4827337 | 4.3664939 | 45.439151 | 138.28675 | 69.610638 | 53 | 0 | Soil Layer |
| Slice 8 | 8.4942446 | 3.5997968 | 51.632224 | 152.92595 | 75.942961 | 53 | 0 | Soil Layer |
| Slice 9 | 9.5503335 | 2.9037302 | 57.074188 | 162.4802 | 79.026062 | 53 | 0 | Soil Layer |

| | | | | | | | | |
|----------|-----------|-------------|-----------|-----------|-----------|----|---|------------|
| Slice 10 | 10.651001 | 2.274017 | 61.806991 | 166.90659 | 78.796336 | 53 | 0 | Soil Layer |
| Slice 11 | 11.751668 | 1.7339062 | 65.661062 | 170.1956 | 78.372692 | 53 | 0 | Soil Layer |
| Slice 12 | 12.852335 | 1.2754603 | 68.714246 | 172.42573 | 77.755624 | 53 | 0 | Soil Layer |
| Slice 13 | 13.953002 | 0.89266864 | 71.025489 | 173.61224 | 76.912376 | 53 | 0 | Soil Layer |
| Slice 14 | 15.053669 | 0.58096045 | 72.639616 | 173.72067 | 75.783508 | 53 | 0 | Soil Layer |
| Slice 15 | 16.154336 | 0.33688431 | 73.590476 | 172.67698 | 74.288135 | 53 | 0 | Soil Layer |
| Slice 16 | 17.255003 | 0.15789328 | 73.903046 | 170.37615 | 72.32879 | 53 | 0 | Soil Layer |
| Slice 17 | 18.35567 | 0.042200896 | 73.594846 | 166.69036 | 69.796512 | 53 | 0 | Soil Layer |
| Slice 18 | 19.383477 | 0 | 72.661423 | 163.10021 | 67.804679 | 53 | 0 | Soil Layer |
| Slice 19 | 20.338424 | 0 | 71.409643 | 154.56429 | 62.343544 | 53 | 0 | Soil Layer |
| Slice 20 | 21.481533 | 0.054988094 | 69.371945 | 147.33055 | 58.447913 | 53 | 0 | Soil Layer |
| Slice 21 | 22.295804 | 0.12849391 | 67.583697 | 140.78341 | 54.880029 | 53 | 0 | Soil Layer |
| Slice 22 | 23.037033 | 0.24388668 | 66.257203 | 137.0837 | 53.100754 | 53 | 0 | Soil Layer |
| Slice 23 | 24.22222 | 0.47539086 | 63.986842 | 129.87869 | 49.401099 | 53 | 0 | Soil Layer |
| Slice 24 | 25.407407 | 0.78403268 | 60.959991 | 120.13589 | 44.365952 | 53 | 0 | Soil Layer |
| Slice 25 | 26.5 | 1.137139 | 57.497077 | 110.04396 | 39.395978 | 53 | 0 | Soil Layer |
| Slice 26 | 27.5 | 1.5267266 | 53.676393 | 102.87576 | 36.88625 | 53 | 0 | Soil Layer |
| Slice 27 | 28.5 | 1.9813871 | 49.217537 | 93.966656 | 33.549762 | 53 | 0 | Soil Layer |
| Slice 28 | 29.5 | 2.5063145 | 44.069574 | 83.304288 | 29.415447 | 53 | 0 | Soil Layer |
| Slice 29 | 30.5 | 3.108224 | 38.166647 | 70.896462 | 24.538528 | 53 | 0 | Soil Layer |
| Slice 30 | 31.5 | 3.7959261 | 31.422353 | 56.765437 | 19.000474 | 53 | 0 | Soil Layer |
| Slice 31 | 32.5 | 4.5812397 | 23.720783 | 40.939339 | 12.90927 | 53 | 0 | Soil Layer |

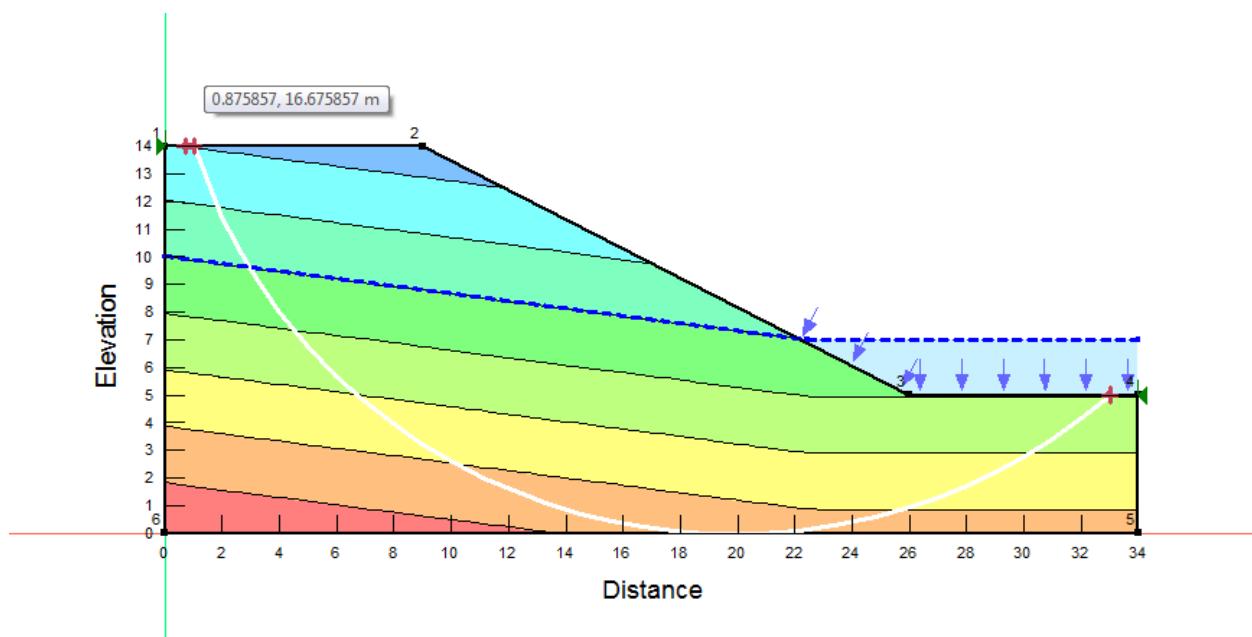


Figure4.1 : Pore Pressure from Piezometric line (Slope/W analysis Punjab region soil with Morgenstern-Price Method)

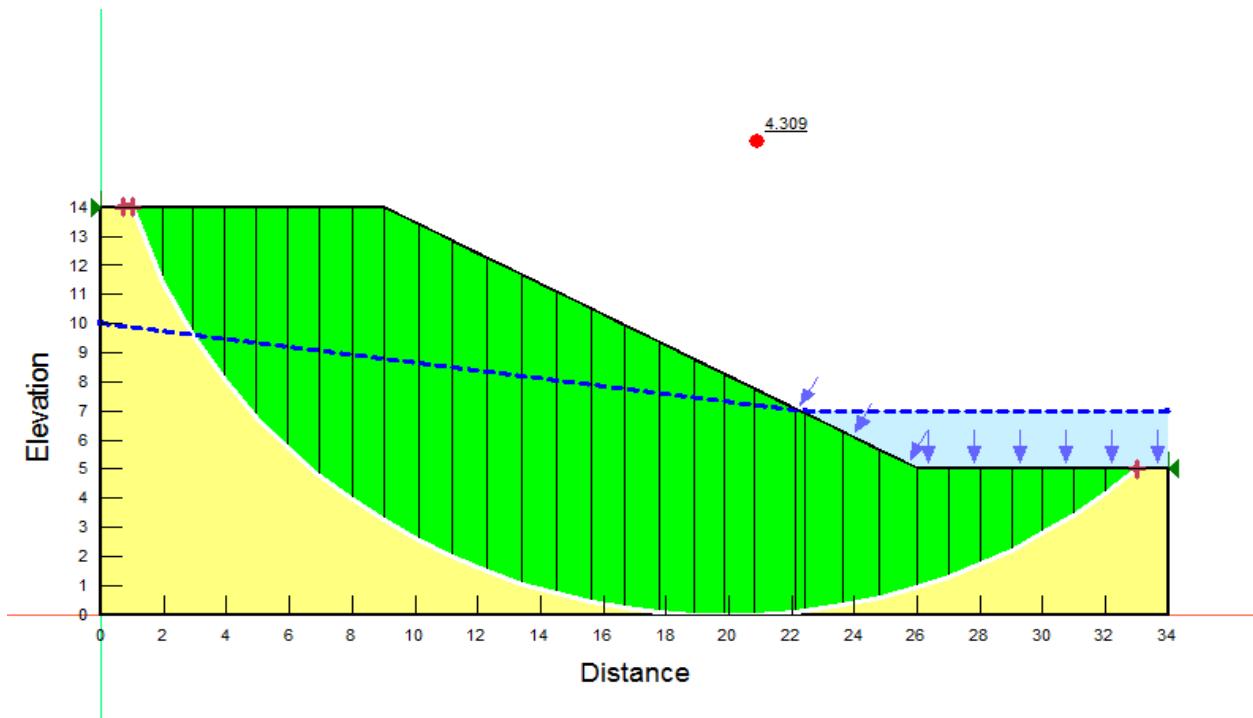


Figure4.2 : Factor of safety and slip surface results of Morgenstern Price analysis (Punjab Region Soil)

4.4.2. Slope/W analysis for Punjab soil with Bishop Method

File Information

File Version: 9.01
 Revision Number: 1
 Date: 06/21/2020
 Time: 06:17:13 PM
 Tool Version: 9.1.1.16749
 File Name: SLOPE W PUNJAB SOIL BISHOP.gsz
 Directory: C:\Users\Sys\Desktop\Major project content\Geoslope Punjab soil content\
 Last Solved Date: 06/21/2020
 Last Solved Time: 06:17:15 PM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

SLOPE W PUNJAB SOIL BISHOP

Kind: SLOPE/W

Method: **Bishop**

Settings

PWP Conditions from: **Piezometric Line**

Apply Phreatic Correction: **Yes**

Use Staged Rapid Drawdown: **No**

Unit Weight of Water: **9.807 kN/m³**

Slip Surface

Direction of movement: **Left to Right**

Use Passive Mode: **No**

Slip Surface Option: **Entry and Exit**

Critical slip surfaces saved: **1**

Optimize Critical Slip Surface Location: **No**

Tension Crack Option: **(none)**

Distribution

F of S Calculation Option: **Constant**

Advanced

Geometry Settings

Minimum Slip Surface Depth: **0.1 m**

Number of Slices: **30**

Factor of Safety Convergence Settings

Maximum Number of Iterations: **2,000**

Tolerable difference in F of S: **0.01**

Materials

New Material

Model: **Mohr-Coulomb**

Unit Weight: **18.24 kN/m³**

Cohesion': **53 kPa**

Phi': **36.86 °**

Phi-B: **0 °**

Pore Water Pressure

Piezometric Line: **1**

Slip Surface Entry and Exit

Left Type: **Range**

Left-Zone Left Coordinate: **(0.7, 14) m**

Left-Zone Right Coordinate: **(1, 14) m**

Left-Zone Increment: **4**

Right Type: **Point**

Right Coordinate: **(33, 5) m**

Right-Zone Increment: **8**

Radius Increments: **4**

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 24

Factor of Safety: 4.295

Volume: 222.64535 m³

Weight: 4,061.0512 kN

Resisting Moment: 81,272.977 kN·m

Activating Moment: 18,922.23 kN·m

Slip Rank: 1 of 25 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 19.695433 m

Center: (19.860951, 19.672269) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength (kPa) | Base Material |
|----------|-----------|------------|------------|-------------------------|--------------------------|-------------------------|------------------------|---------------|
| Slice 1 | 1.4827338 | 12.723295 | -28.148091 | -6.3922564 | -4.7924672 | 53 | 0 kPa | New Material |
| Slice 2 | 2.4482014 | 10.527416 | -8.2344483 | 29.908625 | 22.423397 | 53 | 0 kPa | New Material |
| Slice 3 | 3.4358683 | 8.8424331 | 6.7281822 | 60.997289 | 40.687184 | 53 | 0 kPa | New Material |
| Slice 4 | 4.4457348 | 7.4402892 | 18.937111 | 88.746494 | 52.338197 | 53 | 0 kPa | New Material |
| Slice 5 | 5.4556012 | 6.2615695 | 28.993377 | 112.28205 | 62.444023 | 53 | 0 kPa | New Material |
| Slice 6 | 6.4654676 | 5.2501951 | 37.437295 | 132.69534 | 71.417828 | 53 | 0 kPa | New Material |
| Slice 7 | 7.475334 | 4.372447 | 44.593741 | 150.63673 | 79.503621 | 53 | 0 kPa | New Material |
| Slice 8 | 8.4852004 | 3.6061675 | 50.676203 | 166.53095 | 86.85979 | 53 | 0 kPa | New Material |
| Slice 9 | 9.4950668 | 2.9359079 | 55.833525 | 180.67299 | 93.595905 | 53 | 0 kPa | New Material |
| Slice 10 | 10.556625 | 2.3246277 | 60.356019 | 188.62387 | 96.166268 | 53 | 0 kPa | New Material |
| Slice 11 | 11.669876 | 1.7713842 | 64.252767 | 190.21246 | 94.435776 | 53 | 0 kPa | New Material |
| Slice 12 | 12.783126 | 1.302221 | 67.339412 | 190.04767 | 91.998078 | 53 | 0 kPa | New Material |
| Slice 13 | 13.896377 | 0.91079783 | 69.677042 | 188.26789 | 88.911132 | 53 | 0 kPa | New Material |
| Slice 14 | 15.009627 | 0.59230863 | 71.311964 | 184.97657 | 85.217781 | 53 | 0 kPa | New Material |
| Slice 15 | 16.122877 | 0.34313347 | 72.279055 | 180.25031 | 80.949303 | 53 | 0 kPa | New Material |
| Slice 16 | 17.236128 | 0.1606069 | 72.603995 | 174.14413 | 76.127698 | 53 | 0 kPa | New Material |
| Slice 17 | 18.349378 | 0.04286321 | 72.304761 | 166.69493 | 70.767152 | 53 | 0 kPa | New Material |
| Slice 18 | 19.383477 | 0 | 71.385998 | 159.08553 | 65.750977 | 53 | 0 kPa | New Material |
| Slice 19 | 20.338424 | 0 | 70.156187 | 149.28777 | 59.327328 | 53 | 0 kPa | New Material |
| Slice 20 | 21.223023 | 0.02822915 | 68.744989 | 141.43195 | 54.495603 | 53 | 0 kPa | New Material |
| Slice 21 | 22.037274 | 0.10173232 | 66.988179 | 132.6483 | 49.227371 | 53 | 0 kPa | New Material |

| | | | | | | | | |
|----------|-----------|------------|-----------|-----------|-----------|----|-------|--------------|
| Slice 22 | 23.037015 | 0.24388432 | 66.257226 | 124.0875 | 43.357101 | 53 | 0 kPa | New Material |
| Slice 23 | 24.222222 | 0.47539134 | 63.986837 | 115.41806 | 38.559539 | 53 | 0 kPa | New Material |
| Slice 24 | 25.407407 | 0.78403287 | 60.95999 | 105.21518 | 33.17945 | 53 | 0 kPa | New Material |
| Slice 25 | 26.5 | 1.137139 | 57.49707 | 96.958646 | 29.585526 | 53 | 0 kPa | New Material |
| Slice 26 | 27.5 | 1.5267266 | 53.676393 | 90.895098 | 27.903985 | 53 | 0 kPa | New Material |
| Slice 27 | 28.5 | 1.9813871 | 49.217537 | 83.631384 | 25.801098 | 53 | 0 kPa | New Material |
| Slice 28 | 29.5 | 2.5063145 | 44.069574 | 75.064163 | 23.237577 | 53 | 0 kPa | New Material |
| Slice 29 | 30.5 | 3.108224 | 38.166647 | 65.059026 | 20.162026 | 53 | 0 kPa | New Material |
| Slice 30 | 31.5 | 3.7959261 | 31.422353 | 53.437941 | 16.50575 | 53 | 0 kPa | New Material |
| Slice31 | 32.5 | 4.5812397 | 23.720783 | 39.958724 | 12.174073 | 53 | 0 kPa | New Material |

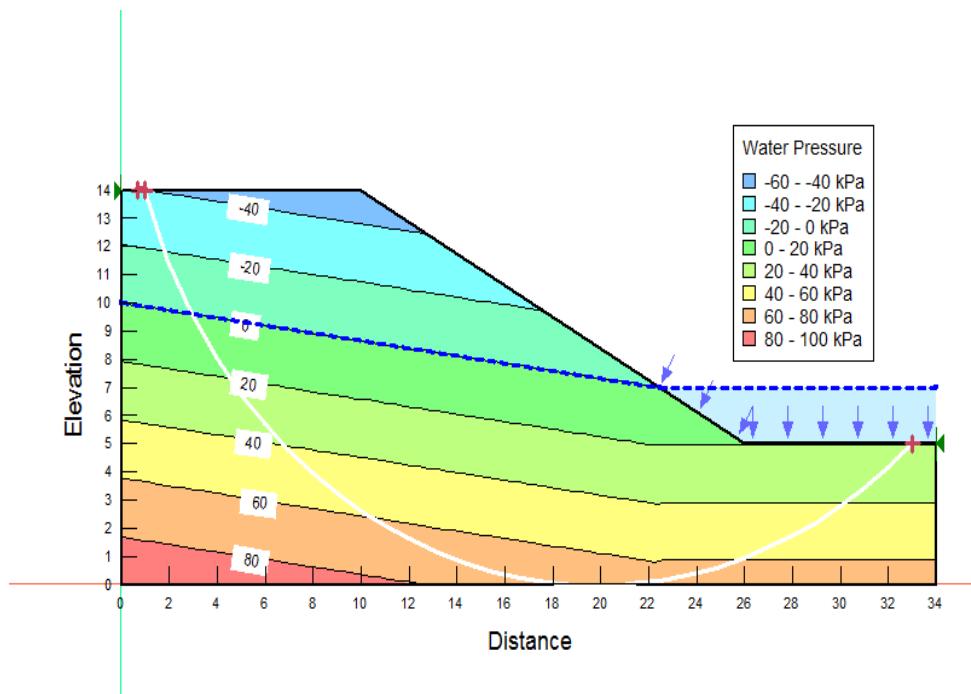


Figure4.3 : Pore Pressure from Piezometric line (Slope/W analysis Punjab region soil with Bishop Method)

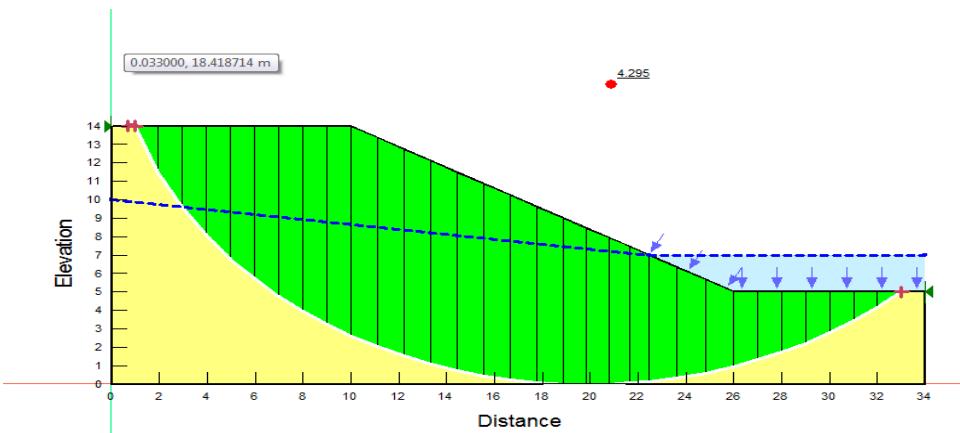


Figure4.4 : Factor of safety and slip surface results of Bishop analysis (Punjab Region Soil)

4.4.3. Slope/W analysis of Punjab soil with Janbu method

File Information

File Version: 9.01
Revision Number: 2
Date: 06/21/2020
Time: 06:46:43 PM
Tool Version: 9.1.1.16749
File Name: SLOPE W PUNJAB JANBU SOIL.gsz
Directory: C:\Users\Sys\Desktop\Major project content\Geoslope Punjab soil content\
Last Solved Date: 06/22/2020
Last Solved Time: 08:24:13 PM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

SLOPE W PUNJAB JANBU

Kind: SLOPE/W

Method: Janbu

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: Yes

Use Staged Rapid Drawdown: No

Unit Weight of Water: 9.807 kN/m³

Slip Surface

Direction of movement: Left to Right

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

Geometry Settings

Minimum Slip Surface Depth: 0.1 m

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 2,000

Tolerable difference in F of S: 0.01

Materials

New Material

Model: Mohr-Coulomb
Unit Weight: 18.24 kN/m³
Cohesion': 53 kPa
Phi': 36.86 °
Phi-B: 0 °
Pore Water Pressure
Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range
Left-Zone Left Coordinate: (0.7, 14) m
Left-Zone Right Coordinate: (1, 14) m
Left-Zone Increment: 4
Right Type: Point
Right Coordinate: (33, 5) m
Right-Zone Increment: 8
Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m
Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 24
Factor of Safety: 3.854
Volume: 222.64535 m³
Weight: 4,061.0512 kN
Resisting Force: 3,446.4976 kN
Activating Force: 894.37729 kN
Slip Rank: 1 of 25 slip surfaces
Exit: (33, 5) m
Entry: (1, 14) m
Radius: 19.695433 m
Center: (19.860951, 19.672269) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength (kPa) | Base Material |
|----------|-----------|------------|------------|-------------------------|--------------------------|-------------------------|------------------------|---------------|
| Slice 1 | 1.4827338 | 12.723295 | -28.148091 | -8.6732878 | -6.5026251 | 53 | 0 | New Material |
| Slice 2 | 2.4482014 | 10.527416 | -8.2344483 | 27.068777 | 20.294277 | 53 | 0 | New Material |
| Slice 3 | 3.4358683 | 8.8424331 | 6.7281822 | 58.023825 | 38.457889 | 53 | 0 | New Material |
| Slice 4 | 4.4457348 | 7.4402892 | 18.937111 | 85.85704 | 50.171886 | 53 | 0 | New Material |
| Slice 5 | 5.4556012 | 6.2615695 | 28.993377 | 109.50201 | 60.359748 | 53 | 0 | New Material |
| Slice 6 | 6.4654676 | 5.2501951 | 37.437295 | 130.0425 | 69.428911 | 53 | 0 | New Material |
| Slice 7 | 7.475334 | 4.372447 | 44.593741 | 148.1249 | 77.620425 | 53 | 0 | New Material |
| Slice 8 | 8.4852004 | 3.6061675 | 50.676203 | 164.17169 | 85.090987 | 53 | 0 | New Material |
| Slice 9 | 9.4950668 | 2.9359079 | 55.833525 | 178.47651 | 91.949143 | 53 | 0 | New Material |
| Slice 10 | 10.556625 | 2.3246277 | 60.356019 | 186.66011 | 94.693979 | 53 | 0 | New Material |
| Slice 11 | 11.669876 | 1.7713842 | 64.252767 | 188.53319 | 93.17678 | 53 | 0 | New Material |
| Slice 12 | 12.783126 | 1.302221 | 67.339412 | 188.63885 | 90.941845 | 53 | 0 | New Material |
| Slice 13 | 13.896377 | 0.91079783 | 69.677042 | 187.11612 | 88.04761 | 53 | 0 | New Material |
| Slice 14 | 15.009627 | 0.59230863 | 71.311964 | 184.06878 | 84.537179 | 53 | 0 | New Material |
| Slice 15 | 16.122877 | 0.34313347 | 72.279055 | 179.57352 | 80.441894 | 53 | 0 | New Material |
| Slice 16 | 17.236128 | 0.1606069 | 72.603995 | 173.68522 | 75.783638 | 53 | 0 | New Material |
| Slice 17 | 18.349378 | 0.04286321 | 72.304761 | 166.44036 | 70.576296 | 53 | 0 | New Material |
| Slice 18 | 19.383477 | 0 | 71.385998 | 159.08553 | 65.750977 | 53 | 0 | New Material |
| Slice 19 | 20.338424 | 0 | 70.156187 | 149.28777 | 59.327328 | 53 | 0 | New Material |
| Slice 20 | 21.223023 | 0.02822915 | 68.744989 | 141.63679 | 54.649176 | 53 | 0 | New Material |
| Slice 21 | 22.037274 | 0.10173232 | 66.988179 | 132.96332 | 49.463554 | 53 | 0 | New Material |
| Slice 22 | 23.037015 | 0.24388432 | 66.257226 | 124.5286 | 43.687807 | 53 | 0 | New Material |
| Slice 23 | 24.222222 | 0.47539134 | 63.986837 | 116.00812 | 39.001921 | 53 | 0 | New Material |
| Slice 24 | 25.407407 | 0.78403287 | 60.95999 | 105.94289 | 33.725036 | 53 | 0 | New Material |
| Slice 25 | 26.5 | 1.137139 | 57.497077 | 97.820784 | 30.231897 | 53 | 0 | New Material |
| Slice 26 | 27.5 | 1.5267266 | 53.676393 | 91.900994 | 28.658135 | 53 | 0 | New Material |
| Slice 27 | 28.5 | 1.9813871 | 49.217537 | 84.784347 | 26.665509 | 53 | 0 | New Material |
| Slice 28 | 29.5 | 2.5063145 | 44.069574 | 76.367333 | 24.214603 | 53 | 0 | New Material |
| Slice 29 | 30.5 | 3.108224 | 38.166647 | 66.515263 | 21.253811 | 53 | 0 | New Material |
| Slice 30 | 31.5 | 3.7959261 | 31.422353 | 55.049594 | 17.714055 | 53 | 0 | New Material |
| Slice 31 | 32.5 | 4.5812397 | 23.720783 | 41.72715 | 13.499916 | 53 | 0 | New Material |

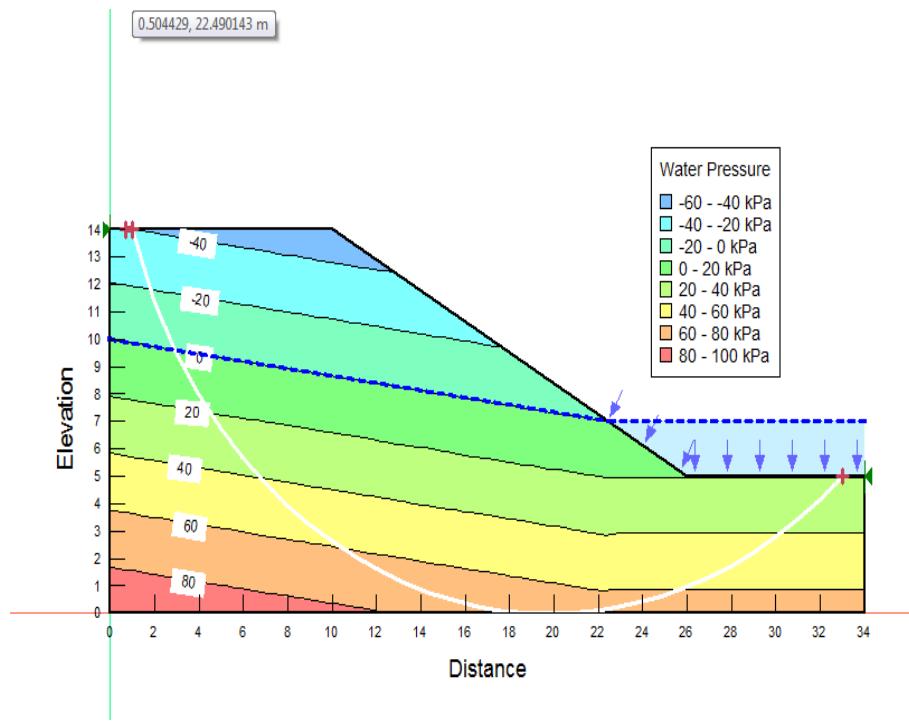


Figure4.5 : Pore Pressure through Piezometric line (Slope/W analysis on Punjab soil with Janbu Method)

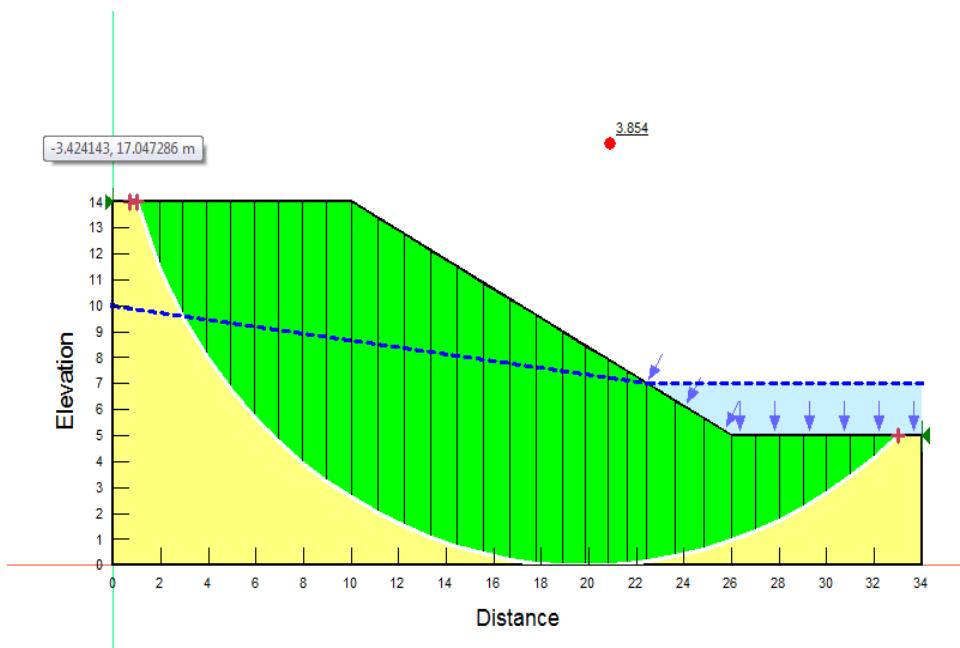


Figure4.6 : Factor of safety and slip surface results from Janbu analysis on Punjab soil

4.4.4.Slope/W analysis on Punjab soil with Ordinary method

File Information

File Version: 9.01

Revision Number: 2

Date: 06/21/2020

Time: 10:44:38 PM

Tool Version: 9.1.1.16749

File Name: SLOPE W PUNJAB SOIL ORDINARY.gsz

Directory: C:\Users\Sys\Desktop\Major project content\Geoslope Punjab soil content\

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

SLOPE W PUNJAB ORDINARY SOIL

Kind: SLOPE/W

Method: Ordinary

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: Yes

Use Staged Rapid Drawdown: No

Unit Weight of Water: 9.807 kN/m³

Slip Surface

Direction of movement: Left to Right

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

Geometry Settings

Minimum Slip Surface Depth: 0.1 m

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 2,000

Tolerable difference in F of S: 0.01

Materials

SOIL LAYER

Model: Mohr-Coulomb

Unit Weight: 18.24 kN/m³

Cohesion': 53 kPa

Phi': 36.86 °

Phi-B: 0 °

Pore Water Pressure

Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (0.7, 14) m

Left-Zone Right Coordinate: (1, 14) m

Left-Zone Increment: 4

Right Type: Point

Right Coordinate: (33, 5) m

Right-Zone Increment: 8

Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 24

Factor of Safety: 3.936

Volume: 222.64535 m³

Weight: 4,061.0512 kN

Resisting Moment: 74,479.334 kN·m

Activating Moment: 18,922.23 kN·m

Slip Rank: 1 of 25 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 19.695433 m

Center: (19.860951, 19.672269) m

Slip Slices

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength (kPa) | Suction Strength (kPa) | Base Material |
|----------|-----------|-------------|------------|-------------------------|--------------------------|-------------------------|------------------------|---------------|
| Slice 1 | 1.4827338 | 12.723295 | -28.148091 | 2.9128377 | 2.1838421 | 53 | 0 | SOIL LAYER |
| Slice 2 | 2.4482014 | 10.527416 | -8.2344483 | 13.693313 | 10.266289 | 53 | 0 | SOIL LAYER |
| Slice 3 | 3.4358683 | 8.8424331 | 6.7281822 | 33.1947 | 19.842798 | 53 | 0 | SOIL LAYER |
| Slice 4 | 4.4457348 | 7.4402892 | 18.937111 | 57.849073 | 29.17347 | 53 | 0 | SOIL LAYER |
| Slice 5 | 5.4556012 | 6.2615695 | 28.993377 | 81.065822 | 39.04028 | 53 | 0 | SOIL LAYER |
| Slice 6 | 6.4654676 | 5.2501951 | 37.437295 | 103.01895 | 49.168542 | 53 | 0 | SOIL LAYER |
| Slice 7 | 7.475334 | 4.372447 | 44.593741 | 123.73961 | 59.338042 | 53 | 0 | SOIL LAYER |
| Slice 8 | 8.4852004 | 3.6061675 | 50.676203 | 143.19794 | 69.366333 | 53 | 0 | SOIL LAYER |
| Slice 9 | 9.4950668 | 2.9359079 | 55.833525 | 161.33685 | 79.099018 | 53 | 0 | SOIL LAYER |
| Slice 10 | 10.556625 | 2.3246277 | 60.356019 | 174.43201 | 85.526203 | 53 | 0 | SOIL LAYER |
| Slice 11 | 11.669876 | 1.7713842 | 64.252767 | 181.3908 | 87.821913 | 53 | 0 | SOIL LAYER |
| Slice 12 | 12.783126 | 1.302221 | 67.339412 | 185.51021 | 88.596206 | 53 | 0 | SOIL LAYER |
| Slice 13 | 13.896377 | 0.91079783 | 69.677042 | 186.92036 | 87.90085 | 53 | 0 | SOIL LAYER |
| Slice 14 | 15.009627 | 0.59230863 | 71.311964 | 185.75859 | 85.804085 | 53 | 0 | SOIL LAYER |
| Slice 15 | 16.122877 | 0.34313347 | 72.279055 | 182.17059 | 82.388992 | 53 | 0 | SOIL LAYER |
| Slice 16 | 17.236128 | 0.1606069 | 72.603995 | 176.31105 | 77.752303 | 53 | 0 | SOIL LAYER |
| Slice 17 | 18.349378 | 0.04286321 | 72.304761 | 168.34406 k | 72.003552 | 53 | 0 | SOIL LAYER |
| Slice 18 | 19.383477 | 0 | 71.385998 | 159.08553 | 65.750977 | 53 | 0 | SOIL LAYER |
| Slice 19 | 20.338424 | 0 | 70.156187 | 149.28777 | 59.327328 | 53 | 0 | SOIL LAYER |
| Slice 20 | 21.223023 | 0.028229151 | 68.744989 | 139.35739 | 52.940247 | 53 | 0 | SOIL LAYER |
| Slice 21 | 22.037274 | 0.10173232 | 66.988179 | 129.23223 | 46.666243 | 53 | 0 | SOIL LAYER |
| Slice 22 | 23.037015 | 0.24388432 | 66.257226 | 118.71809 | 39.331489 | 53 | 0 | SOIL LAYER |
| Slice 23 | 24.222222 | 0.47539134 | 63.986837 | 107.0975Pa | 32.321363 | 53 | 0 | SOIL LAYER |
| Slice 24 | 25.407407 | 0.78403287 | 60.95999 | 93.793289 | 24.616114 | 53 | 0 | SOIL LAYER |
| Slice 25 | 26.5 | 1.137139 | 57.497077 | 86.36844 | 21.64573 | 53 | 0 | SOIL LAYER |
| Slice 26 | 27.5 | 1.5267266 | 53.676393 | 78.556917 | 18.653679 | 53 | 0 | SOIL LAYER |
| Slice 27 | 28.5 | 1.9813871 | 49.217537 | 69.771908 | 15.410231 | 53 | 0 | SOIL LAYER |
| Slice 28 | 29.5 | 2.5063145 | 44.069574 | 60.057677 | 11.986762 | 53 | 0 | SOIL LAYER |
| Slice 29 | 30.5 | 3.108224 | 38.166647 | 49.460681 | 8.4674773 | 53 | 0 | SOIL LAYER |
| Slice 30 | 31.5 | 3.7959261 | 31.422353 | 38.026787 | 4.9515435 | 53 | 0 | SOIL LAYER |
| Slice 31 | 32.5 | 4.5812397 | 23.720783 | 25.796321 | 1.5560937 | 53 | 0 | SOIL LAYER |

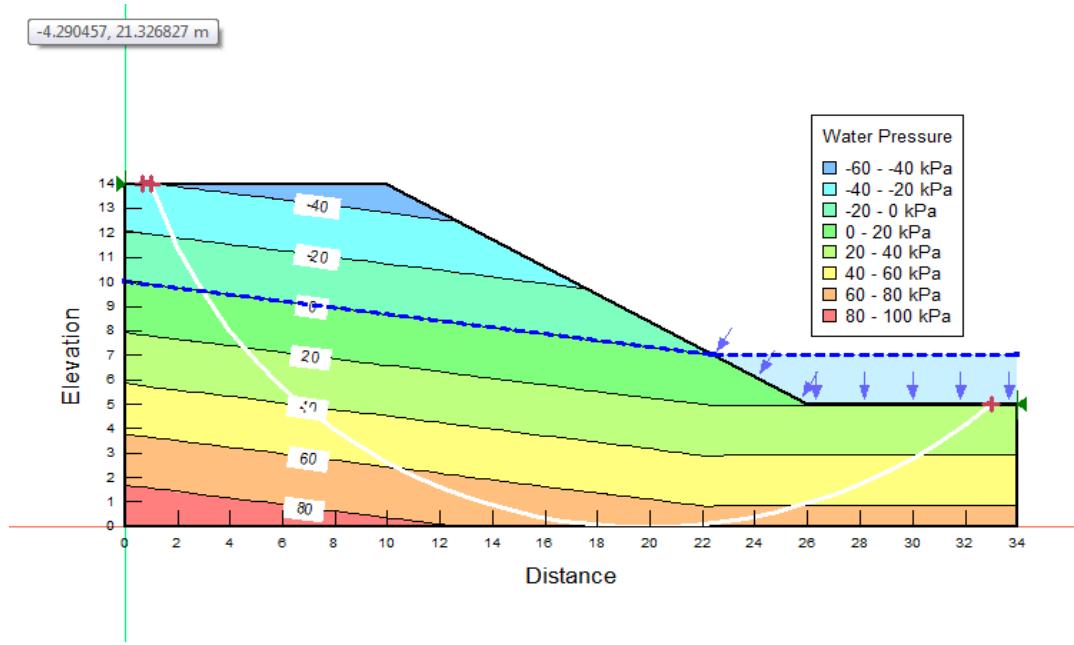


Figure4.7:Pore pressure through piezometric line (Punjab region sample slope/W with Ordinary method)

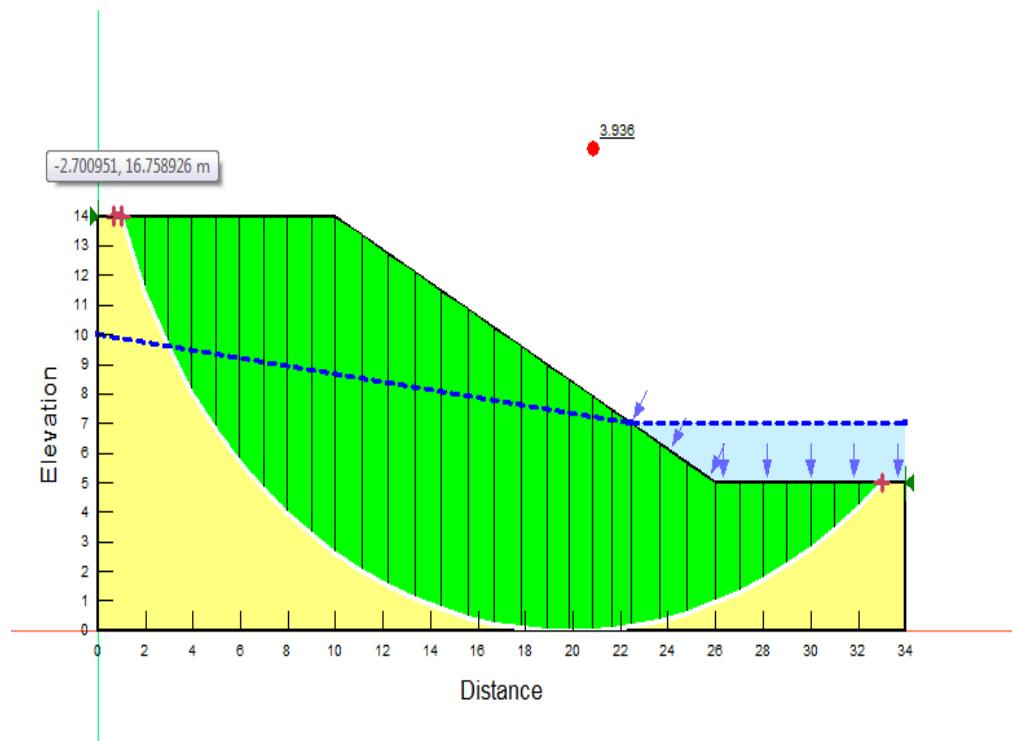


Figure4.8: Factor of safety and slip surface of Punjab soil with Ordinary Method

4.5.1 Slope/W analysis on DTU soil with Morgenstern-Price Method

File Information

File Version: 9.01
Revision Number: 2
Date: 06/25/2020
Time: 12:24:11 AM
Tool Version: 9.1.1.16749
File Name: SLOPE W DTU MORGENSTERN PRICE.gsz
Directory: C:\Users\Sys\Desktop\Major project content\Geoslope DTU soil Content\
Last Solved Date: 06/25/2020
Last Solved Time: 12:25:04 AM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

Slope w on DTU Morgenstern price

Kind: SLOPE/W
Method: Morgenstern-Price
Settings
Side Function
Interslice force function option: Half-Sine
PWP Conditions from: Piezometric Line
Apply Phreatic Correction: Yes
Use Staged Rapid Drawdown: No
Unit Weight of Water: 9.807 kN/m³

Slip Surface
Direction of movement: Left to Right
Use Passive Mode: No
Slip Surface Option: Entry and Exit
Critical slip surfaces saved: 1
Optimize Critical Slip Surface Location: No
Tension Crack Option: (none)

Distribution
F of S Calculation Option: Constant

Advanced
Geometry Settings
Minimum Slip Surface Depth: 0.1 m
Number of Slices: 30
Factor of Safety Convergence Settings
Maximum Number of Iterations: 2,000

Tolerable difference in F of S: [0.01](#)
Solution Settings
Search Method: [Root Finder](#)
Tolerable difference between starting and converged F of S: [3](#)
Maximum iterations to calculate converged lambda: [20](#)
Max Absolute Lambda: [2](#)

Materials

Soil Layer

Model: [Mohr-Coulomb](#)
Unit Weight: [16.57 kN/m³](#)
Cohesion': [4.05 kPa](#)
Phi': [41.78 °](#)
Phi-B: [0 °](#)
Pore Water Pressure
Piezometric Line: [1](#)

Slip Surface Entry and Exit

Left Type: [Range](#)
Left-Zone Left Coordinate: [\(0.7, 14\) m](#)
Left-Zone Right Coordinate: [\(1, 14\) m](#)
Left-Zone Increment: [4](#)
Right Type: [Point](#)
Right Coordinate: [\(33, 5\) m](#)
Right-Zone Increment: [8](#)
Radius Increments: [4](#)

Slip Surface Limits

Left Coordinate: [\(0, 14\) m](#)
Right Coordinate: [\(34, 5\) m](#)

Slip Results

Slip Surfaces Analysed: [20 of 25 converged](#)

Current Slip Surface

Slip Surface: [23](#)
Factor of Safety: [2.319](#)
Volume: [152.26374 m³](#)
Weight: [2,523.0101 kN](#)
Resisting Moment: [40,887.946 kN·m](#)
Activating Moment: [17,622.202 kN·m](#)

Resisting Force: 1,456.9997 kN

Activating Force: 628.44511 kN

Slip Rank: 1 of 25 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 25.087975 m

Center: (22.087975, 27.590578) m

Slip Slices

| | X | Y | PWP | Base Normal Stress | Frictional Strength | Cohesive Strength | Suction Strength | Base Material |
|----------|-----------|-----------|------------|--------------------|---------------------|-------------------|------------------|---------------|
| Slice 1 | 1.4829265 | 13.303515 | -33.738677 | 5.7321118 | 5.1215001 | 4.05 | 0 | Soil Layer |
| Slice 2 | 2.4487794 | 11.998745 | -22.411246 | 20.224143 | 18.069772 | 4.05 | 0 | Soil Layer |
| Slice 3 | 3.4146323 | 10.851721 | -12.603689 | 33.549517 | 29.975664 | 4.05 | 0 | Soil Layer |
| Slice 4 | 4.3804852 | 9.8314613 | -4.0174768 | 45.954697 | 41.059386 | 4.05 | 0 | Soil Layer |
| Slice 5 | 5.3770705 | 8.890909 | 3.7611832 | 58.773545 | 49.152185 | 4.05 | 0 | Soil Layer |
| Slice 6 | 6.4043882 | 8.0202353 | 10.826994 | 71.746781 | 54.430324 | 4.05 | 0 | Soil Layer |
| Slice 7 | 7.4317058 | 7.2386837 | 17.034126 | 83.733562 | 59.594296 | 4.05 | 0 | Soil Layer |
| Slice 8 | 8.4590235 | 6.5362725 | 22.478752 | 94.985716 | 64.78318 | 4.05 | 0 | Soil Layer |
| Slice 9 | 9.4863412 | 5.9052745 | 27.235319 | 105.69583 | 70.102529 | 4.05 | 0 | Soil Layer |
| Slice 10 | 10.518517 | 5.337205 | 31.379324 | 112.1289 | 72.147752 | 4.05 | 0 | Soil Layer |
| Slice 11 | 11.55555 | 4.8277111 | 34.952705 | 114.05933 | 70.679817 | 4.05 | 0 | Soil Layer |
| Slice 12 | 12.592583 | 4.3757077 | 37.972173 | 115.28798 | 69.079759 | 4.05 | 0 | Soil Layer |
| Slice 13 | 13.629617 | 3.9778839 | 40.469627 | 115.80665 | 67.311769 | 4.05 | 0 | Soil Layer |
| Slice 14 | 14.66665 | 3.6315341 | 42.471137 | 115.58017 | 65.321114 | 4.05 | 0 | Soil Layer |
| Slice 15 | 15.703683 | 3.334448 | 43.997997 | 114.55019 | 63.036643 | 4.05 | 0 | Soil Layer |
| Slice 16 | 16.740717 | 3.0848302 | 45.067507 | 112.63935 | 60.373772 | 4.05 | 0 | Soil Layer |
| Slice 17 | 17.77775 | 2.8812391 | 45.693556 | 109.75615 | 57.238345 | 4.05 | 0 | Soil Layer |
| Slice 18 | 18.814783 | 2.7225422 | 45.887056 | 105.80099 | 53.531615 | 4.05 | 0 | Soil Layer |
| Slice 19 | 19.851817 | 2.6078822 | 45.656266 | 100.67336 | 49.156413 | 4.05 | 0 | Soil Layer |
| Slice 20 | 20.88885 | 2.5366535 | 45.007021 | 94.280185 | 44.024354 | 4.05 | 0 | Soil Layer |
| Slice 21 | 21.925883 | 2.5084855 | 43.942892 | 86.544712 | 38.063673 | 4.05 | 0 | Soil Layer |
| Slice 22 | 23.037015 | 2.5275747 | 43.861075 | 80.622249 | 32.8452 | 4.05 | 0 | Soil Layer |
| Slice 23 | 24.222222 | 2.6006247 | 43.144674 | 76.428562 | 29.738331 | 4.05 | 0 | Soil Layer |
| Slice 24 | 25.407407 | 2.7303598 | 41.872361 | 70.265513 | 25.368579 | 4.05 | 0 | Soil Layer |
| Slice 25 | 26.5 | 2.8988272 | 40.220202 | 62.774052 | 20.151307 | 4.05 | 0 | Soil Layer |
| Slice 26 | 27.5 | 3.0986552 | 38.260489 | 59.125957 | 18.64278 | 4.05 | 0 | Soil Layer |
| Slice 27 | 28.5 | 3.341352 | 35.880361 | 54.36405 | 16.514719 | 4.05 | 0 | Soil Layer |
| Slice 28 | 29.5 | 3.6282227 | 33.06702 | 48.51894 | 13.805909 | 4.05 | 0 | Soil Layer |
| Slice 29 | 30.5 | 3.9608794 | 29.804656 | 41.648066 | 10.581794 | 4.05 | 0 | Soil Layer |
| Slice 30 | 31.5 | 4.3412916 | 26.073953 | 33.831636 | 6.9312981 | 4.05 | 0 | Soil Layer |
| Slice 31 | 32.5 | 4.7718535 | 21.851433 | 25.16621 | 2.9616712 | 4.05 | 0 | Soil Layer |

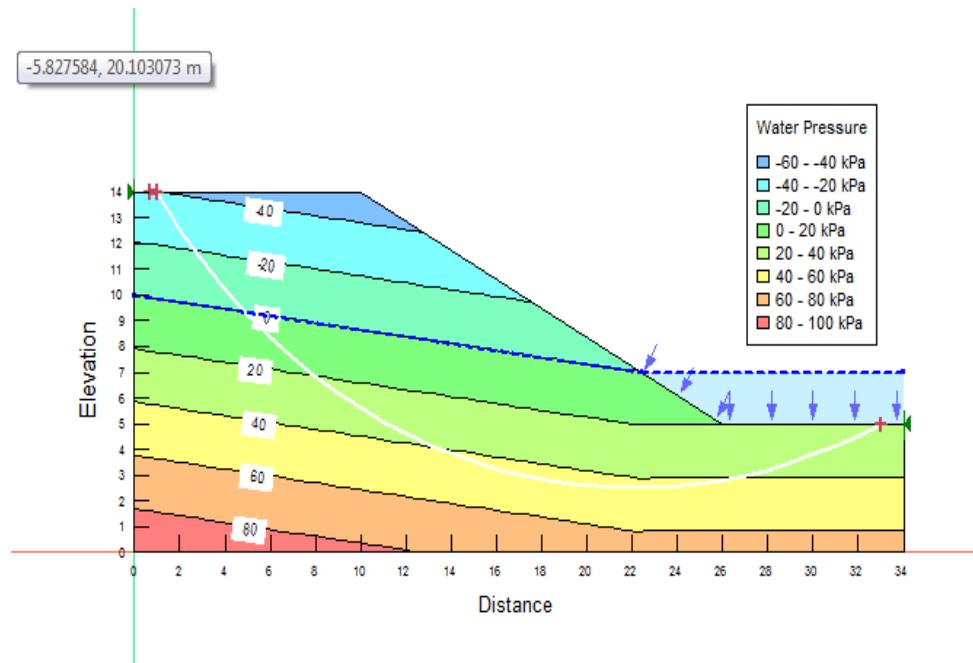


Figure5.1:Pore pressure through piezometric line (DTU region sample slope/W with Morgenstern-Price method)

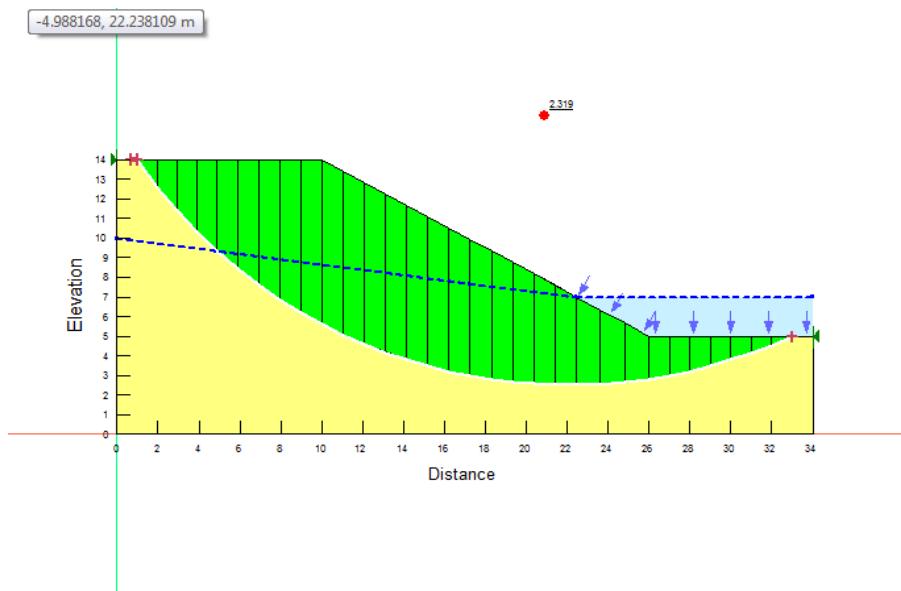


Figure5.2 : Factor of safety and slip surface results from Morgenstern-Price analysis on DTU soil

4.5.2 Slope/W analysis on DTU soil with Bishop Method

File Information

File Version: 9.01
Revision Number: 1
Date: 06/25/2020
Time: 12:33:57 AM
Tool Version: 9.1.1.16749
File Name: SLOPE W DTU BISHOP.gsz
Directory: C:\Users\Sys\Desktop\Major project content\Geoslope DTU soil Content\
Last Solved Date: 06/25/2020
Last Solved Time: 12:34:02 AM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

SLOPE W DTU BISHOP METHOD

Kind: SLOPE/W

Method: Bishop

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: Yes

Use Staged Rapid Drawdown: No

Unit Weight of Water: 9.807 kN/m³

Slip Surface

Direction of movement: Left to Right

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

Geometry Settings

Minimum Slip Surface Depth: 0.1 m

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 2,000

Tolerable difference in F of S: 0.01

Materials

SOIL LAYER

Model: Mohr-Coulomb

Unit Weight: 16.57 kN/m³

Cohesion': 4.05 kPa

Phi': 41.78 °

Phi-B: 0 °

Pore Water Pressure

Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (0.7, 14) m

Left-Zone Right Coordinate: (1, 14) m

Left-Zone Increment: 4

Right Type: Point

Right Coordinate: (33, 5) m

Right-Zone Increment: 8

Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 23

Factor of Safety: 2.309

Volume: 152.26374 m³

Weight: 2,523.0101 kN

Resisting Moment: 40,682.896 kN·m

Activating Moment: 17,622.202 kN·m

Slip Rank: 1 of 25 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 25.087975 m

Center: (22.087975, 27.590578) m

Slip Slices

| | X | Y | PWP | Base Normal Stress | Frictional Strength | Cohesive Strength | Suction Strength | Base Material |
|----------|-----------|-----------|------------|--------------------|---------------------|-------------------|------------------|---------------|
| Slice 1 | 1.4829265 | 13.303515 | -33.738677 | 5.7863362 | 5.1699483 | 4.05 | 0 | SOIL LAYER |
| Slice 2 | 2.4487794 | 11.998745 | -22.411246 | 20.815509 | 18.598143 | 4.05 | 0 | SOIL LAYER |
| Slice 3 | 3.4146323 | 10.851721 | -12.603689 | 35.080217 | 31.343306 | 4.05 | 0 | SOIL LAYER |
| Slice 4 | 4.3804852 | 9.8314613 | -4.0174768 | 48.591532 | 43.415332 | 4.05 | 0 | SOIL LAYER |
| Slice 5 | 5.3770705 | 8.890909 | 3.7611832 | 62.719332 | 52.677648 | 4.05 | 0 | SOIL LAYER |
| Slice 6 | 6.4043882 | 8.0202353 | 10.826994 | 77.133957 | 59.243632 | 4.05 | 0 | SOIL LAYER |
| Slice 7 | 7.4317058 | 7.2386837 | 17.034126 | 90.356431 | 65.511666 | 4.05 | 0 | SOIL LAYER |
| Slice 8 | 8.4590235 | 6.5362725 | 22.478752 | 102.50862 | 71.50471 | 4.05 | 0 | SOIL LAYER |
| Slice 9 | 9.4863412 | 5.9052745 | 27.235319 | 113.68632 | 77.241834 | 4.05 | 0 | SOIL LAYER |
| Slice 10 | 10.518517 | 5.337205 | 31.379324 | 119.98649 | 79.168311 | 4.05 | 0 | SOIL LAYER |
| Slice 11 | 11.55555 | 4.8277111 | 34.952705 | 121.23814 | 77.093904 | 4.05 | 0 | SOIL LAYER |
| Slice 12 | 12.592583 | 4.3757077 | 37.972173 | 121.39911 | 74.539908 | 4.05 | 0 | SOIL LAYER |
| Slice 13 | 13.629617 | 3.9778839 | 40.469627 | 120.52085 | 71.52379 | 4.05 | 0 | SOIL LAYER |
| Slice 14 | 14.66665 | 3.6315341 | 42.471137 | 118.64356 | 68.05818 | 4.05 | 0 | SOIL LAYER |
| Slice 15 | 15.703683 | 3.334448 | 43.997997 | 115.79798 | 64.151506 | 4.05 | 0 | SOIL LAYER |
| Slice 16 | 16.740717 | 3.0848302 | 45.067507 | 112.00658 | 59.80841 | 4.05 | 0 | SOIL LAYER |
| Slice 17 | 17.77775 | 2.8812391 | 45.693556 | 107.28451 | 55.029997 | 4.05 | 0 | SOIL LAYER |
| Slice 18 | 18.814783 | 2.7225422 | 45.887056 | 101.64008 | 49.813948 | 4.05 | 0 | SOIL LAYER |
| Slice 19 | 19.851817 | 2.6078822 | 45.656266 | 95.075094 | 44.1545 | 4.05 | 0 | SOIL LAYER |
| Slice 20 | 20.88885 | 2.5366535 | 45.007021 | 87.58493 | 38.042309 | 4.05 | 0 | SOIL LAYER |
| Slice 21 | 21.925883 | 2.5084855 | 43.942892 | 79.158387 | 31.464174 | 4.05 | 0 | SOIL LAYER |
| Slice 22 | 23.037015 | 2.5275747 | 43.861075 | 72.337128 | 25.442649 | 4.05 | 0 | SOIL LAYER |
| Slice 23 | 24.222222 | 2.6006247 | 43.144674 | 67.074547 | 21.38075 | 4.05 | 0 | SOIL LAYER |
| Slice 24 | 25.407407 | 2.7303598 | 41.872361 | 60.68136 | 16.805376 | 4.05 | 0 | SOIL LAYER |
| Slice 25 | 26.5 | 2.8988272 | 40.220202 | 55.821488 | 13.939364 | 4.05 | 0 | SOIL LAYER |
| Slice 26 | 27.5 | 3.0986552 | 38.260489 | 52.744049 | 12.940703 | 4.05 | 0 | SOIL LAYER |
| Slice 27 | 28.5 | 3.341352 | 35.880361 | 48.891501 | 11.625132 | 4.05 | 0 | SOIL LAYER |
| Slice 28 | 29.5 | 3.6282227 | 33.06702 | 44.220432 | 9.9652983 | 4.05 | 0 | SOIL LAYER |
| Slice 29 | 30.5 | 3.9608794 | 29.804656 | 38.677484 | 7.927652 | 4.05 | 0 | SOIL LAYER |
| Slice 30 | 31.5 | 4.3412916 | 26.073953 | 32.196727 | 5.4705473 | 4.05 | 0 | SOIL LAYER |
| Slice 31 | 32.5 | 4.7718535 | 21.851433 | 24.695971 | 2.5415246 | 4.05 | 0 | SOIL LAYER |

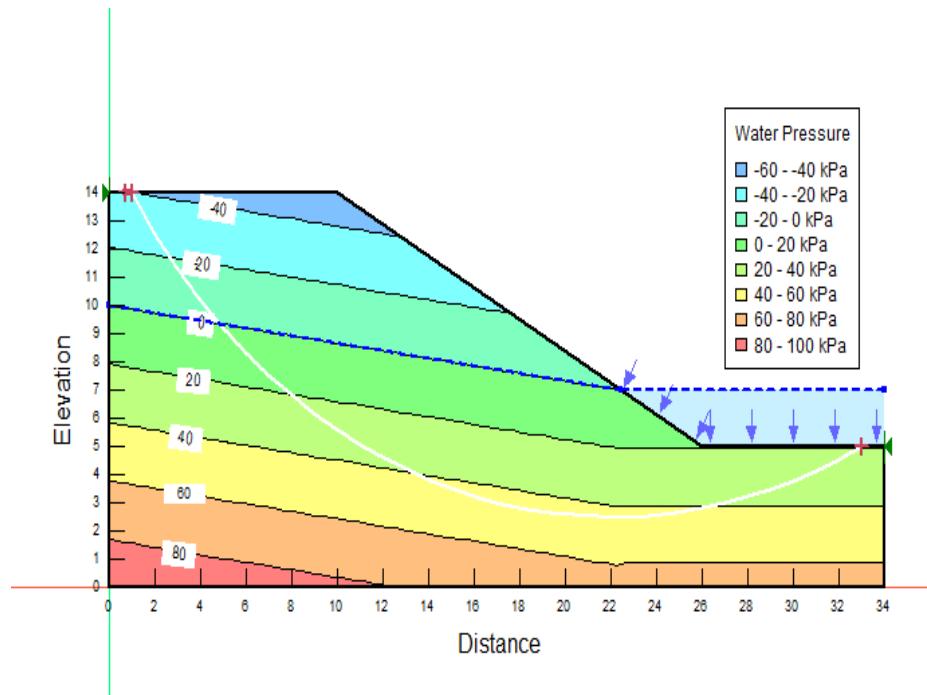


Figure 5.3:Pore pressure through piezometric line (DTU region sample slope/W with Bishop method)

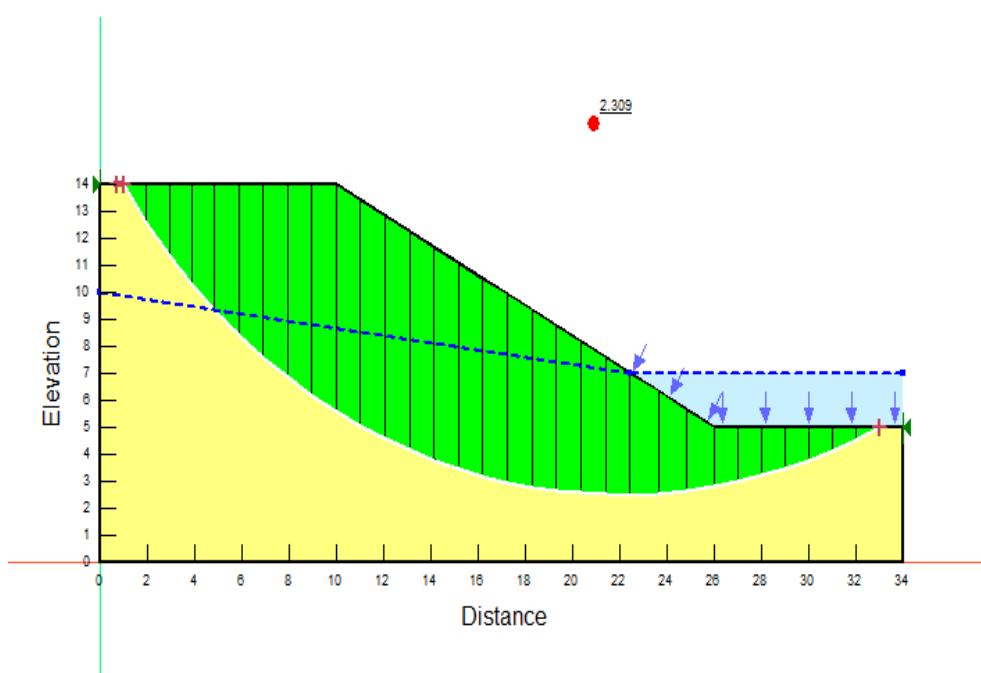


Figure 5.4 : Factor of safety and slip surface results from Bishop analysis on DTU soil

4.5.3 Slope/W analysis on DTU soil with Janbu Method

File Information

File Version: 9.01
Revision Number: 1
Date: 06/25/2020
Time: 12:41:00 AM
Tool Version: 9.1.1.16749
File Name: SLOPE W DTU JANBU.gsz
Directory: C:\Users\Sys\Desktop\Major project content\Geoslope DTU soil Content\
Last Solved Date: 06/25/2020
Last Solved Time: 12:41:02 AM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

SLOPE W DTU JANBU

Kind: SLOPE/W

Method: Janbu

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: Yes

Use Staged Rapid Drawdown: No

Unit Weight of Water: 9.807 kN/m³

Slip Surface

Direction of movement: Left to Right

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

Geometry Settings

Minimum Slip Surface Depth: 0.1 m

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 2,000

Tolerable difference in F of S: 0.01

Materials

SOIL LAYER

Model: Mohr-Coulomb

Unit Weight: 16.57 kN/m³

Cohesion': 4.05 kPa

Phi': 41.78 °

Phi-B: 0 °

Pore Water Pressure

Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (0.7, 14) m

Left-Zone Right Coordinate: (1, 14) m

Left-Zone Increment: 4

Right Type: Point

Right Coordinate: (33, 5) m

Right-Zone Increment: 8

Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 23

Factor of Safety: 2.138

Volume: 152.26374 m³

Weight: 2,523.0101 kN

Resisting Force: 1,425.5128 kN

Activating Force: 666.6162 kN

Slip Rank: 1 of 25 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 25.087975 m

Center: (22.087975, 27.590578) m

Slip Slices

| | X | Y | PWP | Base Normal Stress | Frictional Strength | Cohesive Strength | Suction Strength | Base Material |
|----------|-----------|-----------|------------|--------------------|---------------------|-------------------|------------------|---------------|
| Slice 1 | 1.4829265 | 13.303515 | -33.738677 | 5.5017939 | 4.9157168 | 4.05 | 0 | SOIL LAYER |
| Slice 2 | 2.4487794 | 11.998745 | -22.411246 | 20.17457 | 18.025479 | 4.05 | 0 | SOIL LAYER |
| Slice 3 | 3.4146323 | 10.851721 | -12.603689 | 34.156735 | 30.518198 | 4.05 | 0 | SOIL LAYER |
| Slice 4 | 4.3804852 | 9.8314613 | -4.0174768 | 47.445949 | 42.391782 | 4.05 | 0 | SOIL LAYER |
| Slice 5 | 5.3770705 | 8.890909 | 3.7611832 | 61.453664 | 51.546805 | 4.05 | 0 | SOIL LAYER |
| Slice 6 | 6.4043882 | 8.0202353 | 10.826994 | 75.831038 | 58.079506 | 4.05 | 0 | SOIL LAYER |
| Slice 7 | 7.4317058 | 7.2386837 | 17.034126 | 89.03612 | 64.332001 | 4.05 | 0 | SOIL LAYER |
| Slice 8 | 8.4590235 | 6.5362725 | 22.478752 | 101.18873 | 70.325419 | 4.05 | 0 | SOIL LAYER |
| Slice 9 | 9.4863412 | 5.9052745 | 27.235319 | 112.38311 | 76.077447 | 4.05 | 0 | SOIL LAYER |
| Slice 10 | 10.518517 | 5.337205 | 31.379324 | 118.76788 | 78.079513 | 4.05 | 0 | SOIL LAYER |
| Slice 11 | 11.55555 | 4.8277111 | 34.952705 | 120.15947 | 76.130141 | 4.05 | 0 | SOIL LAYER |
| Slice 12 | 12.592583 | 4.3757077 | 37.972173 | 120.45793 | 73.698982 | 4.05 | 0 | SOIL LAYER |
| Slice 13 | 13.629617 | 3.9778839 | 40.469627 | 119.7136 | 70.802527 | 4.05 | 0 | SOIL LAYER |
| Slice 14 | 14.66665 | 3.6315341 | 42.471137 | 117.96561 | 67.45244 | 4.05 | 0 | SOIL LAYER |
| Slice 15 | 15.703683 | 3.3344448 | 43.997997 | 115.24357 | 63.656159 | 4.05 | 0 | SOIL LAYER |
| Slice 16 | 16.740717 | 3.0848302 | 45.067507 | 111.56883 | 59.417284 | 4.05 | 0 | SOIL LAYER |
| Slice 17 | 17.77775 | 2.8812391 | 45.693556 | 106.95523 | 54.735795 | 4.05 | 0 | SOIL LAYER |
| Slice 18 | 18.814783 | 2.7225422 | 45.887056 | 101.40972 | 49.608128 | 4.05 | 0 | SOIL LAYER |
| Slice 19 | 19.851817 | 2.6078822 | 45.656266 | 94.932525 | 44.027119 | 4.05 | 0 | SOIL LAYER |
| Slice 20 | 20.88885 | 2.5366535 | 45.007021 | 87.517228 | 37.981818 | 4.05 | 0 | SOIL LAYER |
| Slice 21 | 21.925883 | 2.5084855 | 43.942892 | 79.150542 | 31.457164 | 4.05 | 0 | SOIL LAYER |
| Slice 22 | 23.037015 | 2.5275747 | 43.861075 | 72.376022 | 25.4774 | 4.05 | 0 | SOIL LAYER |
| Slice 23 | 24.222222 | 2.6006247 | 43.144674 | 67.151744 | 21.449723 | 4.05 | 0 | SOIL LAYER |
| Slice 24 | 25.407407 | 2.7303598 | 41.872361 | 60.782442 | 16.89569 | 4.05 | 0 | SOIL LAYER |
| Slice 25 | 26.5 | 2.8988272 | 40.220202 | 55.940545 | 14.045738 | 4.05 | 0 | SOIL LAYER |
| Slice 26 | 27.5 | 3.0986552 | 38.260489 | 52.885811 | 13.067364 | 4.05 | 0 | SOIL LAYER |
| Slice 27 | 28.5 | 3.341352 | 35.880361 | 49.051193 | 11.767813 | 4.05 | 0 | SOIL LAYER |
| Slice 28 | 29.5 | 3.6282227 | 33.06702 | 44.391051 | 10.117742 | 4.05 | 0 | SOIL LAYER |
| Slice 29 | 30.5 | 3.9608794 | 29.804656 | 38.849137 | 8.0810204 | 4.05 | 0 | SOIL LAYER |
| Slice 30 | 31.5 | 4.3412916 | 26.073953 | 32.35569 | 5.6125766 | 4.05 | 0 | SOIL LAYER |
| Slice 31 | 32.5 | 4.7718535 | 21.851433 | 24.82331 | 2.6552983 | 4.05 | 0 | SOIL LAYER |

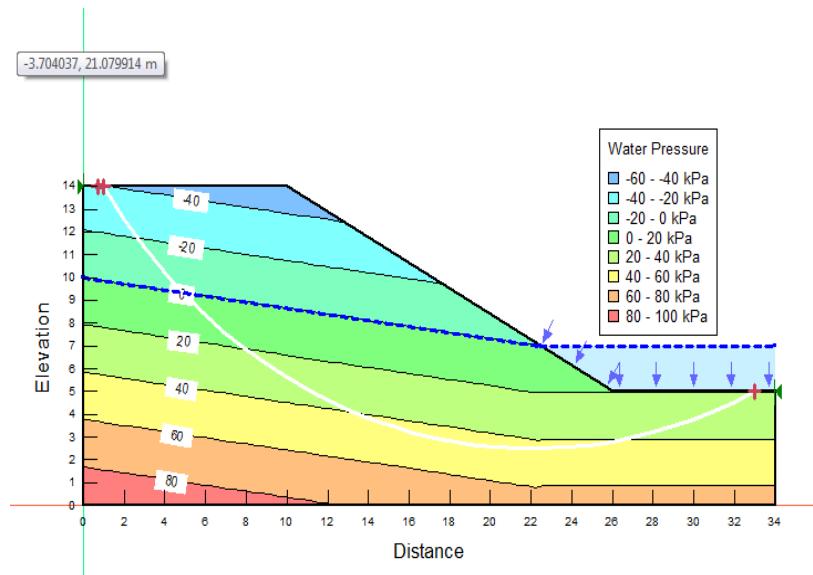


Figure5.5:Pore pressure through piezometric line (DTU region sample slope/W with Janbu method)

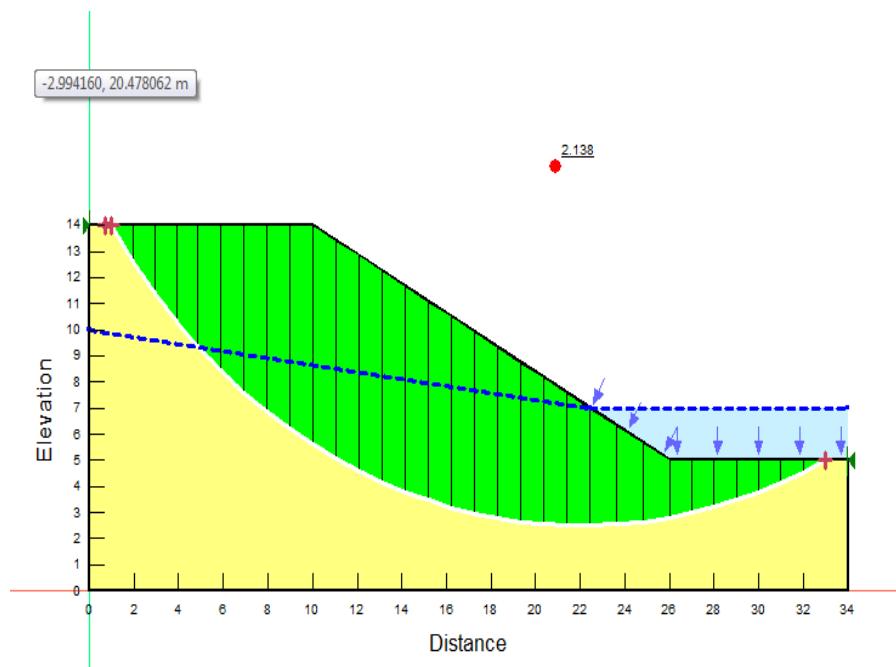


Figure5.6 : Factor of safety and slip surface results from Janbu analysis on DTU soil

4.5.4 Slope/W analysis on DTU soil with Ordinary Method

File Information

File Version: 9.01
Revision Number: 1
Date: 06/25/2020
Time: 12:46:28 AM
Tool Version: 9.1.1.16749
File Name: SLOPE W DTU ORDINARY.gsz
Directory: C:\Users\Sys\Desktop\Major project content\Geoslope DTU soil Content\
Last Solved Date: 06/25/2020
Last Solved Time: 12:46:32 AM

Project Settings

Unit System: International System of Units (SI)

Analysis Settings

Slope Stability

Kind: SLOPE/W
Method: Ordinary
Settings
PWP Conditions from: Piezometric Line
Apply Phreatic Correction: Yes
Use Staged Rapid Drawdown: No
Unit Weight of Water: 9.807 kN/m³

Slip Surface

Direction of movement: Left to Right
Use Passive Mode: No
Slip Surface Option: Entry and Exit
Critical slip surfaces saved: 1
Optimize Critical Slip Surface Location: No
Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

Geometry Settings
Minimum Slip Surface Depth: 0.1 m
Number of Slices: 30
Factor of Safety Convergence Settings
Maximum Number of Iterations: 2,000
Tolerable difference in F of S: 0.01

Materials

SOIL LAYER

Model: Mohr-Coulomb

Unit Weight: 16.57 kN/m³

Cohesion': 4.05 kPa

Phi': 41.78 °

Phi-B: 0 °

Pore Water Pressure

Piezometric Line: 1

Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (0.7, 14) m

Left-Zone Right Coordinate: (1, 14) m

Left-Zone Increment: 4

Right Type: Point

Right Coordinate: (33, 5) m

Right-Zone Increment: 8

Radius Increments: 4

Slip Surface Limits

Left Coordinate: (0, 14) m

Right Coordinate: (34, 5) m

Slip Results

Slip Surfaces Analysed: 20 of 25 converged

Current Slip Surface

Slip Surface: 23

Factor of Safety: 2.140

Volume: 152.26374 m³

Weight: 2,523.0101 kN

Resisting Moment: 37,711.895 kN·m

Activating Moment: 17,622.202 kN·m

Slip Rank: 1 of 25 slip surfaces

Exit: (33, 5) m

Entry: (1, 14) m

Radius: 25.087975 m

Centr: (22.087975, 27.590578) m

Slip Slice

| | X(m) | Y(m) | PWP(kPa) | Base Normal Stress(kPa) | Frictional Strength(kPa) | Cohesive Strength(kPa) | Suction Strength(kPa) | Base Material |
|----------|-----------|-----------|------------|-------------------------|--------------------------|------------------------|-----------------------|---------------|
| Slice 1 | 1.4829265 | 13.303515 | -33.738677 | 3.7470095 | 3.3478604 | 4.05 | 0 | SOIL LAYER |
| Slice 2 | 2.4487794 | 11.998745 | -22.411246 | 12.820489 | 11.45479 | 4.05 | 0 | SOIL LAYER |
| Slice 3 | 3.4146323 | 10.851721 | -12.603689 | 23.242205 | 20.766336 | 4.05 | 0 | SOIL LAYER |
| Slice 4 | 4.3804852 | 9.8314613 | -4.0174768 | 34.636888 | 30.947203 | 4.05 | 0 | SOIL LAYER |
| Slice 5 | 5.3770705 | 8.890909 | 3.7611832 | 48.738512 | 40.186131 | 4.05 | 0 | SOIL LAYER |
| Slice 6 | 6.4043882 | 8.0202353 | 10.826994 | 64.56943 | 48.017537 | 4.05 | 0 | SOIL LAYER |
| Slice 7 | 7.4317058 | 7.2386837 | 17.034126 | 79.592097 | 55.894 | 4.05 | 0 | SOIL LAYER |
| Slice 8 | 8.4590235 | 6.5362725 | 22.478752 | 93.7918 | 63.716445 | 4.05 | 0 | SOIL LAYER |
| Slice 9 | 9.4863412 | 5.9052745 | 27.235319 | 107.14472 | 71.39707 | 4.05 | 0 | SOIL LAYER |
| Slice 10 | 10.518517 | 5.337205 | 31.379324 | 115.87189 | 75.492016 | 4.05 | 0 | SOIL LAYER |
| Slice 11 | 11.55555 | 4.8277111 | 34.952705 | 119.40539 | 75.456381 | 4.05 | 0 | SOIL LAYER |
| Slice 12 | 12.592583 | 4.3757077 | 37.972173 | 121.35943 | 74.504448 | 4.05 | 0 | SOIL LAYER |
| Slice 13 | 13.629617 | 3.9778839 | 40.469627 | 121.80015 | 72.666814 | 4.05 | 0 | SOIL LAYER |
| Slice 14 | 14.66665 | 3.6315341 | 42.471137 | 120.79461 | 69.980088 | 4.05 | 0 | SOIL LAYER |
| Slice 15 | 15.703683 | 3.334448 | 43.997997 | 118.41125 | 66.486405 | 4.05 | 0 | SOIL LAYER |
| Slice 16 | 16.740717 | 3.0848302 | 45.067507 | 114.72029 | 62.233036 | 4.05 | 0 | SOIL LAYER |
| Slice 17 | 17.77775 | 2.8812391 | 45.693556 | 109.79391 | 57.272083 | 4.05 | 0 | SOIL LAYER |
| Slice 18 | 18.814783 | 2.7225422 | 45.887056 | 103.7065 | 51.660239 | 4.05 | 0 | SOIL LAYER |
| Slice 19 | 19.851817 | 2.6078822 | 45.656266 | 96.534679 | 45.458604 | 4.05 | 0 | SOIL LAYER |
| Slice 20 | 20.88885 | 2.5366535 | 45.007021 | 88.357458 | 38.732544 | 4.05 | 0 | SOIL LAYER |
| Slice 21 | 21.925883 | 2.5084855 | 43.942892 | 79.256234 | 31.551597 | 4.05 | 0 | SOIL LAYER |
| Slice 22 | 23.037015 | 2.5275747 | 43.861075 | 71.744232 | 24.912911 | 4.05 | 0 | SOIL LAYER |
| Slice 23 | 24.222222 | 2.6006247 | 43.144674 | 65.500462 | 19.974344 | 4.05 | 0 | SOIL LAYER |
| Slice 24 | 25.407407 | 2.7303598 | 41.872361 | 57.961792 | 14.375508 | 4.05 | 0 | SOIL LAYER |
| Slice 25 | 26.5 | 2.8988272 | 40.220202 | 53.990767 | 12.303659 | 4.05 | 0 | SOIL LAYER |
| Slice 26 | 27.5 | 3.0986552 | 38.260489 | 50.520639 | 10.954141 | 4.05 | 0 | SOIL LAYER |
| Slice 27 | 28.5 | 3.341352 | 35.880361 | 46.364741 | 9.3675342 | 4.05 | 0 | SOIL LAYER |
| Slice 28 | 29.5 | 3.6282227 | 33.06702 | 41.53422 | 7.5652339 | 4.05 | 0 | SOIL LAYER |
| Slice 29 | 30.5 | 3.9608794 | 29.804656 | 36.041788 | 5.5727227 | 4.05 | 0 | SOIL LAYER |
| Slice 30 | 31.5 | 4.3412916 | 26.073953 | 29.901508 | 3.4198257 | 4.05 | 0 | SOIL LAYER |
| Slice 31 | 32.5 | 4.7718535 | 21.851433 | 23.128499 | 1.1410265 | 4.05 | 0 | SOIL LAYER |

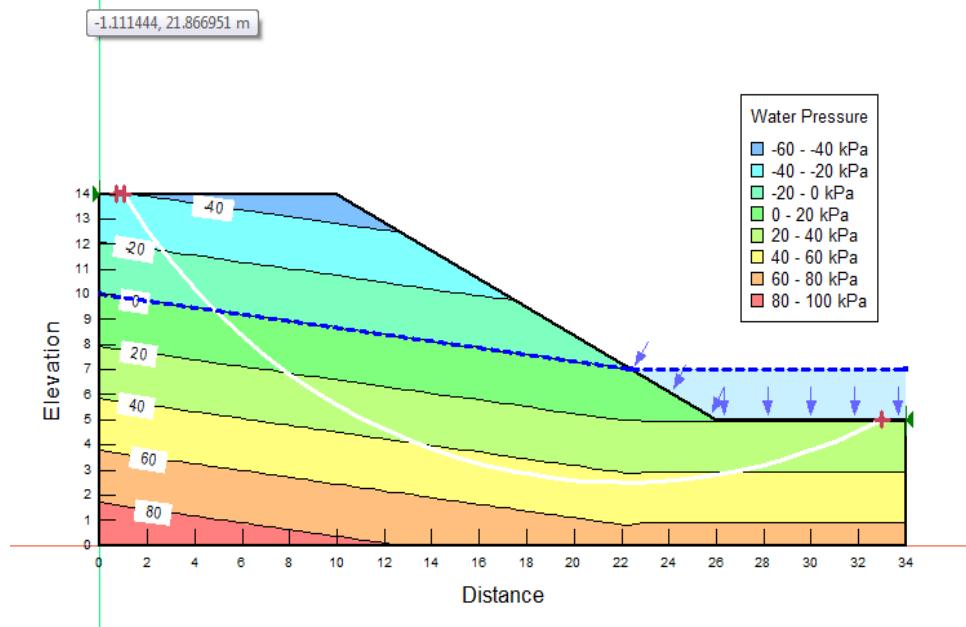


Figure5.7:Pore pressure through piezometric line (DTU region sample slope/W with Ordinary method)

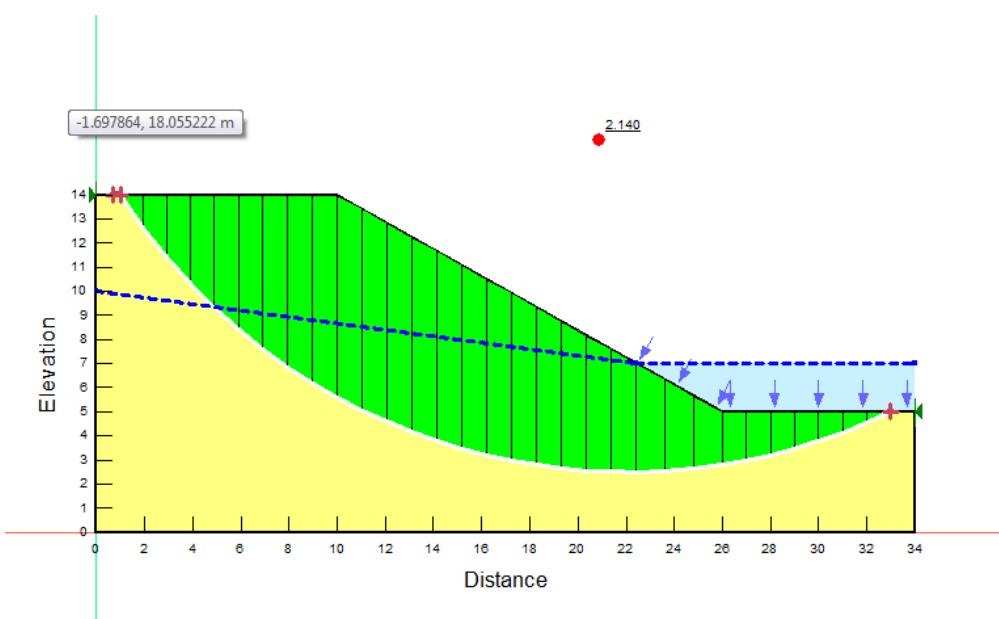


Figure5.8 : Factor of safety and slip surface results from Ordinary analysis on DTU soil

In Discussion for Morgenstern-Price method contains inter-slice forces and satisfy all equation of statics. The other methods(Bishop, Janbu and Ordinary) ignores inter-slice shear force for determining FOS of the slopes. Bishop assumes that normal or horizontal force explains the inter-slice forces. In Ordinary method that results in a linear factor of safety equation. In Ordinary method inter-slices force can be neglected due to they are parallel to base of each slice. In Janbu method a correction factor is used due to the effect of forces of the inter slice factor so this method gives the least stability to the structure . Bishop Method is very suitable for circular slip surfaces and Morgenstern price method is suitable for any type of Slip surface and Janbu is suitable for Shallow and Elongated slip surfaces. For circular slip surface Bishop method is best so it gives the maximum FOS And stability to the structure in the present study only. We can come to conclusion that DTU soil has lowest C value which gives the Lowest FOS according to the software Slope/W.

5. CONCLUSION

Table 4.1 : FOS obtained for different soil with different method

| | Punjab Soil | Jammu soil | Himachal soil | DTU Soil |
|------------------------|-------------|------------|---------------|----------|
| Φ | 36.86° | 64.6° | 48° | 41.78° |
| FOS(Morgenstern Price) | 4.309 | 6.624 | 4.552 | 2.319 |
| Bishop | 4.395 | 6.644 | 4.575 | 2.309 |
| Janbu | 3.854 | 6.146 | 4.173 | 2.138 |
| Ordinary | 3.936 | 6.149 | 4.246 | 2.140 |

- The results obtained from the software for F.O.S of safety of slope stability increases with the increase in Internal friction angle except in DTU soil, Due to its very less C value DTU soil has least FOS also.
- The FOS for Bishop method is obtained highest and for Janbu method obtained lowest.
- According to the theory of F.O.S here F.O.S >1.5 , so all the structures will be safe.

- All the detailed forces on each slice, failure mechanism, variety of the parameters distribution on the slip surfaces with respect to F.O.S. can be analyzed with the help of Geotechnical engineering software Slope/W (Geo-studio).
- Morgenstern-Price Method consider not only the normal and tangential equilibrium but also the moment equilibrium for each slice in circular and non-circular slip surfaces. It is solved for the factor of safety using the summation of forces tangential and normal to the base of a slice and the summation of moments about the center of the base of each slice.
- For calculating the F.O.S. of earth and rock slopes Slope/W software gives good results. Simple to simple and complex to complex problems can be solved for different slip shapes , Pore water pressure conditions, loading conditions and soil properties by using this software. For heterogeneous soil types ,complex stratigraphic and geometry of slip surface , variable pore water pressure conditions slope/W can take into consideration using limit equilibrium.
- After Performing all the method analysis on Slope/W software we come to conclusion that Bishop method gives highest FOS then Morgenstern-Price method then Ordinary method then Janbu method gives the least value of FOS.

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