

**ANALYSIS OF ENERGY LOSS ON STEPPED SPILLWAY USING
OBSTRUCTIONS THROUGH ANSYS**

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IN

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Submitted By

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I hereby certify that the Project Dissertation titled “**ANALYSIS OF ENERGY LOSS ON STEPPED SPILLWAY USING OBSTRUCTIONS THROUGH ANSYS**” by **Anshuman Gupta**, Roll No. **2K16/HFE/05**, Department of Civil Engineering, Delhi in partial fulfillment of the requirement for the award of the degree of Master of Technology, is a record of the project work carried out by the student under my supervision. To the best of my knowledge, this work has not been submitted in parts or full for any Degree or Diploma to this University or elsewhere.

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Date:

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First, I would like to thank my family, without their love and support over the years, none of this would have been possible. They have always been there for me and I am thankful for everything they have helped me achieve.

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ABSTRACT

In order to pass surplus water and sediment particles from upstream to downstream of dams, structure called spillway is used. Spillways are among important hydraulic structures which play a significant role in stability of dams. In some cases and when the slope is too steep to build a chute, in order to transfer water from upstream to downstream, a stepped spillway which is used which improves energy dissipation as well as . In the present study, in order to ascertain the effect of different parameters such as obstruction on every step, arrangement of obstruction and percentage area of projected area on energy dissipation in the simple stepped spillway, the models of stepped spillway was used with four different types:

- Spillway with no obstruction
- Spillway with 10% obstruction
- Spillway with 20% obstruction
- Spillway with 25% obstruction

Models were studied for various energy losses, velocity distribution and pressure distribution. And thereafter optimum area of the obstruction was observed. Initially different heads and velocity were taken into consideration and thereafter arrangement of the obstruction was also taken into consideration i.e. initially obstruction created was vertical but in subsequent stages horizontal obstruction was also taken into consideration.

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CHAPTER-1

INTRODUCTION

1.1 SCOPE OF THE PROJECT

Stepped block protection has significant potential as a economical method for the construction of spillways and the protection of banks from erosion by overtopping flow. Stepped spillways are structurally stable, resistant to heavy loads and increases the rate of energy dissipation on the spillway face hence reducing the need for a large energy dissipation basin at the spillway toe. It can also be constructed for use in diversion works during dam construction and for providing additional spillway capacity to existing dams. While constructing stepped spillway over embankment dam, the stepped block is used in conjunction with an under layer which includes a free draining medium and a lower zone which has the purpose of filtering seepage flow out of the subsoil and also protecting the subsoil from erosion by flow in the draining layer. Blocks are laid in stretcher bond configuration.

While stepped spillways are constructed from ancient times, the hydraulic design of stepped spillways has interestingly been an active topic for research over the past 50 years. Studies in laboratories have added to the knowledge base in the field and have provided a greater perspective on design questions. There have been several notable papers and books that have in particular discussed hydraulic design guidance for stepped channels operating in the nappe and skimming flow regimes; Essery & Horner (1978), Pravdivets & Bramley (1989) , Chanson (1994a), Christodoulou (1999), Boes & Minor (2000), Matos (2000), Chanson (2001), Chanson (2002), Boes & Hager (2003b), Frizell (2006), Gonzalez & Chanson (2007), Hunt (2008), Renna & Fratino (2010), Meireles et al. (2012), Matos & Meireles (2014), and Chanson et al. (2015)

These works are focused on the hydraulics of stepped spillways. Many more studies have been established that focus on specific features of the flow on stepped

spillways. This thesis will present generalized design guidance for stepped spillways with regards to their hydraulic characteristics and requirement. It will be made from experiences at Reclamation; however, studies and experience from all over the world will be included in order to provide a broad perspective of the design and use of stepped spillways today. In terms of construction, the last few decades have likely been the most amazing period in history for stepped spillways. The guide will reflect the current state-of-the-practice, realizing that with passing time, improvements and changes in design philosophy may certainly affect the appropriateness of some of these contents.

1.2 SUITABILITY

Energy dissipation below hydraulic structures is ensured generally by single – fall hydraulic jump type stilling basins, roller buckets or trajectory buckets. However, when the kinetic energy at the toe of the spillway is high. The tail water depths in the river are never satisfactory. Then first two devices cannot be used as in the case of high head dams. In narrow curved gorges consisting of fractured rocks, buckets cannot be used. In such situations, a system of cascading falls down the side of a valley, with a stilling basin in the downstream, can be used as an alternative spillway. Cascade spillways can be used for any type of dam irrespective of the material of construction.

The only disadvantage with stepped spillway is that at large discharges, as the jet is not aerated for some distance downstream of the spillway, low pressure may occur and lead to cavitation damage.

CHAPTER 2

LITERATURE REVIEW

Stepped overflow weirs and spillways have been used for few decades. Design of these structures went on simultaneously with dam-building which, in ancient times, lacked the presence of a rational approach (Smith, 1972). With advancement of technology and the ever-increasing need for safety, the knowledge and design of dams developed into the modern sophisticated designs. However, advancement in design of appurtenant structures, such as stepped spillways, appears to have lagged dam design, and only in recent years has it become an important topic of research. The difficulty in analyzing hydraulically rough surfaces like stepped spillways is the presence of highly turbulent, air entrained flow. Classic hydraulics theory and instrumentation can only approximate characteristics such as air entrainment, depth, and velocity of the two-phase flow.

In recent years, significant amounts of time and money have been devoted to laboratory model studies in order to study these characteristics. Following is a review of selected articles on research of stepped spillway flow. Selection of the articles was based on research conducted with physical scale models or of literature that has significantly contributed to the knowledge of stepped spillway flow.

3.1 Flow Regimes Defined

Research literature generally recognizes two types of flow behaviour on a stepped slope: Nappe flow regime and skimming flow regime. Research on the hydraulics of stepped spillway flow usually concentrates on one regime or the other with the type of regime dictated by a combination of step geometry and flow discharge.

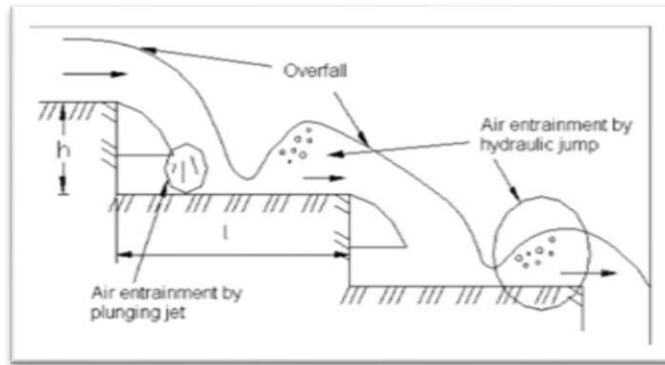


Fig.1: Nappe flow regime

Nappe flow normally occurs for low discharges and small flow depths while skimming flow occurs for high discharges and large flow depths. Nappe flow regime is distinguished by a series of plunges from one step to another with the formation of a nappe at each drop. This type of flow can be approximated by a series of single-step drop structures (Chamani and Rajaratnam 1994; Chanson 1993). The flow leaves the step as a free-falling jet and impinges on the tread of the next step. Energy dissipation occurs by jet breakup, jet mixing on the step, and the formation of a partially or fully developed hydraulic jump on the step (Chanson 1994; Rajaratnam 1990).

In the case of a fully developed hydraulic jump referred to as isolated nappe flow (Essery and Homer 1978; Peyras et. al. 1992), the flow passes through critical depth at the brink of the step forming a supercritical free-falling jet and returns to subcritical flow downstream of the jump. Flow with a partially developed hydraulic jump, referred to as nappe interference (Essery and Homer 1978) or partial nappe flow (Peyras 1992 et. al.), overshoots the next step and does not fully impinge on the step tread. For nappe flow to occur, the step horizontal tread needs to be greater than the water depth (Stephenson 1991; Lejeune et. al. 1994). In dam design, this would normally result in a relatively flat slope.

In skimming flow regime, water flows down the stepped face as a coherent stream, skimming over the steps and cushioned by the recirculating fluid trapped between them (Rajaratnam 1990). The skimming stream is supported by a pseudo-bottom formed by the external edges of the steps and horizontal-axis recirculating vortices. Energy dissipation occurs by momentum transfer, or the transmission of turbulent shear stress, between the skimming stream and the vortices (Chanson 1994).

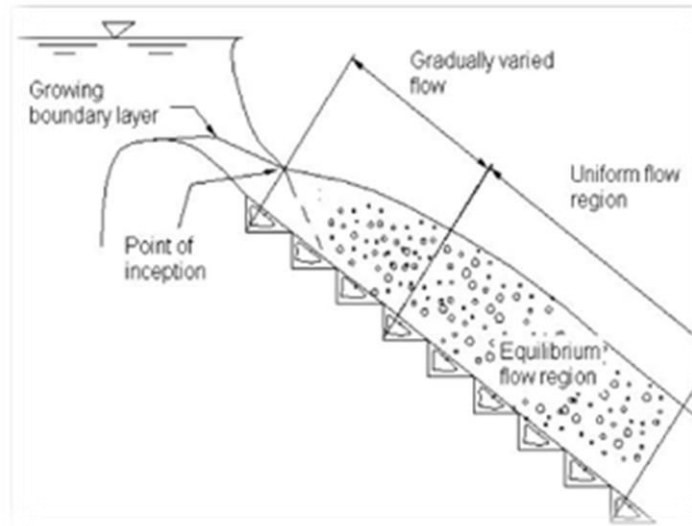


Fig.2: Skimming flow regime

Skimming flow is characterized by complete submergence of the steps with the development of fully aerated uniform flow in the downstream region (Figure 2.2). Along the upstream steps, a non-aerated flow region exists within which a turbulent boundary layer develops. Air entrainment in the flow begins where the boundary layer intersects the free surface, referred to as the point of inception. Downstream from the point of inception, the flow continues aerate and varies gradually in depth. The flow eventually becomes fully aerated, uniform flow in which the water depth, velocity, and air concentration are constant (Bindo et. al. 1993).

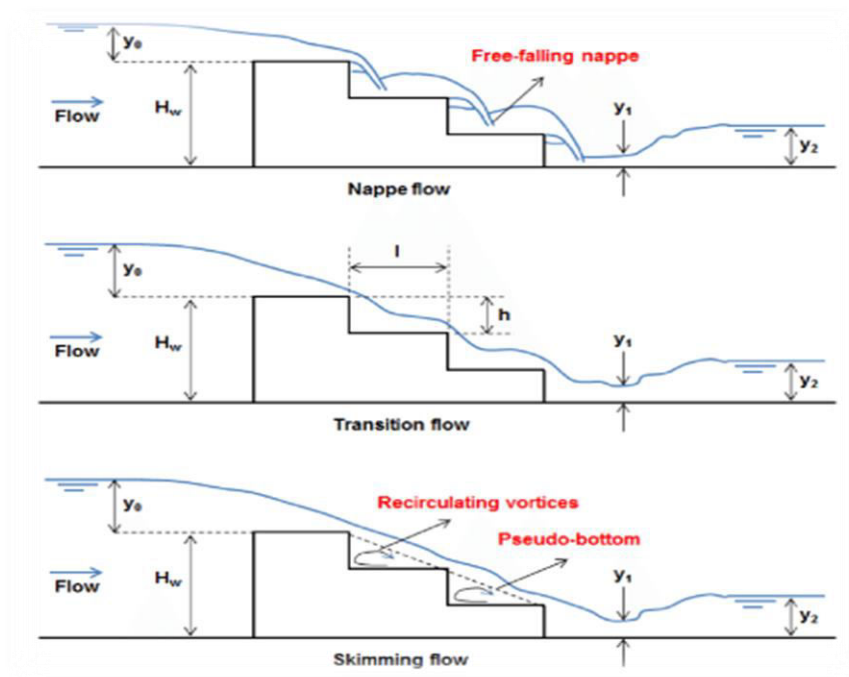


FIG.-3 FLOW REGIME

3.2 HYDRAULIC STUDIES

Essery and Horner et al. (1978)

Essery and Homer (1978), of the Construction Industry Research Information Association of the U.K., appear to be the earliest researchers to thoroughly investigate the hydraulics of stepped spillways. The research was conducted by means of model studies covering a wide range of step configurations and slopes. Numerous tests were carried out varying the parameters of step height-to-length ratio (slope) JUL , step length L , inclination of the step tread B , and the number of steps N . Model parameters spanned a wide range with overall slopes from 0.421 to 1.0, step length from 0.22 ft to 0.82 ft, step inclination from 0° to 20° , and the number of steps from 10 to 30.

For each test, velocity measurements were taken using Pitot tubes placed in the flow at a horizontal section downstream of the last step. Distance from the last step varied accordingly such that the flow was free of air entrainment. The most important characteristics of the flow at the horizontal section were described by specific energy E_s , and specific force F_s , given by:

$$E = y + \frac{v^2}{2g} \quad (3.1)$$

$$F_s = \frac{v^2 y}{g} + \frac{y^2}{2} \quad (3.2)$$

Where: y = Mean depth; V = Mean velocity; g = Acc. due to gravity

Sorensen et al. (1985)

Sorensen (1985) conducted a model study to evaluate the proposed design of a stepped spillway for the new Monksville Dam in New Jersey. The profile of the spillway was a modification of the Waterways Experiment Station (WES) ogee crest profile. From the crest to the point of tangency, the spillway face followed the WES profile. Below the point of tangency, the spillway had a constant slope of 0.78H:IV. Steps were fit into the spillway in such a manner that the envelope of their tips followed the WES profile and the downstream slope.

The prototype concrete dam and spillway were designed for 2.00 ft vertical by 1.56 ft horizontal steps below the point of tangency. Above the point of tangency, step sizes decreased in transition to the standard non-stepped ogee profile. Three scale models of the Monks Ville Dam spillway were tested. Model A consisted of a 1:10 scale model of the upper 22.75 ft of the spillway tested to evaluate the flow transition over the spillway crest and the first several steps. The model extended down to seven steps below the point of tangency. Model B was a 1:25 scale model of the entire, standard, non-stepped WES profile spillway. This model was tested to provide comparison data. Model C was a 1:25 scale model of the entire stepped spillway profile. All model tests were conducted in a 1.0 ft wide flume with a maximum discharge of just less than 3.0 cfs.

Measurements of flow depth were made at several locations along the spillway for each model test over a range of discharges. When air entrainment was present, the flow depths were estimated taking into account the bulk of the flow. Spillway discharges ranged from a minimum of 0.056 cfs/ft to a maximum of 2.53 cfs/ft with corresponding upstream head measurements of 0.063 ft and 0.710 ft, respectively. Average flow velocities were calculated from continuity. It was noted that some of the velocities were checked with a stagnation tube and measurements were reported to yield results within 10-15% of the values calculated from continuity. In addition, scaled velocities from model B were 15-20% higher than the prototype data. Proposed reasoning was that air entrainment was not present in the flow during the testing of model B and in the prototype, air entrainment would be expected. This scaling effect was described to be the primary cause for the velocity differences.

It was found that the kinetic energy of the flow at the stepped spillway toe varied from about 6-12% of the energy at the standard spillway toe for the range of model discharges. For the prototype design, toe velocities were scaled up using Froude scaling ratios and velocities for model B were compared with prototype velocities found on similar spillways using "experience" data from Bradley and Peterka (1957). It was estimated that the stepped spillway for the Monksville dam may provide up to 84% kinetic energy dissipation at design discharges. Sorensen also recorded the step number, from the top, at which air entrainment commenced for each run. It was noted that typically, the depth decreased as the flow descended from the crest to the point at which

air entrainment commenced. Beyond that point, the depth continually increased due to bulking of the flow by air entrainment.

Houston et al. (1987)

The U.S. Bureau of Reclamation conducted hydraulic model studies for design of the spillway for the Upper Stillwater dam in Utah. The dam incorporates Roller Compacted Concrete (RCC) construction techniques used for the dam into construction of the stepped spillway. The principle objective of the study was to design and analyze the configuration of the stepped spillway to provide information on sizing the stilling basin. Providing increased energy dissipation using steps resulted in reduction in size and cost of the stilling basin. Several sectional models of the spillway were tested ranging in scale from 1:5 to 1:10.

The final spillway design follows the theoretical nappe shape for an ogee crest. Several small steps began at the crest and gradually protruded into the profile downstream. The profile intersected a point of tangency where the slope became constant at 0.32H: 1V. Following the shape of the dam, the slope changed to 0.6H: 1V approximately one-third of the full distance down the face. The beginning steps varied in size and were determined based on model results. Step size was selected to prevent the jet produced from a protruding step from springing free of the spillway. The final design maintained a uniform flow against the spillway face. The stilling basin was designed using the model of the final spillway design. Based on stilling basin velocities at the design discharge, it was estimated that 72% energy dissipation was provided by the spillway.

Rajaratnam et al. (1990)

Rajaratnam (1990) presented a method for predicting shear stress and frictional energy loss for a skimming flow regime. It was proposed that the average Reynolds shear stress between the skimming stream and the recirculating fluid underneath can be estimated by finding the coefficient of fluid friction for a given set of flow conditions.

For a stepped spillway of constant slope $S_0 = \sin\alpha$ and fully developed flow with a constant mean velocity V_0 , and normal depth y_0 , the shear stress may given by:

$$\tau = y_0 \gamma \sin\alpha \quad (3.3)$$

Where: γ = weight per unit volume of water; τ = average Reynolds shear stress between the skimming flow and the recirculating fluid.

It was also assumed that the turbulent shear stress could be approximated by:

$$\tau = \frac{C_f(\rho V_0^2)}{2} \quad (3.4)$$

Where: C_f = coefficient of fluid friction; ρ = mass density of water.

Rajaratnam evaluated values of C_f for skimming flow using experimental data from Sorensen (1985) on a 1:25 scale model of Monksville dam. Using the experimental data from Sorensen's model test, Cl-C8, Rajaratnam found vary from 0.11 to 0.20 with an average value of 0.18. He states that this is an estimate due to the aeration occurring in the flow and that flow depths measured by Sorensen are approximate. An estimate of the energy loss for skimming flow on a stepped spillway was found by comparing energy loss caused by the steps E , to that caused by a smooth spillway E' given by:

$$\Delta E = E' - E$$

Relative energy loss was defined as $\Delta E/E'$ and is given by the expression:

$$\frac{\Delta E}{E'} = \frac{(1-A) + \frac{F_0'^2}{2} \frac{(A^2-1)}{A^2}}{1 + \frac{F_0'^2}{2}} \quad (3.5)$$

$$\& A = (C_f/C_f')^{1/3}$$

Where: C_f' = coefficient of skin friction for a smooth spillway.

F_0' = Froude number at the toe of a smooth spillway.

Taking, $C_f \approx 0.18$, $C_f' \approx 0.0065$, $A \approx 3$, and for a relatively large value of F_0' , $\Delta E/E'$ is approximately equal to $(A^2-1)/A^2$, which further reduces to a value of 8/9 or 89%. It was concluded from this that a considerable energy loss could be produced by the steps. Rajaratnam also performed an analysis with data from Essery and Homer (1978). He found that the type of flow regime existing on a stepped spillway depends on the ratio y_c/h , where Y_c is critical depth and h is the vertical height of the step. For a ratio of y/h greater than 0.8, skimming flow occurs and for a ratio less than 0.8, nappe flow exists.

Tozzi et.al. (1994)

Tozzi (1994) performed model studies on a 1:15 scale, 1V:0.75H slope, stepped spillway chute. Five step heights were tested in the model: 0.016, 0.033, 0.066, 0.098, and 0.197 ft. A method was proposed for determining the non-aerated flow depth, h , along the chute. This depth could then be used to find the residual energy at the spillway toe.

It was proposed to find the depth through computation of the gradually varied flow profile using the Standard Step Method. Determining the flow depth analytically requires determination of the Darcy-Weisbach friction factor f . In order to apply the friction factor concept to steps, the roughness height k was defined as the step height from the spillway chute to the step tip, perpendicular to the flow. The friction factor was first investigated using air flow in a closed conduit. For $h/k < 1.80$, f became constant at 0.163, for $h/k > 1.80$, the following relationship was found:

$$\frac{1}{\sqrt{f}} = 2.16 + 1.24 \log\left(\frac{h}{k}\right) \quad (3.6)$$

Similar relationships were found for slopes 1 V :2H and 1 V :6.69H.

Analytically determined depths were compared with experimentally determined depths and were found to differ by around 7% regardless of step height. The friction factor relationship appeared to adequately represent water flow. For water, the depth of flow was defined as the normal depth from the step tip to the point of maximum velocity (using a Pitot-static tube) above which the velocity was essentially constant.

The analytically computed non-aerated flow depth was found for the toe of the spillway for different flow-rates and step heights (roughness). The residual energy was then calculated by:

$$E_r = q^2 + q^2/2gh^2 \quad (3.7)$$

Results from the stepped test found the residual energy to be 25-50% of the total head for unit discharges varying between 53.8 and 129.2 cfs/ft. For comparison, the model tests were run with a hydraulically smooth chute. Results showed that the stepped spillway was able to dissipate three to four times more energy than the smooth chute.

Further investigations were carried out to define the development of the turbulent boundary layer. The thickness of the layer was considered the flow depth at the point of inception of aeration, as computed by the Standard Step Method.

The data was shown to fit well to an equation developed by Campbell (1963):

$$\frac{h}{L_a} = 0.08 \left(\frac{L_a}{K} \right) - 0.233 \quad (3.8)$$

Where: L_a = the total length of the spillway.

The steps at which inception of air entrainment took place, found by the analytical method, were compared to the model data from Sorensen (1985) and were found to check very closely.

CHAPTER-3

NUMERICAL SIMULATION

Weirs with finite crest width in the direction of flow are called Broad crested weirs. They are also called as weirs with finite crest width and find extensive applications as control structures and flow measuring devices.

How to calculate C_d for different conditions:

- For long-crested weir ($H_1/B_W < 0.1$)($B_W=L_{CREST}$)

$$C_D = 0.561(H_1/B_W)^{0.222} \quad (3.9)$$

- For broad crested weir ($0.1 < H_1/B_W < 0.35$)

$$C_D = 0.28(H_1/B_W) + 0.521 \quad (3.10)$$

- For narrow crested weir ($0.45 < H_1/B_W < \text{about } 1.5$)

$$C_D = 0.12(H_1/B_W) + 0.492 \quad (3.11)$$

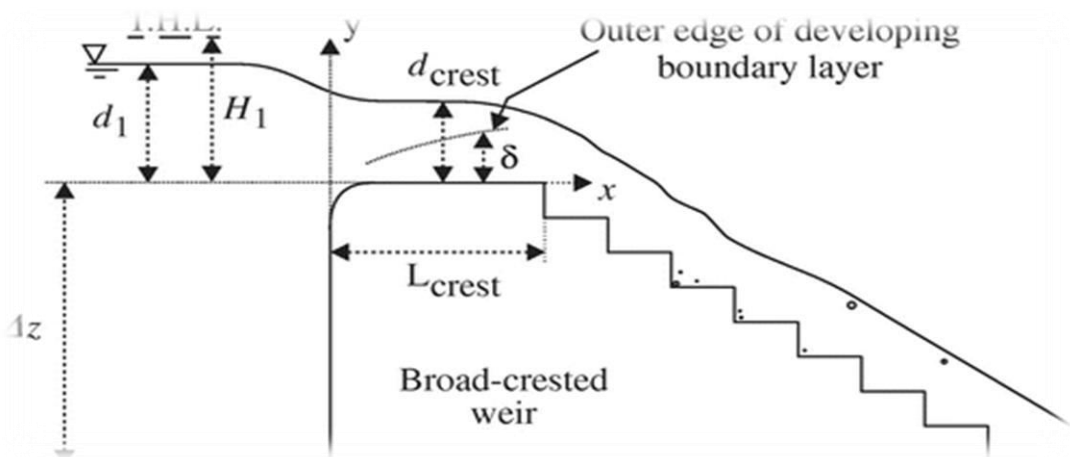


FIG.-4 DEFINITION SKETCH OF BROAD CRESTED WEIR

TO CALCULATE THE VELOCITY CORRESPONDING TO HEAD OF 3cm

L= transverse to the direction of flow

$$L=0.3\text{m} \quad B_w=0.16\text{m} \quad H_1=0.03\text{m}$$

$$\text{SO} \quad H_1/B_w < 0.35$$

$$C_D = 0.28(H_1/B_w) + 0.521$$

$$= 0.28 * 0.1875 + 0.521 = .52625$$

$$Q = \frac{2}{3} * C_D * \sqrt{2g} * L * (H_1)^{3/2} \quad (3.12)$$

$$= 0.666 * 0.52625 * 4.42718 * 0.3 * (0.03)^{3/2}$$

$$= 0.00239 \text{ m}^3/\text{s}$$

To calculate velocity

$$Q = A * V$$

$$0.00239 = (0.3 * 0.03) * V$$

$$V = 0.266 \text{ m/s}$$

TO CALCULATE THE VELOCITY CORRESPONDING TO HEAD OF 5cm

L= transverse to the direction of flow

$$L=0.3\text{m} \quad B_w=0.16\text{m} \quad H_1=0.05\text{m}$$

$$\text{SO} \quad H_1/B_w < 0.35$$

$$C_D = 0.28(H_1/B_w) + 0.521$$

$$= 0.28 * 0.3125 + 0.521 = 0.52975$$

$$Q = \frac{2}{3} * C_D * \sqrt{2g} * L * (H_1)^{3/2}$$

$$= 0.666 * 0.52975 * 4.42718 * 0.3 * (0.05)^{3/2}$$

$$= 0.00519 \text{ m}^3/\text{s}$$

To calculate velocity

$$Q = A * V$$

$$0.00519 = (0.3 * 0.05) * V$$

$$V = 0.3461 \text{ m/s}$$

TO CALCULATE THE VELOCITY CORRESPONDING TO HEAD OF 8cm

L= transverse to the direction of flow

$$L=0.3\text{m} \quad B_w=0.16\text{m} \quad H_1=0.08\text{m}$$

$$\text{SO} \quad H_1/B_w > 0.45$$

$$C_D = 0.12(H_1/B_w) + 0.492$$

$$= 0.12 * 0.2 + 0.492 = 0.516$$

$$Q = \frac{2}{3} * C_D * \sqrt{2g} * L * (H_1)^{3/2}$$

$$= 0.666 * 0.516 * 4.42718 * 0.3 * (0.08)^{3/2}$$

$$= 0.01023 \text{ m}^3/\text{s}$$

To calculate velocity

$$Q = A * V$$

$$0.01023 = (0.3 * 0.08) * V$$

$$V = 0.4263 \text{ m/s}$$

CHAPTER-4

SIMULATION STUDIES

CASE 1: Spillway without obstruction

GEOMETRY

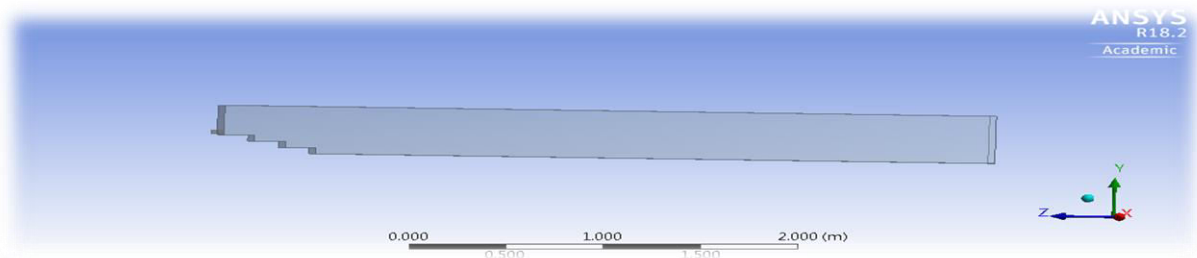


FIG.-5 GEOMETRY FOR NO OBSTRUCTION

MESHING

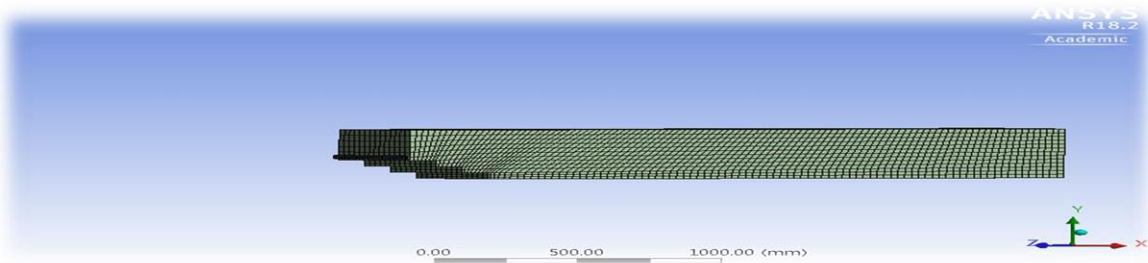


FIG.-6 MESHING FOR NO OBSTRUCTION

WALL SHEAR

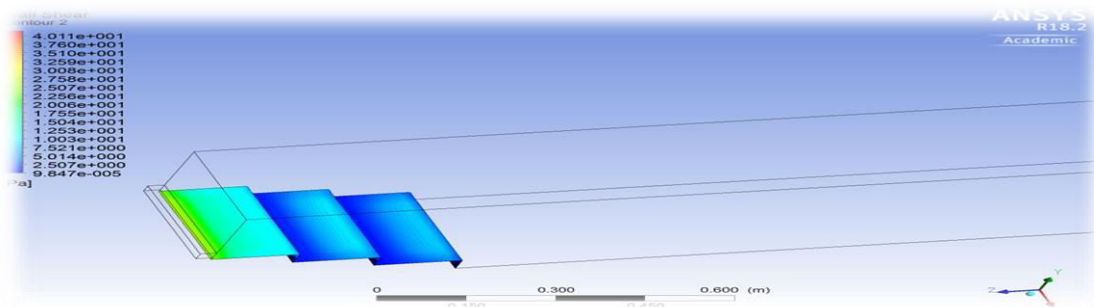


FIG.-7 WALL SHEAR FOR NO OBSTRUCTION

CASE II: Spillway with 10% obstruction

GEOMETRY

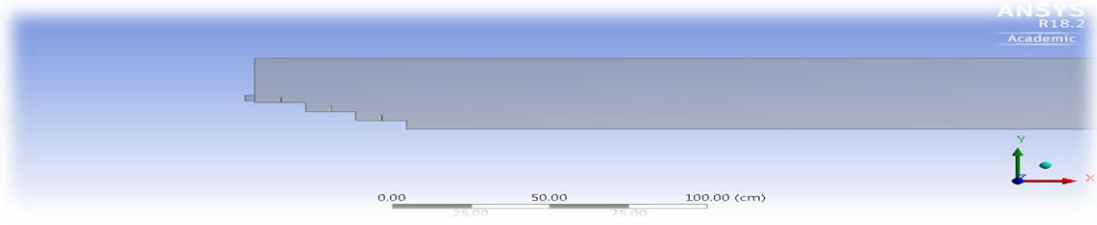


FIG.-8 GEOMETRY FOR 10% OBSTRUCTION

MESHING

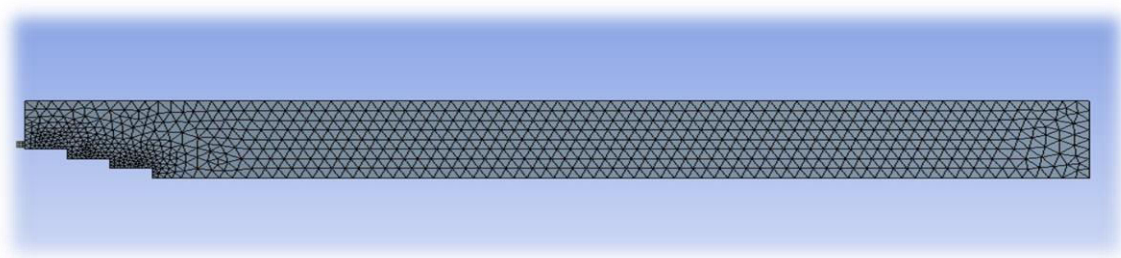


FIG.-9 MESHING FOR 10% OBSTRUCTION

WALL SHEAR

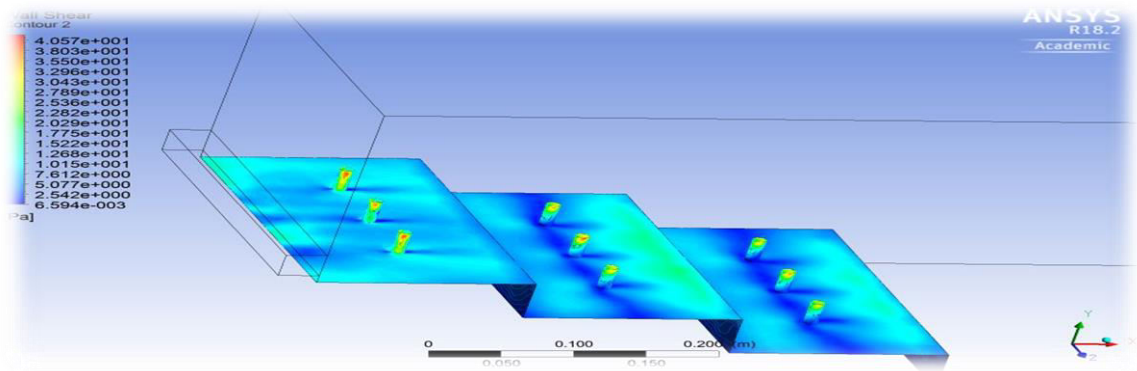


FIG.-10 WALL SHEAR FOR 10% OBSTRUCTION

STREAMLINES

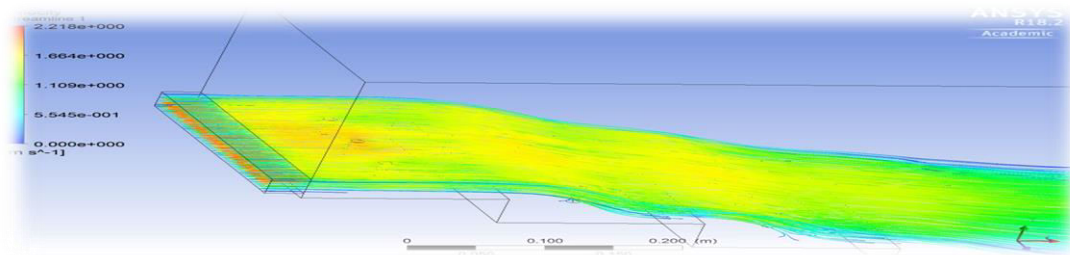


FIG.-11 STREAMLINES FOR 10% OBSTRUCTION

VECTOR

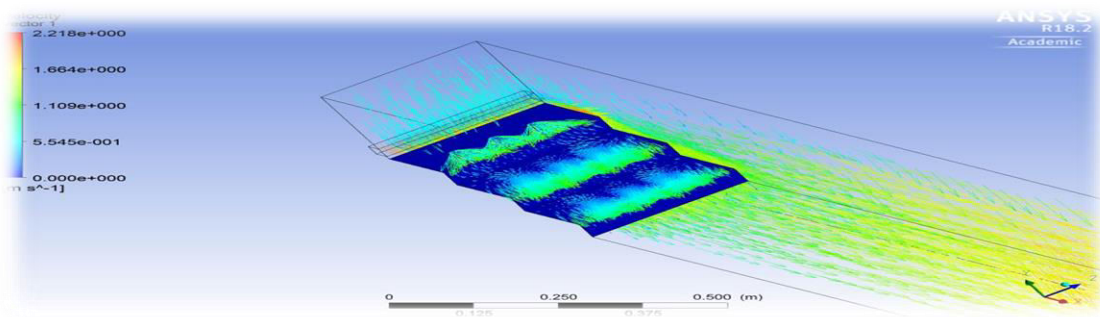


FIG.-12 VECTOR FOR 10% OBSTRUCTION

CASE III: Spillway with 20% obstruction

GEOMETRY

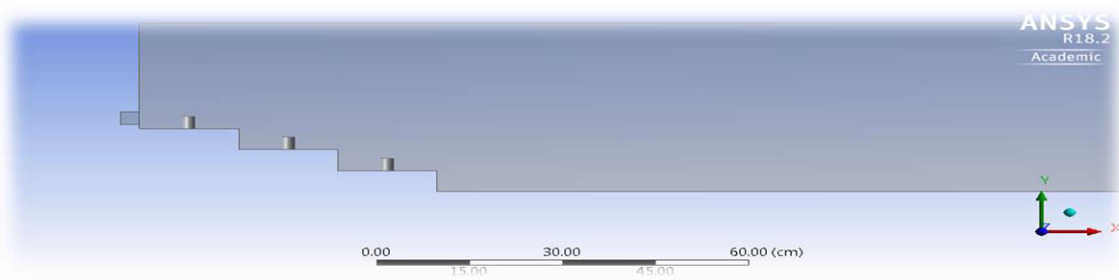


FIG.-13 GEOMETRY FOR 20% OBSTRUCTION

MESHING

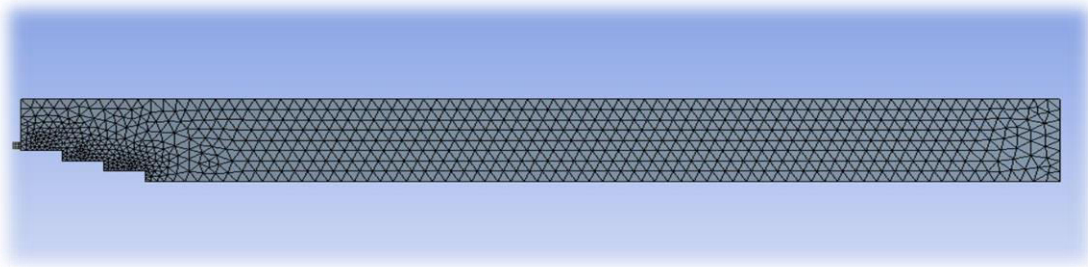


FIG.-14 MESHING FOR 20% OBSTRUCTION

STREAMLINE

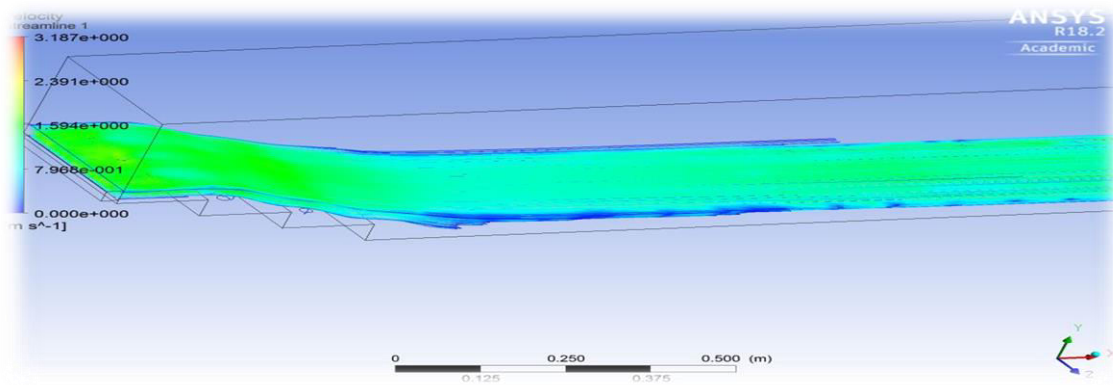


FIG.-15 STREAMLINE FOR 20% OBSTRUCTION

VECTOR

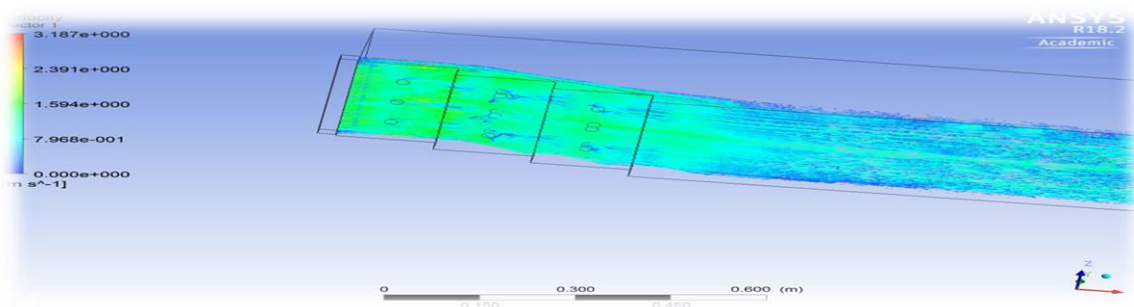


FIG.-16 VECTOR FOR 20% OBSTRUCTION

WALL SHEAR

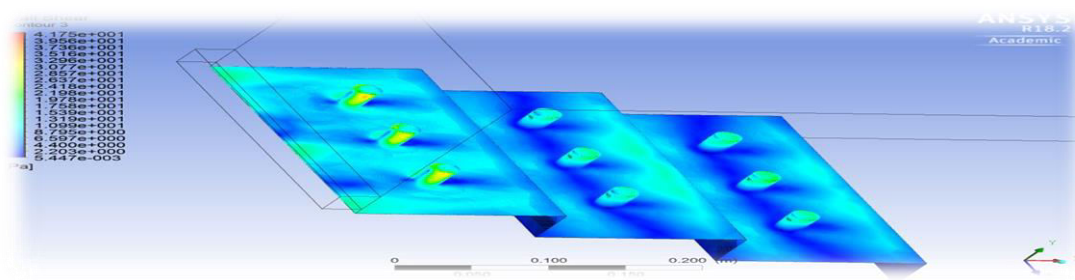


FIG.-17 WALL SHEAR FOR 20% OBSTRUCTION

VELOCITY

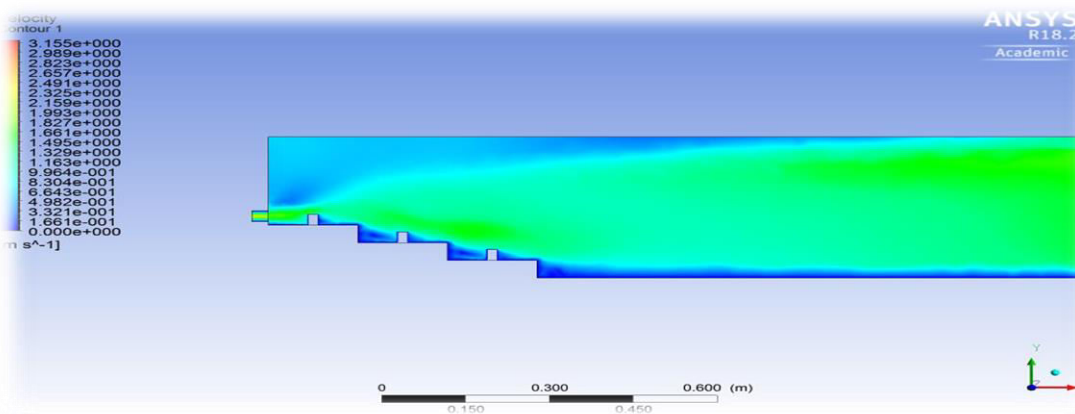


FIG.-18 VELOCITY FOR 20% OBSTRUCTION

CASE IV: Spillway with 30 % obstruction

GEOMETRY

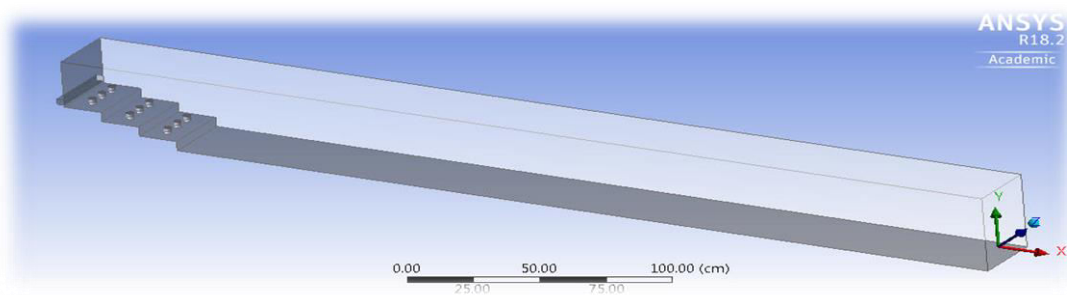


FIG.-19 GEOMETRY FOR 30% OBSTRUCTION

MESHING

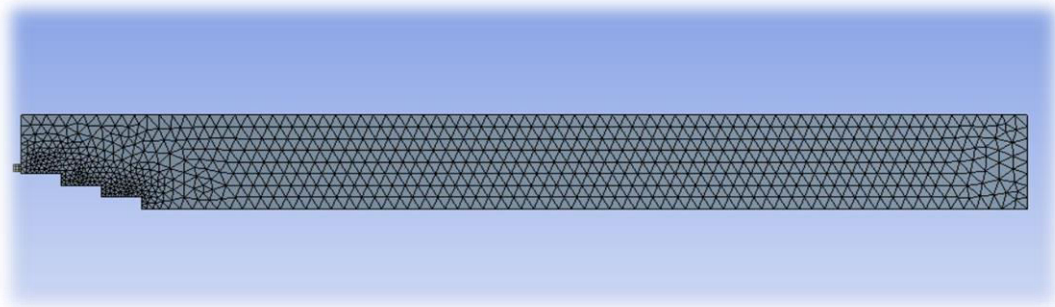
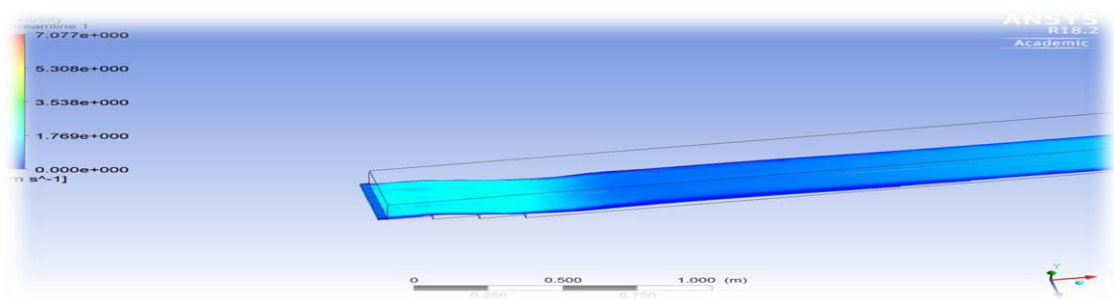


FIG.-20 MESHING FOR 30% OBSTRUCTION

STREAMLINES



21 STREAMLINES FOR 30% OBSTRUCTION

FIG.-

VECTOR

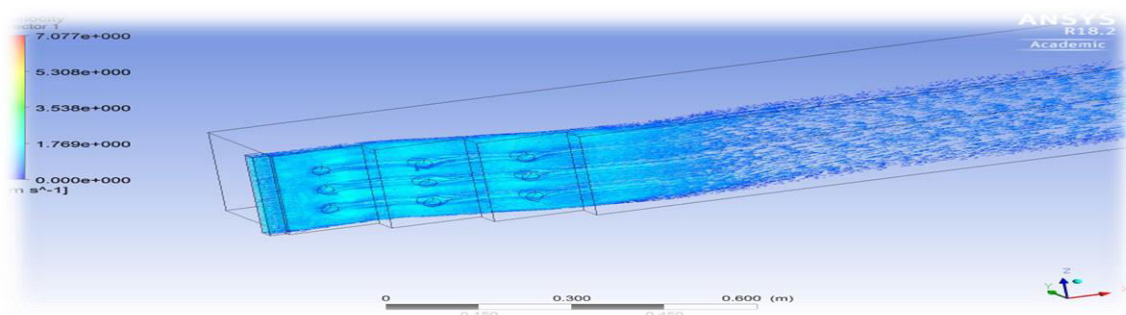


FIG.-22 VECTOR FOR 30% OBSTRUCTION

CHAPTER-5

RESULTS & DISCUSSIONS

WHERE Z=along the diection of flow

X=perpendicular to the direction of flow

Y=against the gravity

V=velocity measured along the direction of flow

VELOCITY HEAD= $V*V/2g$

$$= V*V/19.6$$

PRESSURE= Static pressure

PRESSURE HEAD= $P/9810$

DATUM HEAD=Distance from the bottom of the flume

USING BERNOULLI'S EQUATION:

PRESSURE HEAD+VELOCITY HEAD+DATUM HEAD=CONSTANT

$(E_1-E_0)/E_0$ =Energy difference

E_1 = Energy at the downstream before the hydraulic jump FORMATION.

E_0 = Energy at the upstream

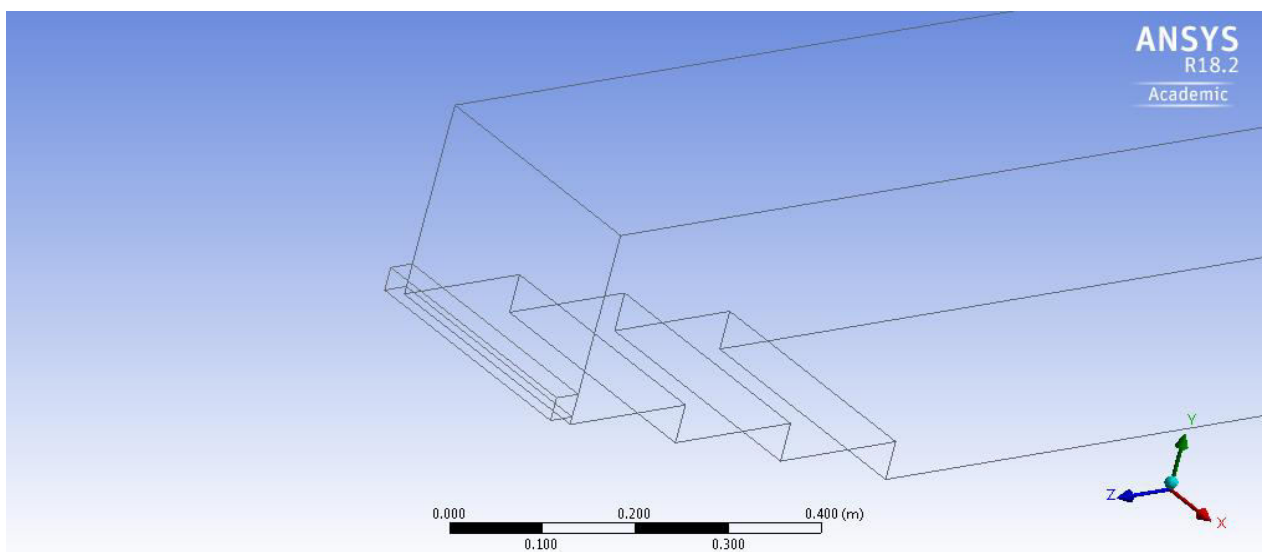


FIG.-23 PROJECTION OF AXIS

**TABLE-1 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=3cm
IN NO OBSTRUCTION**

WITHOUT OBSTRUCTION vertical (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.1419	0.001027327	1632.63	0.166425076	0.18	0.347452403	0.261615044
2	0.15	0.18	3.97	0.1216	0.000754416	1637.29	0.166900102	0.18	0.347654518	0.224188791
3	0.15	0.18	3.96	0.099	0.000500051	1640.21	0.167197757	0.18	0.347697808	0.182522124
4	0.15	0.18	3.95	0.0786	0.000315202	1643.11	0.167493374	0.18	0.347808576	0.144911504
5	0.15	0.18	3.94	0.0651	0.000216225	1643.98	0.167582059	0.18	0.347798284	0.120022124
6	0.15	0.18	3.93	0.0545	0.000151543	1643.7	0.167553517	0.18	0.34770506	0.100479351
7	0.15	0.18	3.92	0.0444	0.00010058	1643.43	0.167525994	0.18	0.347626573	0.081858407
8	0.15	0.18	3.91	0.0362	6.68592E-05	1642.9	0.167471967	0.18	0.347538827	0.066740413
9	0.15	0.18	3.9	0.0285	4.14413E-05	1642.35	0.167415902	0.18	0.347457343	0.052544248
10	0.15	0.18	3.89	0.0225	2.58291E-05	1642.23	0.16740367	0.18	0.347429499	0.041482301
11	0.15	0.18	3.88	0.0188	1.80327E-05	1642.75	0.167456677	0.18	0.34747471	0.034660767
12	0.15	0.18	3.87	0.0156	1.24163E-05	1643.26	0.167508665	0.18	0.347521081	0.028761062
13	0.15	0.18	3.86	0.0157	1.2576E-05	1645.08	0.16769419	0.18	0.347706766	0.028945428
14	0.15	0.18	3.85	0.0174	1.54469E-05	1646.93	0.167882773	0.18	0.34789822	0.032079646

TABLE-2 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=3cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION vertical (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.05	0.0258	3.39612E-05	3256.98	0.332006116	0.03	0.362040077	0.047566372
2	0.15	0.03	3.49	0.0284	4.1151E-05	3259.2	0.332232416	0.03	0.362273567	0.052359882
3	0.15	0.03	3.48	0.0353	6.3576E-05	3261.42	0.332458716	0.03	0.362522292	0.065081121
4	0.15	0.03	3.47	0.0411	8.61842E-05	3263.91	0.332712538	0.03	0.362798722	0.075774336
5	0.15	0.03	3.46	0.046	0.000107959	3266.52	0.332978593	0.03	0.363086552	0.08480826
6	0.15	0.03	3.45	0.0512	0.000133747	3269.14	0.333245668	0.03	0.363379415	0.09439528
7	0.15	0.03	3.44	0.0554	0.00015659	3272.44	0.333582059	0.03	0.363738649	0.102138643
8	0.15	0.03	3.43	0.0595	0.000180625	3275.8	0.333924567	0.03	0.364105192	0.10969764
9	0.15	0.03	3.42	0.0636	0.000206376	3279.18	0.334269113	0.03	0.364475489	0.117256637
10	0.15	0.03	3.41	0.0674	0.000231773	3282.84	0.334642202	0.03	0.364873975	0.124262537
11	0.15	0.03	3.4	0.0708	0.000255747	3286.84	0.335049949	0.03	0.365305696	0.130530973
12	0.15	0.03	3.39	0.0742	0.0002809	3290.81	0.335454638	0.03	0.365735538	0.13679941
13	0.15	0.03	3.38	0.0777	0.000308025	3294.78	0.335859327	0.03	0.366167352	0.143252212
14	0.15	0.03	3.37	0.0809	0.000333919	3298.79	0.336268094	0.03	0.366602013	0.149151917

**TABLE-3 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=3cm
IN 10% OBSTRUCTION**

WITH 10% OBSTRUCTION VERTICAL (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.1455	0.00108 0115	1507.03	0.15362 1814	0.18	0.33470 1929	0.23242 8115
2	0. 15	0. 18	3. 97	0.1386	0.00098 01	1501.23	0.15303 0581	0.18	0.33401 0681	0.22140 5751
3	0. 15	0. 18	3. 96	0.1408	0.00101 1461	1502.06	0.15311 5189	0.18	0.33412 665	0.22492 0128
4	0. 15	0. 18	3. 95	0.1471	0.00110 4001	1503.81	0.15329 3578	0.18	0.33439 7578	0.23498 4026
5	0. 15	0. 18	3. 94	0.1538	0.00120 6859	1507.15	0.15363 4047	0.18	0.33484 0906	0.24568 6901
6	0. 15	0. 18	3. 93	0.1464	0.00109 3518	1547.08	0.15770 4383	0.18	0.33879 7902	0.23386 5815
7	0. 15	0. 18	3. 92	0	0	0	0	0.18	0.18	0
8	0. 15	0. 18	3. 91	0.1622	0.00134 2288	1520.5	0.15499 4903	0.18	0.33633 7191	0.25910 5431
9	0. 15	0. 18	3. 9	0.1781	0.00161 8347	1567.27	0.15976 2487	0.18	0.34138 0835	0.28450 4792
10	0. 15	0. 18	3. 89	0.1768	0.00159 4808	1574.81	0.16053 1091	0.18	0.34212 5899	0.28242 8115
11	0. 15	0. 18	3. 88	0.1744	0.00155 1804	1575.54	0.16060 5505	0.18	0.34215 7309	0.27859 4249
12	0. 15	0. 18	3. 87	0.172	0.00150 9388	1575.38	0.16058 9195	0.18	0.34209 8582	0.27476 0383
13	0. 15	0. 18	3. 86	0.1716	0.00150 2376	1576.77	0.16073 0887	0.18	0.34223 3262	0.27412 1406
14	0. 15	0. 18	3. 85	0.1719	0.00150 7633	1579.74	0.16103 3639	0.18	0.34254 1272	0.27460 0639

TABLE- 4 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=3cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION VERTICAL (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0342	0.00174 4898	3267.3	0.33305 8104	0.03	0.36480 3002	0.05463 2588
2	0.15	0.03	3.49	0.0421	0.00214 7959	3279.58	0.33430 9888	0.03	0.36645 7847	0.06725 2396
3	0.15	0.03	3.48	0.0606	0.00309 1837	3275.71	0.33391 5392	0.03	0.36700 7229	0.09680 5112
4	0.15	0.03	3.47	0.0725	0.00369 898	3267.3	0.33305 8104	0.03	0.36675 7084	0.11581 4696
5	0.15	0.03	3.46	0.0772	0.00393 8776	3274.33	0.33377 472	0.03	0.36771 3495	0.12332 2684
6	0.15	0.03	3.45	0.08	0.00408 1633	3286.27	0.33499 1845	0.03	0.36907 3478	0.12779 5527
7	0.15	0.03	3.44	0.0824	0.00420 4082	3300.97	0.33649 0316	0.03	0.37069 4398	0.13162 9393
8	0.15	0.03	3.43	0.0872	0.00444 898	3306.11	0.33701 4271	0.03	0.37146 3251	0.13929 7125
9	0.15	0.03	3.42	0.093	0.00474 4898	3303.8	0.33677 8797	0.03	0.37152 3695	0.14856 23
10	0.15	0.03	3.41	0.0989	0.00504 5918	3301.48	0.33654 2304	0.03	0.37158 8222	0.15798 722
11	0.15	0.03	3.4	0.1035	0.00528 0612	3301.08	0.33650 1529	0.03	0.37178 2141	0.16533 5463
12	0.15	0.03	3.39	0.1044	0.00532 6531	3309.44	0.33735 3721	0.03	0.37268 0251	0.16677 3163
13	0.15	0.03	3.38	0.099	0.00505 102	3319.97	0.33842 7115	0.03	0.37347 8136	0.15814 6965
14	0.15	0.03	3.37	0.0937	0.00478 0612	3330.5	0.33950 051	0.03	0.37428 1122	0.14968 0511

**TABLE-5 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=3cm
IN 20% OBSTRUCTION**

WITH 20% OBSTRUCTION VERTICAL (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.1437	0.00105 3556	1705.53	0.17385 6269	0.18	0.35490 9825	0.22955 2716
2	0. 15	0. 18	3. 97	0.1385	0.00097 8686	1710.97	0.17441 0805	0.18	0.35538 9492	0.22124 6006
3	0. 15	0. 18	3. 96	0.1407	0.00101 0025	1716.42	0.17496 6361	0.18	0.35597 6386	0.22476 0383
4	0. 15	0. 18	3. 95	0.145	0.00107 2704	1722.42	0.17557 7982	0.18	0.35665 0686	0.23162 9393
5	0. 15	0. 18	3. 94	0.1429	0.00104 1858	1744.48	0.17782 6707	0.18	0.35886 8565	0.22827 476
6	0. 15	0. 18	3. 93	0.0013	8.62245 E-08	1945.98	0.19836 6972	0.18	0.37836 7059	0.00207 6677
7	0. 15	0. 18	3. 92	0	0	1802.25	0.18371 5596	0.18	0.36371 5596	0
8	0. 15	0. 18	3. 91	0.0005	1.27551 E-08	1615.16	0.16464 4241	0.18	0.34464 4253	0.00079 8722
9	0. 15	0. 18	3. 9	0.1778	0.00161 29	1772.28	0.18066 055	0.18	0.36227 345	0.28402 5559
10	0. 15	0. 18	3. 89	0.1932	0.00190 44	1791.53	0.18262 2834	0.18	0.36452 7234	0.30862 6198
11	0. 15	0. 18	3. 88	0.1992	0.00202 4522	1801.18	0.18360 6524	0.18	0.36563 1046	0.31821 0863
12	0. 15	0. 18	3. 87	0.2048	0.00213 9951	1795.39	0.18301 631	0.18	0.36515 6261	0.32715 655
13	0. 15	0. 18	3. 86	0.2064	0.00217 3518	1806.65	0.18416 4118	0.18	0.36633 7637	0.32971 246
14	0. 15	0. 18	3. 85	0.2139	0.00233 4347	1797.93	0.18327 5229	0.18	0.36560 9577	0.34169 3291

TABLE-6 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=3cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION VERTICAL (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0465	0.00237 2449	3417.41	0.34835 9837	0.03	0.38073 2286	0.07428 115
2	0.15	0.03	3.49	0.0724	0.00369 3878	3423.8	0.34901 1213	0.03	0.38270 5091	0.11565 4952
3	0.15	0.03	3.48	0.0925	0.00471 9388	3434.78	0.35013 0479	0.03	0.38484 9867	0.14776 3578
4	0.15	0.03	3.47	0.0993	0.00506 6327	3443.45	0.35101 4271	0.03	0.38608 0598	0.15862 6198
5	0.15	0.03	3.46	0.1089	0.00555 6122	3448.96	0.35157 5943	0.03	0.38713 2065	0.17396 1661
6	0.15	0.03	3.45	0.1206	0.00615 3061	3454.7	0.35216 106	0.03	0.38831 4121	0.19265 1757
7	0.15	0.03	3.44	0.1241	0.00633 1633	3466.68	0.35338 2263	0.03	0.38971 3896	0.19824 2812
8	0.15	0.03	3.43	0.1335	0.00681 1224	3467.83	0.35349 949	0.03	0.39031 0715	0.21325 8786
9	0.15	0.03	3.42	0.1424	0.00726 5306	3467.51	0.35346 6871	0.03	0.39073 2177	0.22747 6038
10	0.15	0.03	3.41	0.1478	0.00754 0816	3468	0.35351 682	0.03	0.39105 7636	0.23610 2236
11	0.15	0.03	3.4	0.1558	0.00794 898	3468.98	0.35361 6718	0.03	0.39156 5697	0.24888 1789
12	0.15	0.03	3.39	0.1637	0.00835 2041	3469.76	0.35369 6228	0.03	0.39204 8269	0.26150 1597
13	0.15	0.03	3.38	0.1679	0.00856 6327	3474.53	0.35418 2467	0.03	0.39274 8793	0.26821 0863
14	0.15	0.03	3.37	0.1717	0.00876 0204	3481.04	0.35484 6075	0.03	0.39360 628	0.27428 115

**TABLE-7 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=3cm
IN 30% OBSTRUCTION**

WITH 30% OBSTRUCTION VERTICAL (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.1341	0.00091 749	1565	0.15953 1091	0.18	0.34044 8581	0.21421 7252
2	0. 15	0. 18	3. 97	0.1147	0.00067 1229	1570.14	0.16005 5046	0.18	0.34072 6275	0.18322 6837
3	0. 15	0. 18	3. 96	0.1025		1565.68	0.15960 0408	0.18	0.33960 0408	0.16373 8019
4	0. 15	0. 18	3. 95	0.0924	0.00043 56	1567.44	0.15977 9817	0.18	0.34021 5417	0.14760 3834
5	0. 15	0. 18	3. 94	0.0782	0.00031 2002	1575.95	0.16064 7299	0.18	0.34095 9301	0.12492 0128
6	0. 15	0. 18	3. 93	0	0	1562.93	0.15932 0082	0.18	0.33932 0082	0
7	0. 15	0. 18	3. 92	0	0	1569.67	0.16000 7136	0.18	0.34000 7136	0
8	0. 15	0. 18	3. 91	0	0	1584.98	0.16156 7788	0.18	0.34156 7788	0
9	0. 15	0. 18	3. 9	0.0901	0.00041 4184	1552.22	0.15822 8338	0.18	0.33864 2523	0.14392 9712
10	0. 15	0. 18	3. 89	0.1121	0.00064 1143	1576.53	0.16070 6422	0.18	0.34134 7565	0.17907 3482
11	0. 15	0. 18	3. 88	0.117	0.00069 8418	1589.35	0.16201 3252	0.18	0.34271 167	0.18690 0958
12	0. 15	0. 18	3. 87	0.1208	0.00074 4522	1589.03	0.16198 0632	0.18	0.34272 5154	0.19297 1246
13	0. 15	0. 18	3. 86	0.1232	0.00077 44	1588.95	0.16197 2477	0.18	0.34274 6877	0.19680 5112
14	0. 15	0. 18	3. 85	0.1255	0.00080 3584	1595.8	0.16267 0744	0.18	0.34347 4328	0.20047 9233

TABLE-8 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=3cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION VERTICAL (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.05	0.0299	0.00152551	3260.39	0.332353721	0.03	0.363879231	0.047763578
2	0.15	0.03	3.49	0.042	0.002142857	3261.05	0.332420999	0.03	0.364563856	0.067092652
3	0.15	0.03	3.48	0.0541	0.002760204	3261.4	0.332456677	0.03	0.365216881	0.086421725
4	0.15	0.03	3.47	0.0638	0.003255102	3255.52	0.331857288	0.03	0.365112391	0.101916933
5	0.15	0.03	3.46	0.0751	0.003831633	3256.03	0.331909276	0.03	0.365740909	0.119968051
6	0.15	0.03	3.45	0.0757	0.003862245	3260.43	0.332357798	0.03	0.366220043	0.120926518
7	0.15	0.03	3.44	0.0804	0.004102041	3266.97	0.333024465	0.03	0.367126506	0.128434505
8	0.15	0.03	3.43	0.0822	0.004193878	3279.74	0.334326198	0.03	0.368520075	0.131309904
9	0.15	0.03	3.42	0.085	0.004336735	3294.17	0.335797146	0.03	0.37013388	0.135782748
10	0.15	0.03	3.41	0.0863	0.004403061	3308.69	0.337277268	0.03	0.371680329	0.137859425
11	0.15	0.03	3.4	0.0901	0.004596939	3310.46	0.337457696	0.03	0.372054635	0.143929712
12	0.15	0.03	3.39	0.0933	0.004760204	3311.13	0.337525994	0.03	0.372286198	0.149041534
13	0.15	0.03	3.38	0.0943	0.004811224	3313.1	0.337726809	0.03	0.372538034	0.150638978
14	0.15	0.03	3.37	0.0953	0.004862245	3315.07	0.337927625	0.03	0.37278987	0.152236422

**TABLE-9 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=5cm
IN NO OBSTRUCTION**

WITHOUT OBSTRUCTION VERTICAL (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.2327	0.00276 2719	1671.76	0.17041 3863	0.18	0.35317 6582	0.42901 9174
2	0.15	0.18	3.97	0.2079	0.00220 5225	1680.02	0.17125 5861	0.18	0.35346 1086	0.38329 646
3	0.15	0.18	3.96	0.1802	0.00165 6737	1686.68	0.17193 476	0.18	0.35359 1497	0.33222 7139
4	0.15	0.18	3.95	0.1534	0.00120 059	1693.34	0.17261 366	0.18	0.35381 4249	0.28281 7109
5	0.15	0.18	3.94	0.138	0.00097 1633	1696.67	0.17295 3109	0.18	0.35392 4742	0.25442 4779
6	0.15	0.18	3.93	0.1288	0.00084 64	1698.23	0.17311 213	0.18	0.35395 853	0.23746 3127
7	0.15	0.18	3.92	0.1205	0.00074 0829	1699.85	0.17327 7268	0.18	0.35401 8097	0.22216 0767
8	0.15	0.18	3.91	0.1177	0.00070 6801	1702.71	0.17356 8807	0.18	0.35427 5608	0.21699 8525
9	0.15	0.18	3.9	0.1156	0.00068 1804	1705.58	0.17386 1366	0.18	0.35454 317	0.21312 6844
10	0.15	0.18	3.89	0.1152	0.00067 7094	1709.11	0.17422 1203	0.18	0.35489 8297	0.21238 9381
11	0.15	0.18	3.88	0.1168	0.00069 6033	1713.65	0.17468 3996	0.18	0.35538 0029	0.21533 9233
12	0.15	0.18	3.87	0.1187	0.00071 8862	1718.18	0.17514 577	0.18	0.35586 4631	0.21884 2183
13	0.15	0.18	3.86	0.1223	0.00076 3127	1724.19	0.17575 841	0.18	0.35652 1537	0.22547 9351
14	0.15	0.18	3.85	0.126	0.00081	1730.24	0.17637 5127	0.18	0.35718 5127	0.23230 0885
15	0.15	0.18	3.84	0.1296	0.00085 6947	1740.41	0.17741 1825	0.18	0.35826 8772	0.23893 8053

TABLE-10 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=5cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION VERTICAL ($v=0.3461$ m/s)($h=5$ cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0811	0.000335572	3352.29	0.341721713	0.03	0.372057284	0.149520649
2	0.15	0.03	3.49	0.1003	0.00051327	3362.2	0.342731906	0.03	0.373245176	0.184918879
3	0.15	0.03	3.48	0.1198	0.000732247	3372.1	0.343741081	0.03	0.374473327	0.220870206
4	0.15	0.03	3.47	0.1334	0.000907937	3380.14	0.344560652	0.03	0.375468589	0.245943953
5	0.15	0.03	3.46	0.1446	0.001066794	3387.46	0.34530683	0.03	0.376373624	0.26659292
6	0.15	0.03	3.45	0.1559	0.001240041	3394.8	0.346055046	0.03	0.377295087	0.287426254
7	0.15	0.03	3.44	0.1641	0.001373919	3401.31	0.346718654	0.03	0.378092573	0.302544248
8	0.15	0.03	3.43	0.1722	0.0015129	3407.76	0.347376147	0.03	0.378889047	0.317477876
9	0.15	0.03	3.42	0.1804	0.001660416	3414.24	0.348036697	0.03	0.379697114	0.33259587
10	0.15	0.03	3.41	0.1876	0.0017956	3420.19	0.348643221	0.03	0.380438821	0.345870206
11	0.15	0.03	3.4	0.1939	0.001918225	3425.66	0.349200815	0.03	0.38111904	0.357485251
12	0.15	0.03	3.39	0.1003	0.00051327	3431.14	0.349759429	0.03	0.380272699	0.184918879
13	0.15	0.03	3.38	0.1068	0.000581951	3436.63	0.350319062	0.03	0.380901013	0.196902655
14	0.15	0.03	3.37	0.1123	0.000643433	3441.26	0.35079103	0.03	0.381434463	0.207042773
15	0.15	0.03	3.36	0.1171	0.000699613	3445.38	0.351211009	0.03	0.381910622	0.21589233

**TABLE-11 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=5cm
IN 10% OBSTRUCTION**

WITH 10% OBSTRUCTION VERTICAL (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.25	0.00318 8776	1363.35	0.13897 5535	0.18	0.32216 4311	0.46091 4454
2	0. 15	0. 18	3. 97	0.2315	0.00273 4298	1355.05	0.13812 946	0.18	0.32086 3758	0.42680 6785
3	0. 15	0. 18	3. 96	0.215	0.00235 8418	1357.23	0.13835 1682	0.18	0.32071 01	0.39638 6431
4	0. 15	0. 18	3. 95	0.1998	0.00203 6737	1365.18	0.13916 208	0.18	0.32119 8816	0.36836 2832
5	0. 15	0. 18	3. 94	0.1789	0.00163 2919	1388.39	0.14152 8033	0.18	0.32316 0951	0.32983 0383
6	0. 15	0. 18	3. 93	0.1347	0.00092 5719	1468.15	0.14965 8512	0.18	0.33058 4231	0.24834 0708
7	0. 15	0. 18	3. 92	0	0	1295	0.13200 8155	0.18	0.31200 8155	0
8	0. 15	0. 18	3. 91	0.1348	0.00092 7094	1285.76	0.13106 6259	0.18	0.31199 3353	0.24852 5074
9	0. 15	0. 18	3. 9	0.1918	0.00187 69	1380.36	0.14070 948	0.18	0.32258 638	0.35361 3569
10	0. 15	0. 18	3. 89	0.2148	0.00235 4033	1410.21	0.14375 2294	0.18	0.32610 6326	0.39601 7699
11	0. 15	0. 18	3. 88	0.2277	0.00264 527	1419.27	0.14467 5841	0.18	0.32732 1111	0.41980 0885
12	0. 15	0. 18	3. 87	0.2315	0.00273 4298	1435.15	0.14629 4597	0.18	0.32902 8896	0.42680 6785
13	0. 15	0. 18	3. 86	0.2365	0.00285 3686	1444.09	0.14720 5912	0.18	0.33005 9599	0.43602 5074
14	0. 15	0. 18	3. 85	0.2419	0.00298 549	1440.36	0.14682 5688	0.18	0.32981 1178	0.44598 0826
15	0. 15	0. 18	3. 84	0.2478	0.00313 29	1442.64	0.14705 8104	0.18	0.33019 1004	0.45685 8407

TABLE-12 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=5cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION VERTICAL (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0445	0.000101033	3204.73	0.326679918	0.03	0.356780952	0.082042773
2	0.15	0.03	3.49	0.0606	0.000187365	3214.8	0.327706422	0.03	0.357893787	0.111725664
3	0.15	0.03	3.48	0.0788	0.000316808	3216.03	0.327831804	0.03	0.358148612	0.145280236
4	0.15	0.03	3.47	0.0927	0.000438433	3220.95	0.328333333	0.03	0.358771766	0.17090708
5	0.15	0.03	3.46	0.0968	0.000478073	3222.82	0.328523955	0.03	0.359002029	0.178466077
6	0.15	0.03	3.45	0.1044	0.00055609	3227.79	0.329030581	0.03	0.359586671	0.192477876
7	0.15	0.03	3.44	0.1148	0.0006724	3233.81	0.329644241	0.03	0.360316641	0.211651917
8	0.15	0.03	3.43	0.12	0.000734694	3240.73	0.330349643	0.03	0.361084337	0.221238938
9	0.15	0.03	3.42	0.1252	0.000799747	3247.65	0.331055046	0.03	0.361854793	0.230825959
10	0.15	0.03	3.41	0.1258	0.000807431	3256.56	0.331963303	0.03	0.362770733	0.231932153
11	0.15	0.03	3.4	0.127	0.000822908	3259.76	0.332289501	0.03	0.363112409	0.234144543
12	0.15	0.03	3.39	0.1282	0.000838533	3262.96	0.332615698	0.03	0.363454231	0.236356932
13	0.15	0.03	3.38	0.1295	0.000855625	3266.16	0.332941896	0.03	0.363797521	0.238753687
14	0.15	0.03	3.37	0.1299	0.000860919	3269.47	0.333279307	0.03	0.364140226	0.23949115
15	0.15	0.03	3.36	0.1292	0.000851665	3274.41	0.333782875	0.03	0.36463454	0.23820059

**TABLE-13 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=5cm
IN 20% OBSTRUCTION**

WITH 20% OBSTRUCTION VERTICAL (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.248	0.00313 7959	1408.38	0.14356 5749	0.18	0.32670 3708	0.45722 7139
2	0. 15	0. 18	3. 97	0.2232	0.00254 1747	1403.29	0.14304 6891	0.18	0.32558 8638	0.41150 4425
3	0. 15	0. 18	3. 96	0.1956	0.00195 2008	1413.9	0.14412 844	0.18	0.32608 0449	0.36061 9469
4	0. 15	0. 18	3. 95	0.1634	0.00136 2222	1423.79	0.14513 6595	0.18	0.32649 8818	0.30125 3687
5	0. 15	0. 18	3. 94	0.1228	0.00076 938	1443.61	0.14715 6983	0.18	0.32792 6362	0.22640 118
6	0. 15	0. 18	3. 93	0.0031	4.90306 E-07	1534.8	0.15645 2599	0.18	0.33645 309	0.00571 5339
7	0. 15	0. 18	3. 92	0	0		0	0.18	0.18	0
8	0. 15	0. 18	3. 91	0.0023	2.69898 E-07	1283.89	0.13087 5637	0.18	0.31087 5907	0.00424 0413
9	0. 15	0. 18	3. 9	0.1204	0.00073 96	1380	0.14067 2783	0.18	0.32141 2383	0.22197 6401
10	0. 15	0. 18	3. 89	0.1615	0.00133 0727	1411.31	0.14386 4424	0.18	0.32519 5151	0.29775 0737
11	0. 15	0. 18	3. 88	0.1835	0.00171 7972	1426.41	0.14540 367	0.18	0.32712 1642	0.33831 1209
12	0. 15	0. 18	3. 87	0.194	0.00192 0204	1437.8	0.14656 473	0.18	0.32848 4934	0.35766 9617
13	0. 15	0. 18	3. 86	0.2016	0.00207 36	1442.75	0.14706 9317	0.18	0.32914 2917	0.37168 1416
14	0. 15	0. 18	3. 85	0.2085	0.00221 7972	1448.53	0.14765 8512	0.18	0.32987 6484	0.38440 2655
15	0. 15	0. 18	3. 84	0.2177	0.00241 8025	1450.77	0.14788 685	0.18	0.33030 4875	0.40136 4307

TABLE-14 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=5cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION VERTICAL (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0388	7.68082 E-05	3196.62	0.32585 3211	0.03	0.35593 0019	0.07153 3923
2	0.15	0.03	3.49	0.0542	0.00014 988	3210.67	0.32728 5423	0.03	0.35743 5303	0.09992 6254
3	0.15	0.03	3.48	0.0727	0.00026 9658	3213.94	0.32761 8756	0.03	0.35788 8414	0.13403 3923
4	0.15	0.03	3.47	0.0827	0.00034 8943	3219.67	0.32820 2854	0.03	0.35855 1798	0.15247 0501
5	0.15	0.03	3.46	0.0889	0.00040 3225	3221.8	0.32841 998	0.03	0.35882 3205	0.16390 118
6	0.15	0.03	3.45	0.1	0.00051 0204	3224.98	0.32874 4139	0.03	0.35925 4343	0.18436 5782
7	0.15	0.03	3.44	0.1058	0.00057 1104	3228.66	0.32911 9266	0.03	0.35969 037	0.19505 8997
8	0.15	0.03	3.43	0.1107	0.00062 5229	3233.82	0.32964 526	0.03	0.36027 0489	0.20409 292
9	0.15	0.03	3.42	0.1178	0.00070 8002	3236.59	0.32992 7625	0.03	0.36063 5627	0.21718 2891
10	0.15	0.03	3.41	0.125	0.00079 7194	3239.36	0.33020 999	0.03	0.36100 7184	0.23045 7227
11	0.15	0.03	3.4	0.1332	0.00090 5216	3242.13	0.33049 2355	0.03	0.36139 7571	0.24557 5221
12	0.15	0.03	3.39	0.1331	0.00090 3858	3244.24	0.33070 7441	0.03	0.36161 1299	0.24539 0855
13	0.15	0.03	3.38	0.1312	0.00087 8237	3249.15	0.33120 7951	0.03	0.36208 6188	0.24188 7906
14	0.15	0.03	3.37	0.1294	0.00085 4304	3254.05	0.33170 7441	0.03	0.36256 1745	0.23856 9322
15	0.15	0.03	3.36	0.1281	0.00083 7225	3259.3	0.33224 261	0.03	0.36307 9835	0.23617 2566

**TABLE-15 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=5cm
IN 30% OBSTRUCTION**

WITH 30% OBSTRUCTION VERTICAL (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.2453	0.00307 0005	1432.69	0.14604 3833	0.18	0.32911 3837	0.45224 9263
2	0. 15	0. 18	3. 97	0.214	0.00233 6531	1437.58	0.14654 2304	0.18	0.32887 8834	0.39454 2773
3	0. 15	0. 18	3. 96	0.1828	0.00170 489	1436.2	0.14640 1631	0.18	0.32810 6521	0.33702 0649
4	0. 15	0. 18	3. 95	0.139	0.00098 5765	1444.9	0.14728 8481	0.18	0.32827 4246	0.25626 8437
5	0. 15	0. 18	3. 94	0.0772	0.00030 4073	1481.28	0.15099 6942	0.18	0.33130 1015	0.14233 0383
6	0. 15	0. 18	3. 93	0	0	1509.66	0.15388 9908	0.18	0.33388 9908	0
7	0. 15	0. 18	3. 92	0	0	0	0	0.18	0.18	0
8	0. 15	0. 18	3. 91	0	0	1313.53	0.13389 7044	0.18	0.31389 7044	0
9	0. 15	0. 18	3. 9	0.079	0.00031 8418	1367.32	0.13938 0224	0.18	0.31969 8643	0.14564 8968
10	0. 15	0. 18	3. 89	0.1173	0.00070 2005	1409.23	0.14365 2396	0.18	0.32435 44	0.21626 1062
11	0. 15	0. 18	3. 88	0.1485	0.00112 5115	1426.19	0.14538 1244	0.18	0.32650 6358	0.27378 3186
12	0. 15	0. 18	3. 87	0.1656	0.00139 9151	1438.43	0.14662 895	0.18	0.32802 8101	0.30530 9735
13	0. 15	0. 18	3. 86	0.1802	0.00165 6737	1438.82	0.14666 8705	0.18	0.32832 5442	0.33222 7139
14	0. 15	0. 18	3. 85	0.189	0.00182 25	1446.11	0.14741 1825	0.18	0.32923 4325	0.34845 1327
15	0. 15	0. 18	3. 84	0.1975	0.00199 0115	1456.15	0.14843 527	0.18	0.33042 5385	0.36412 2419

TABLE-16 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=5cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION VERTICAL (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0476	0.0001156	3192.35	0.325417941	0.03	0.355533541	0.087758112
2	0.15	0.03	3.49	0.0625	0.000199298	3205.22	0.326729867	0.03	0.356929166	0.115228614
3	0.15	0.03	3.48	0.071	0.000257194	3215.32	0.327759429	0.03	0.358016623	0.130899705
4	0.15	0.03	3.47	0.087	0.000386173	3211.04	0.32732314	0.03	0.357709313	0.16039823
5	0.15	0.03	3.46	0.097	0.000480051	3210.77	0.327295617	0.03	0.357775668	0.178834808
6	0.15	0.03	3.45	0.1022	0.0005329	3210.57	0.327275229	0.03	0.357808129	0.188421829
7	0.15	0.03	3.44	0.0987	0.000497025	3227.85	0.329036697	0.03	0.359533722	0.181969027
8	0.15	0.03	3.43	0.1012	0.000522522	3235.08	0.3297737	0.03	0.360296223	0.186578171
9	0.15	0.03	3.42	0.1095	0.000611747	3240.33	0.330308869	0.03	0.360920616	0.201880531
10	0.15	0.03	3.41	0.1156	0.000681804	3245.25	0.330810398	0.03	0.361492202	0.213126844
11	0.15	0.03	3.4	0.1152	0.000677094	3258.53	0.332164118	0.03	0.362841212	0.212389381
12	0.15	0.03	3.39	0.1147	0.000671229	3272.38	0.333575943	0.03	0.364247172	0.211467552
13	0.15	0.03	3.38	0.1131	0.000652633	3287.65	0.335132518	0.03	0.365785151	0.208517699
14	0.15	0.03	3.37	0.1146	0.000670059	3291.45	0.335519878	0.03	0.366189937	0.211283186
15	0.15	0.03	3.36	0.121	0.00074699	3290.66	0.335439348	0.03	0.366186337	0.223082596

**TABLE-17 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=8cm
IN NO OBSTRUCTION**

WITHOUT OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.3412	0.005939665	1498.91	0.152794088	0.18	0.338733753	0.629056047
2	0.15	0.18	3.97	0.3212	0.005263747	1507.74	0.15369419	0.18	0.338957937	0.592182891
3	0.15	0.18	3.96	0.2973	0.004509556	1515.55	0.154490316	0.18	0.338999872	0.548119469
4	0.15	0.18	3.95	0.2744	0.0038416	1523.44	0.155294597	0.18	0.339136197	0.505899705
5	0.15	0.18	3.94	0.2562	0.0033489	1526.67	0.155623853	0.18	0.338972753	0.472345133
6	0.15	0.18	3.93	0.2407	0.002955943	1527.37	0.155695209	0.18	0.338651152	0.443768437
7	0.15	0.18	3.92	0.2258	0.002601308	1528.09	0.155768603	0.18	0.338369912	0.416297935
8	0.15	0.18	3.91	0.2127	0.002308229	1527.5	0.155708461	0.18	0.33801669	0.392146018
9	0.15	0.18	3.9	0.2001	0.002042858	1526.92	0.155649337	0.18	0.337692195	0.368915929
10	0.15	0.18	3.89	0.1883	0.001809025	1526.61	0.155617737	0.18	0.337426762	0.347160767
11	0.15	0.18	3.88	0.1776	0.001609273	1526.67	0.155623853	0.18	0.337233127	0.327433628
12	0.15	0.18	3.87	0.1672	0.001426318	1526.75	0.155632008	0.18	0.337058327	0.308259587
13	0.15	0.18	3.86	0.1591	0.00129147	1527.35	0.15569317	0.18	0.33698464	0.293325959
14	0.15	0.18	3.85	0.1513	0.001167943	1527.96	0.155755352	0.18	0.336923295	0.278945428
15	0.15	0.18	3.84	0.1446	0.001066794	1531.8	0.156146789	0.18	0.337213583	0.26659292

TABLE-18 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=8cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0409	8.53474 E-05	3115.39	0.31757 2885	0.03	0.34765 8232	0.00538 6115
2	0.15	0.03	3.49	0.0519	0.00013 7429	3119.05	0.31794 5973	0.03	0.34808 3403	0.09568 5841
3	0.15	0.03	3.48	0.0672	0.00023 04	3122.79	0.31832 7217	0.03	0.34855 7617	0.12389 3805
4	0.15	0.03	3.47	0.0783	0.00031 2801	3127.18	0.31877 472	0.03	0.34908 752	0.14435 8407
5	0.15	0.03	3.46	0.0872	0.00038 7951	3132	0.31926 6055	0.03	0.34965 4006	0.16076 6962
6	0.15	0.03	3.45	0.0963	0.00047 3147	3136.83	0.31975 841	0.03	0.35023 1557	0.17754 4248
7	0.15	0.03	3.44	0.1033	0.00054 4433	3142.29	0.32031 4985	0.03	0.35085 9418	0.19044 9853
8	0.15	0.03	3.43	0.1103	0.00062 0719	3147.81	0.32087 7676	0.03	0.35149 8395	0.20335 5457
9	0.15	0.03	3.42	0.1173	0.00070 2005	3153.35	0.32144 2406	0.03	0.35214 441	0.21626 1062
10	0.15	0.03	3.41	0.1236	0.00077 9437	3158.93	0.32201 1213	0.03	0.35279 065	0.22787 6106
11	0.15	0.03	3.4	0.1294	0.00085 4304	3164.65	0.32259 4292	0.03	0.35344 8596	0.23856 9322
12	0.15	0.03	3.39	0.1353	0.00093 3984	3170.34	0.32317 4312	0.03	0.35410 8296	0.24944 6903
13	0.15	0.03	3.38	0.1412	0.00101 7216	3176.04	0.32375 5352	0.03	0.35477 2568	0.26032 4484
14	0.15	0.03	3.37	0.1466	0.00109 6508	3181.51	0.32431 2946	0.03	0.35540 9454	0.27028 0236
15	0.15	0.03	3.36	0.1518	0.00117 5676	3186.84	0.32485 6269	0.03	0.35603 1945	0.27986 7257

**TABLE-19 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=8cm
IN 10% OBSTRUCTION**

WITH 10% OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.3457	0.00609 7372	1607.29	0.16384 1998	0.18	0.34993 937	0.63735 2507
2	0. 15	0. 18	3. 97	0.3328	0.00565 0808	1608.22	0.16393 6799	0.18	0.34958 7607	0.61356 9322
3	0. 15	0. 18	3. 96	0.3175	0.00514 3176	1618.66	0.16500 1019	0.18	0.35014 4195	0.58536 1357
4	0. 15	0. 18	3. 95	0.3056	0.00476 4865	1629.19	0.16607 4414	0.18	0.35083 9279	0.56342 1829
5	0. 15	0. 18	3. 94	0.2863	0.00418 2025	1661.74	0.16939 2457	0.18	0.35357 4482	0.52783 9233
6	0. 15	0. 18	3. 93	0.2121	0.00229 5225	1792.44	0.18271 5596	0.18	0.36501 0821	0.39103 9823
7	0. 15	0. 18	3. 92	0	0	1624.3	0.16557 5943	0.18	0.34557 5943	0
8	0. 15	0. 18	3. 91	0.1938	0.00191 6247	1499.75	0.15287 9715	0.18	0.33479 5962	0.35730 0885
9	0. 15	0. 18	3. 9	0.2722	0.00378 0247	1596.21	0.16271 2538	0.18	0.34649 2785	0.50184 3658
10	0. 15	0. 18	3. 89	0.3067	0.00479 9229	1644.32	0.16761 6718	0.18	0.35241 5947	0.56544 9853
11	0. 15	0. 18	3. 88	0.3289	0.00551 9143	1660.36	0.16925 1784	0.18	0.35477 0927	0.60637 9056
12	0. 15	0. 18	3. 87	0.3456	0.00609 3845	1669.03	0.17013 5576	0.18	0.35622 9421	0.63716 8142
13	0. 15	0. 18	3. 86	0.358	0.00653 898	1671.4	0.17037 7166	0.18	0.35691 6146	0.66002 9499
14	0. 15	0. 18	3. 85	0.3727	0.00708 7005	1667.35	0.16996 4322	0.18	0.35705 1327	0.68713 1268
15	0. 15	0. 18	3. 84	0.3835	0.00750 3686	1657.96	0.16900 7136	0.18	0.35651 0822	0.70704 2773

TABLE-20 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=8cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0637	0.000207025	3323	0.338735984	0.03	0.368943009	0.117441003
2	0.15	0.03	3.49	0.0985	0.000495013	3342.65	0.340739042	0.03	0.371234055	0.181600295
3	0.15	0.03	3.48	0.1195	0.000728584	3358.32	0.342336391	0.03	0.373064976	0.220317109
4	0.15	0.03	3.47	0.1432	0.001046237	3374.86	0.344022426	0.03	0.375068663	0.264011799
5	0.15	0.03	3.46	0.1569	0.001256001	3389.08	0.345471967	0.03	0.376727968	0.289269912
6	0.15	0.03	3.45	0.1652	0.0013924	3400.18	0.346603466	0.03	0.377995866	0.304572271
7	0.15	0.03	3.44	0.1841	0.001729225	3409.68	0.347571865	0.03	0.37930109	0.339417404
8	0.15	0.03	3.43	0.2	0.002040816	3420.05	0.34862895	0.03	0.380669766	0.368731563
9	0.15	0.03	3.42	0.209	0.002228622	3425.75	0.34920999	0.03	0.381438612	0.385324484
10	0.15	0.03	3.41	0.2218	0.002509961	3429.73	0.349615698	0.03	0.382125659	0.408923304
11	0.15	0.03	3.4	0.2337	0.002786515	3434.08	0.350059123	0.03	0.382845638	0.430862832
12	0.15	0.03	3.39	0.2386	0.00290459	3446.42	0.351317023	0.03	0.384221613	0.439896755
13	0.15	0.03	3.38	0.2344	0.002803233	3450.85	0.351768603	0.03	0.384571836	0.432153392
14	0.15	0.03	3.37	0.2272	0.002633665	3452.9	0.351977574	0.03	0.384611239	0.418879056
15	0.15	0.03	3.36	0.2201	0.002471633	3455.22	0.352214067	0.03	0.3846857	0.405789086

**TABLE-21 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=8cm
IN 20% OBSTRUCTION**

WITH 20% OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.3383	0.00583 9127	1399.85	0.14269 6228	0.18	0.32853 5355	0.62370 944
2	0. 15	0. 18	3. 97	0.3123	0.00497 6086	1405.14	0.14323 5474	0.18	0.32821 156	0.57577 4336
3	0. 15	0. 18	3. 96	0.2862	0.00417 9104	1412.94	0.14403 0581	0.18	0.32820 9685	0.52765 4867
4	0. 15	0. 18	3. 95	0.2588	0.00341 7216	1419.85	0.14473 4964	0.18	0.32815 2181	0.47713 8643
5	0. 15	0. 18	3. 94	0.2011	0.00206 3327	1458.03	0.14862 6911	0.18	0.33069 0238	0.37075 9587
6	0. 15	0. 18	3. 93	0.0129	8.49031 E-06	1551.93	0.15819 8777	0.18	0.33820 7267	0.02378 3186
7	0. 15	0. 18	3. 92	0	0	0	0	0.18	0.18	0
8	0. 15	0. 18	3. 91	0.0065	2.15561 E-06	1258.31	0.12826 8094	0.18	0.30827 0249	0.01198 3776
9	0. 15	0. 18	3. 9	0.1544	0.00121 6294	1338.45	0.13643 7309	0.18	0.31765 3603	0.28466 0767
10	0. 15	0. 18	3. 89	0.1903	0.00184 7658	1370.82	0.13973 7003	0.18	0.32158 4661	0.35084 8083
11	0. 15	0. 18	3. 88	0.2132	0.00231 9094	1383.27	0.14100 6116	0.18	0.32332 521	0.39306 7847
12	0. 15	0. 18	3. 87	0.2301	0.00270 1327	1388	0.14148 8277	0.18	0.32418 9604	0.42422 5664
13	0. 15	0. 18	3. 86	0.2452	0.00306 7502	1391.91	0.14188 685	0.18	0.32495 4352	0.45206 4897
14	0. 15	0. 18	3. 85	0.2581	0.00339 8756	1399.47	0.14265 7492	0.18	0.32605 6248	0.47584 8083
15	0. 15	0. 18	3. 84	0.2702	0.00372 49	1403.74	0.14309 2762	0.18	0.32681 7662	0.49815 6342

TABLE-22 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=8cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0459	0.00010749	3152.96	0.32140265	0.03	0.351510141	0.084623894
2	0.15	0.03	3.49	0.0651	0.000216225	3159.79	0.322098879	0.03	0.352315104	0.120022124
3	0.15	0.03	3.48	0.0828	0.000349788	3161.36	0.322258919	0.03	0.352608707	0.152654867
4	0.15	0.03	3.47	0.0961	0.000471184	3165.79	0.322710499	0.03	0.353181684	0.177175516
5	0.15	0.03	3.46	0.1098	0.000615104	3169.44	0.323082569	0.03	0.353697673	0.202433628
6	0.15	0.03	3.45	0.1192	0.000724931	3173.78	0.323524975	0.03	0.354249905	0.219764012
7	0.15	0.03	3.44	0.1287	0.000845086	3182.54	0.324417941	0.03	0.355263027	0.237278761
8	0.15	0.03	3.43	0.1353	0.000933984	3191.8	0.325361876	0.03	0.35629586	0.249446903
9	0.15	0.03	3.42	0.1423	0.001033127	3203.97	0.326602446	0.03	0.357635574	0.262352507
10	0.15	0.03	3.41	0.1473	0.001107005	3206.47	0.326857288	0.03	0.357964293	0.271570796
11	0.15	0.03	3.4	0.1526	0.0011881	3206.14	0.326823649	0.03	0.358011749	0.281342183
12	0.15	0.03	3.39	0.1613	0.001327433	3205.58	0.326766565	0.03	0.358093998	0.297382006
13	0.15	0.03	3.38	0.1701	0.001476225	3205.01	0.326708461	0.03	0.358184686	0.313606195
14	0.15	0.03	3.37	0.1789	0.001632919	3207.24	0.32693578	0.03	0.358568699	0.329830383
15	0.15	0.03	3.36	0.174	0.001544694	3219.13	0.328147808	0.03	0.359692502	0.32079646

**TABLE-23 UPSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=8cm
IN 30% OBSTRUCTION**

WITH 30% OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0. 15	0. 18	3. 98	0.3321	0.00562 7062	1617.6	0.16489 2966	0.18	0.35052 0028	0.61227 8761
2	0. 15	0. 18	3. 97	0.3082	0.00484 6288	1623.05	0.16544 8522	0.18	0.35029 481	0.56821 5339
3	0. 15	0. 18	3. 96	0.2642	0.00356 1308	1641.37	0.16731 6004	0.18	0.35087 7312	0.48709 4395
4	0. 15	0. 18	3. 95	0.224	0.00256	1663.47	0.16956 8807	0.18	0.35212 8807	0.41297 9351
5	0. 15	0. 18	3. 94	0.1303	0.00086 6229	1738.45	0.17721 2029	0.18	0.35807 8258	0.24022 8614
6	0. 15	0. 18	3. 93	0	0	1798.35	0.18331 8043	0.18	0.36331 8043	0
7	0. 15	0. 18	3. 92	0	0	0	0	0.18	0.18	0
8	0. 15	0. 18	3. 91	0	0	1249.53	0.12737 3089	0.18	0.30737 3089	0
9	0. 15	0. 18	3. 9	0.1033	0.00054 4433	1487.13	0.15159 3272	0.18	0.33213 7705	0.19044 9853
10	0. 15	0. 18	3. 89	0.1737	0.00153 9372	1554.33	0.15844 3425	0.18	0.33998 2797	0.32024 3363
11	0. 15	0. 18	3. 88	0.2035	0.00211 287	1578.96	0.16095 4128	0.18	0.34306 6998	0.37518 4366
12	0. 15	0. 18	3. 87	0.2363	0.00284 8862	1586.69	0.16174 21	0.18	0.34459 0962	0.43565 6342
13	0. 15	0. 18	3. 86	0.2587	0.00341 4576	1595.95	0.16268 6035	0.18	0.34610 0611	0.47695 4277
14	0. 15	0. 18	3. 85	0.2761	0.00388 9347	1610.91	0.16421 1009	0.18	0.34810 0357	0.50903 3923
15	0. 15	0. 18	3. 84	0.2927	0.00437 1086	1617.22	0.16485 423	0.18	0.34922 5317	0.53963 8643

TABLE-24 DOWNSTREAM READING FOR VERTICAL OBSTRUCTION AT HEAD=8cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0594	0.000180018	3290.51	0.335424057	0.03	0.365604075	0.109513274
2	0.15	0.03	3.49	0.0846	0.000365161	3309.79	0.337389399	0.03	0.36775456	0.155973451
3	0.15	0.03	3.48	0.0969	0.000479062	3330.57	0.339507645	0.03	0.369986707	0.178650442
4	0.15	0.03	3.47	0.1158	0.000684165	3339.29	0.340396534	0.03	0.371080699	0.213495575
5	0.15	0.03	3.46	0.1347	0.000925719	3345.86	0.341066259	0.03	0.371991978	0.248340708
6	0.15	0.03	3.45	0.144	0.001057959	3345.45	0.341024465	0.03	0.372082424	0.265486726
7	0.15	0.03	3.44	0.1579	0.001272062	3355.97	0.34209684	0.03	0.373368902	0.291113569
8	0.15	0.03	3.43	0.1721	0.001511143	3366.49	0.343169215	0.03	0.374680358	0.31729351
9	0.15	0.03	3.42	0.1801	0.001654898	3374.89	0.344025484	0.03	0.375680383	0.332042773
10	0.15	0.03	3.41	0.1909	0.001859327	3382.29	0.344779817	0.03	0.376639144	0.351954277
11	0.15	0.03	3.4	0.2023	0.002088025	3389.13	0.345477064	0.03	0.377565089	0.372971976
12	0.15	0.03	3.39	0.2142	0.0023409	3395.06	0.346081549	0.03	0.378422449	0.394911504
13	0.15	0.03	3.38	0.2254	0.0025921	3401.22	0.34670948	0.03	0.37930158	0.415560472
14	0.15	0.03	3.37	0.2183	0.002431372	3401.32	0.346719674	0.03	0.379151046	0.402470501
15	0.15	0.03	3.36	0.2085	0.002217972	3416.84	0.348301733	0.03	0.380519705	0.384402655

TABLE-25 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=3cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION horizontal (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELOCITY	VELOCITY HEAD	PRESSURE	PRESSURE HEAD	DATUM HEAD	TOTAL HEAD	FROUDE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.1419	0.001027327	1632.63	0.166425076	0.18	0.347452403	0.261615044
2	0.15	0.18	3.97	0.1216	0.000754416	1637.29	0.166900102	0.18	0.347654518	0.224188791
3	0.15	0.18	3.96	0.099	0.000500051	1640.21	0.167197757	0.18	0.347697808	0.182522124
4	0.15	0.18	3.95	0.0786	0.000315202	1643.11	0.167493374	0.18	0.347808576	0.144911504
5	0.15	0.18	3.94	0.0651	0.000216225	1643.98	0.167582059	0.18	0.347798284	0.120022124
6	0.15	0.18	3.93	0.0545	0.000151543	1643.7	0.167553517	0.18	0.34770506	0.100479351
7	0.15	0.18	3.92	0.0444	0.00010058	1643.43	0.167525994	0.18	0.347626573	0.081858407
8	0.15	0.18	3.91	0.0362	6.68592E-05	1642.9	0.167471967	0.18	0.347538827	0.066740413
9	0.15	0.18	3.9	0.0285	4.14413E-05	1642.35	0.167415902	0.18	0.347457343	0.052544248
10	0.15	0.18	3.89	0.0225	2.58291E-05	1642.23	0.16740367	0.18	0.347429499	0.041482301
11	0.15	0.18	3.88	0.0188	1.80327E-05	1642.75	0.167456677	0.18	0.34747471	0.034660767
12	0.15	0.18	3.87	0.0156	1.24163E-05	1643.26	0.167508665	0.18	0.347521081	0.028761062
13	0.15	0.18	3.86	0.0157	1.2576E-05	1645.08	0.16769419	0.18	0.347706766	0.028945428
14	0.15	0.18	3.85	0.0174	1.54469E-05	1646.93	0.167882773	0.18	0.34789822	0.032079646

TABLE-26 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=3cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION horizontal (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0258	3.39612E-05	3256.98	0.332006116	0.03	0.362040077	0.047566372
2	0.15	0.03	3.49	0.0284	4.1151E-05	3259.2	0.332232416	0.03	0.362273567	0.052359882
3	0.15	0.03	3.48	0.0353	6.3576E-05	3261.42	0.332458716	0.03	0.362522292	0.065081121
4	0.15	0.03	3.47	0.0411	8.61842E-05	3263.91	0.332712538	0.03	0.362798722	0.075774336
5	0.15	0.03	3.46	0.046	0.000107959	3266.52	0.332978593	0.03	0.363086552	0.08480826
6	0.15	0.03	3.45	0.0512	0.000133747	3269.14	0.333245668	0.03	0.363379415	0.09439528
7	0.15	0.03	3.44	0.0554	0.00015659	3272.44	0.333582059	0.03	0.363738649	0.102138643
8	0.15	0.03	3.43	0.0595	0.000180625	3275.8	0.333924567	0.03	0.364105192	0.10969764
9	0.15	0.03	3.42	0.0636	0.000206376	3279.18	0.334269113	0.03	0.364475489	0.117256637
10	0.15	0.03	3.41	0.0674	0.000231773	3282.84	0.334642202	0.03	0.364873975	0.124262537
11	0.15	0.03	3.4	0.0708	0.000255747	3286.84	0.335049949	0.03	0.365305696	0.130530973
12	0.15	0.03	3.39	0.0742	0.0002809	3290.81	0.335454638	0.03	0.365735538	0.13679941
13	0.15	0.03	3.38	0.0777	0.000308025	3294.78	0.335859327	0.03	0.366167352	0.143252212
14	0.15	0.03	3.37	0.0809	0.000333919	3298.79	0.336268094	0.03	0.366602013	0.149151917

TABLE-27 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=3cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION horizontal (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.1151	0.000675919	1532.63	0.156231397	0.04	0.196907315	0.183865815
2	0.15	0.18	3.97	0.0809	0.000333919	1537.29	0.156706422	0.04	0.197040341	0.129233227
3	0.15	0.18	3.96	0.0835	0.000355727	1540.21	0.157004077	0.04	0.197359805	0.133386581
4	0.15	0.18	3.95	0.084	0.00036	1543.11	0.157299694	0.04	0.197659694	0.134185304
5	0.15	0.18	3.94	0.0865	0.000381747	1543.98	0.157388379	0.04	0.197770127	0.138178914
6	0.15	0.18	3.93	0.2147	0.002351841	1543.7	0.157359837	0.04	0.199711678	0.342971246
7	0.15	0.18	3.92	0.0592	0.000178808	1543.43	0.157332314	0.04	0.197511122	0.09456869
8	0.15	0.18	3.91	0.1997	0.002034698	1542.9	0.157278287	0.04	0.199312986	0.319009585
9	0.15	0.18	3.9	0.0304	4.7151E-05	1542.35	0.157222222	0.04	0.197269373	0.0485623
10	0.15	0.18	3.89	0.0149	1.1327E-05	1542.23	0.15720999	0.04	0.197221317	0.023801917
11	0.15	0.18	3.88	0.0192	1.88082E-05	1542.75	0.157262997	0.04	0.197281805	0.030670927
12	0.15	0.18	3.87	0.0634	0.00020508	1543.26	0.157314985	0.04	0.197520064	0.101277955
13	0.15	0.18	3.86	0.0851	0.00036949	1545.08	0.15750051	0.04	0.19787	0.135942492
14	0.15	0.18	3.85	0.1074	0.000588508	1546.93	0.157689093	0.04	0.198277601	0.171565495

TABLE-28 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=3cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION horizontal (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0302	0.001540816	3215.5	0.327777778	0.04	0.369318594	0.048242812
2	0.15	0.03	3.49	0.0356	0.001816327	3216.4	0.327869521	0.04	0.369685847	0.05686901
3	0.15	0.03	3.48	0.0421	0.002147959	3218.16	0.32804893	0.04	0.370196889	0.067252396
4	0.15	0.03	3.47	0.0451	0.00230102	3219.96	0.328232416	0.04	0.370533436	0.072044728
5	0.15	0.03	3.46	0.0481	0.002454082	3222.4	0.328481142	0.04	0.370935223	0.076837061
6	0.15	0.03	3.45	0.0511	0.002607143	3224.85	0.328730887	0.04	0.37133803	0.081629393
7	0.15	0.03	3.44	0.0545	0.002780612	3227.91	0.329042813	0.04	0.371823426	0.087060703
8	0.15	0.03	3.43	0.058	0.002959184	3231.59	0.329417941	0.04	0.372377125	0.092651757
9	0.15	0.03	3.42	0.0616	0.003142857	3235.24	0.32979001	0.04	0.372932867	0.098402556
10	0.15	0.03	3.41	0.0652	0.003326531	3238.91	0.330164118	0.04	0.373490649	0.104153355
11	0.15	0.03	3.4	0.0696	0.00355102	3242.6	0.330540265	0.04	0.374091285	0.111182109
12	0.15	0.03	3.39	0.0742	0.003785714	3246.33	0.330920489	0.04	0.374706204	0.118530351
13	0.15	0.03	3.38	0.0788	0.004020408	3249.97	0.331291539	0.04	0.375311947	0.125878594
14	0.15	0.03	3.37	0.0834	0.004255102	3253.84	0.331686035	0.04	0.375941137	0.133226837

TABLE-29 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=3cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION horizontal (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.1133	0.00065 4943	1386.58	0.14134 3527	0.18	0.32199 847	0.20888 6431
2	0.15	0.18	3.97	0.0808	0.00033 3094	1405.36	0.14325 79	0.18	0.32359 0994	0.14896 7552
3	0.15	0.18	3.96	0.0834	0.00035 4876	1423.27	0.14508 3588	0.18	0.32543 8464	0.15376 1062
4	0.15	0.18	3.95	0.0819	0.00034 2225	1437.53	0.14653 7207	0.18	0.32687 9432	0.15099 5575
5	0.15	0.18	3.94	0.0756	0.00029 16	1460.63	0.14889 1947	0.18	0.32918 3547	0.13938 0531
6	0.15	0.18	3.93	0.0696	0.00024 7151	1469.56	0.14980 2243	0.18	0.33004 9394	0.12831 8584
7	0.15	0.18	3.92	0.0592	0.00017 8808	1479.23	0.15078 7971	0.18	0.33096 678	0.10914 4543
8	0.15	0.18	3.91	0.038	7.36735 E-05	1477.13	0.15057 3904	0.18	0.33064 7578	0.07005 8997
9	0.15	0.18	3.9	0.0301	0.00004 6225	1458.65	0.14869 0112	0.18	0.32873 6337	0.05549 41
10	0.15	0.18	3.89	0.0313	4.99842 E-05	1461.23	0.14895 3109	0.18	0.32900 3093	0.05770 649
11	0.15	0.18	3.88	0.044	9.87755 E-05	1708.28	0.17413 6595	0.18	0.35423 5371	0.08112 0944
12	0.15	0.18	3.87	0.0962	0.00047 2165	1862.1	0.18981 6514	0.18	0.37028 8679	0.17735 9882
13	0.15	0.18	3.86	0.1199	0.00073 347	1858.19	0.18941 7941	0.18	0.37015 1411	0.22105 4572
14	0.15	0.18	3.85	0.1494	0.00113 8794	1847.04	0.18828 1346	0.18	0.36942 0139	0.27544 2478

TABLE-30 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=3cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION horizontal (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.05	0.0302	4.65327 E-05	3288.83	0.33525 2803	0.03	0.36529 9336	0.05567 8466
2	0.15	0.03	3.49	0.0356	6.46612 E-05	3288.83	0.33525 2803	0.03	0.36531 7464	0.06563 4218
3	0.15	0.03	3.48	0.0421	9.04291 E-05	3287.78	0.33514 577	0.03	0.36523 6199	0.07761 7994
4	0.15	0.03	3.47	0.0451	0.00010 3776	3286.42	0.33500 7136	0.03	0.36511 0912	0.08314 8968
5	0.15	0.03	3.46	0.0481	0.00011 8041	3285.04	0.33486 6463	0.03	0.36498 4504	0.08867 9941
6	0.15	0.03	3.45	0.0511	0.00013 3225	3283.64	0.33472 3751	0.03	0.36485 6976	0.09421 0914
7	0.15	0.03	3.44	0.0545	0.00015 1543	3284.43	0.33480 4281	0.03	0.36495 5825	0.10047 9351
8	0.15	0.03	3.43	0.058	0.00017 1633	3285.43	0.33490 6218	0.03	0.36507 7851	0.10693 2153
9	0.15	0.03	3.42	0.0616	0.00019 36	3286.41	0.33500 6116	0.03	0.36519 9716	0.11356 9322
10	0.15	0.03	3.41	0.0652	0.00021 689	3287.36	0.33510 2956	0.03	0.36531 9846	0.12020 649
11	0.15	0.03	3.04	0.0696	0.00024 7151	3289.43	0.33531 3965	0.03	0.36556 1116	0.12831 8584
12	0.15	0.03	3.39	0.0742	0.00028 09	3291.85	0.33556 0652	0.03	0.36584 1552	0.13679 941
13	0.15	0.03	3.38	0.0788	0.00031 6808	3294.27	0.33580 7339	0.03	0.36612 4148	0.14528 0236
14	0.15	0.03	3.37	0.0834	0.00035 4876	3296.71	0.33605 6065	0.03	0.36641 0941	0.15376 1062

TABLE-31 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=3cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION horizontal (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.1247	0.000793372	1378.81	0.140551478	0.18	0.32134485	0.22990413
2	0.15	0.18	3.97	0.0789	0.000317613	1369.69	0.139621814	0.18	0.319939427	0.145464602
3	0.15	0.18	3.96	0.0615	0.000192972	1390.6	0.141753313	0.18	0.321946285	0.113384956
4	0.15	0.18	3.95	0.0513	0.00013427	1404.18	0.143137615	0.18	0.323271885	0.094579646
5	0.15	0.18	3.94	0.0462	0.0001089	1408.7	0.143598369	0.18	0.323707269	0.085176991
6	0.15	0.18	3.93	0.0538	0.000147676	1409.58	0.143688073	0.18	0.323835749	0.099188791
7	0.15	0.18	3.92	0.006	1.83673E-06	1296.72	0.132183486	0.18	0.312185323	0.011061947
8	0.15	0.18	3.91	0.0075	2.8699E-06	1135.96	0.115796126	0.18	0.295798996	0.013827434
9	0.15	0.18	3.9	0.0239	2.91434E-05	1488.81	0.151764526	0.18	0.331793669	0.044063422
10	0.15	0.18	3.89	0.1126	0.000646876	1619.41	0.165077472	0.18	0.345724347	0.20759587
11	0.15	0.18	3.88	0.1409	0.001012898	1644.94	0.167679918	0.18	0.348692817	0.259771386
12	0.15	0.18	3.87	0.142	0.001028776	1640.13	0.167189602	0.18	0.348218378	0.26179941
13	0.15	0.18	3.86	0.155	0.001225765	1634.81	0.166647299	0.18	0.347873064	0.285766962
14	0.15	0.18	3.85	0.1399	0.000998572	1628.15	0.1659684	0.18	0.346966972	0.257927729

TABLE-32 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=3cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION horizontal (v=.266 m/s)(h=3 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0137	9.57602 E-06	3215.5	0.32777 7778	0.03	0.35778 7354	0.02525 8112
2	0.15	0.03	3.49	0.0042	0.00000 09	3216.4	0.32786 9521	0.03	0.35787 0421	0.00774 3363
3	0.15	0.03	3.48	0.0052	1.37959 E-06	3218.16	0.32804 893	0.03	0.35805 0309	0.00958 7021
4	0.15	0.03	3.47	0.0096	4.70204 E-06	3219.96	0.32823 2416	0.03	0.35823 7118	0.01769 9115
5	0.15	0.03	3.46	0.0117	6.98418 E-06	3222.4	0.32848 1142	0.03	0.35848 8126	0.02157 0796
6	0.15	0.03	3.45	0.0148	1.11755 E-05	3224.85	0.32873 0887	0.03	0.35874 2062	0.02728 6136
	0.15	0.03	3.44	0.018	1.65306 E-05	3227.91	0.32904 2813	0.03	0.35905 9344	0.03318 5841
8	0.15	0.03	3.43	0.0212	2.29306 E-05	3231.59	0.32941 7941	0.03	0.35944 0871	0.03908 5546
9	0.15	0.03	3.42	0.02476	3.12784 E-05	3235.24	0.32979 001	0.03	0.35982 1289	0.04564 8968
10	0.15	0.03	3.41	0.028	0.00004	3238.91	0.33016 4118	0.03	0.36020 4118	0.05162 2419
11	0.15	0.03	3.4	0.0305	4.74617 E-05	3242.6	0.33054 0265	0.03	0.36058 7727	0.05623 1563
12	0.15	0.03	3.39	0.0332	5.62367 E-05	3246.33	0.33092 0489	0.03	0.36097 6726	0.06120 944
13	0.15	0.03	3.38	0.036	6.61224 E-05	3249.97	0.33129 1539	0.03	0.36135 7662	0.06637 1681
14	0.15	0.03	3.37	0.0387	7.64128 E-05	3253.84	0.33168 6035	0.03	0.36176 2447	0.07134 9558

TABLE-33 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=5cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION horizontal (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELOC ITY	VELOC ITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTAL HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.2327	0.00276 2719	1671.76	0.17041 3863	0.18	0.35317 6582	0.42901 9174
2	0.15	0.18	3.97	0.2079	0.00220 5225	1680.02	0.17125 5861	0.18	0.35346 1086	0.38329 646
3	0.15	0.18	3.96	0.1802	0.00165 6737	1686.68	0.17193 476	0.18	0.35359 1497	0.33222 7139
4	0.15	0.18	3.95	0.1534	0.00120 059	1693.34	0.17261 366	0.18	0.35381 4249	0.28281 7109
5	0.15	0.18	3.94	0.138	0.00097 1633	1696.67	0.17295 3109	0.18	0.35392 4742	0.25442 4779
6	0.15	0.18	3.93	0.1288	0.00084 64	1698.23	0.17311 213	0.18	0.35395 853	0.23746 3127
7	0.15	0.18	3.92	0.1205	0.00074 0829	1699.85	0.17327 7268	0.18	0.35401 8097	0.22216 0767
8	0.15	0.18	3.91	0.1177	0.00070 6801	1702.71	0.17356 8807	0.18	0.35427 5608	0.21699 8525
9	0.15	0.18	3.9	0.1156	0.00068 1804	1705.58	0.17386 1366	0.18	0.35454 317	0.21312 6844
10	0.15	0.18	3.89	0.1152	0.00067 7094	1709.11	0.17422 1203	0.18	0.35489 8297	0.21238 9381
11	0.15	0.18	3.88	0.1168	0.00069 6033	1713.65	0.17468 3996	0.18	0.35538 0029	0.21533 9233
12	0.15	0.18	3.87	0.1187	0.00071 8862	1718.18	0.17514 577	0.18	0.35586 4631	0.21884 2183
13	0.15	0.18	3.86	0.1223	0.00076 3127	1724.19	0.17575 841	0.18	0.35652 1537	0.22547 9351
14	0.15	0.18	3.85	0.126	0.00081	1730.24	0.17637 5127	0.18	0.35718 5127	0.23230 0885
15	0.15	0.18	3.84	0.1296	0.00085 6947	1740.41	0.17741 1825	0.18	0.35826 8772	0.23893 8053

TABLE-34 DOWNSTREAM READING FOR HORIZONTAL L OBSTRUCTION AT HEAD=5cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION VERTICAL (v=..3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0811	0.000335572	3352.29	0.341721713	0.03	0.372057284	0.149520649
2	0.15	0.03	3.49	0.1003	0.00051327	3362.2	0.342731906	0.03	0.373245176	0.184918879
3	0.15	0.03	3.48	0.1198	0.000732247	3372.1	0.343741081	0.03	0.374473327	0.220870206
4	0.15	0.03	3.47	0.1334	0.000907937	3380.14	0.344560652	0.03	0.375468589	0.245943953
5	0.15	0.03	3.46	0.1446	0.001066794	3387.46	0.34530683	0.03	0.376373624	0.26659292
6	0.15	0.03	3.45	0.1559	0.001240041	3394.8	0.346055046	0.03	0.377295087	0.287426254
7	0.15	0.03	3.44	0.1641	0.001373919	3401.31	0.346718654	0.03	0.378092573	0.302544248
8	0.15	0.03	3.43	0.1722	0.0015129	3407.76	0.347376147	0.03	0.378889047	0.317477876
9	0.15	0.03	3.42	0.1804	0.001660416	3414.24	0.348036697	0.03	0.379697114	0.33259587
10	0.15	0.03	3.41	0.1876	0.0017956	3420.19	0.348643221	0.03	0.380438821	0.345870206
11	0.15	0.03	3.4	0.1939	0.001918225	3425.66	0.349200815	0.03	0.38111904	0.357485251
12	0.15	0.03	3.39	0.1003	0.00051327	3431.14	0.349759429	0.03	0.380272699	0.184918879
13	0.15	0.03	3.38	0.1068	0.000581951	3436.63	0.350319062	0.03	0.380901013	0.196902655
14	0.15	0.03	3.37	0.1123	0.000643433	3441.26	0.35079103	0.03	0.381434463	0.207042773
15	0.15	0.03	3.36	0.1171	0.000699613	3445.38	0.351211009	0.03	0.381910622	0.21589233

TABLE-35 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=5cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION horizontal (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.1724	0.001516416	1007.08	0.102658512	0.18	0.284174928	0.317846608
2	0.15	0.18	3.97	0.1277	0.000832005	1013.71	0.103334353	0.18	0.284166357	0.235435103
3	0.15	0.18	3.96	0.1018	0.000528737	1027.97	0.104787971	0.18	0.285316708	0.187684366
4	0.15	0.18	3.95	0.08	0.000326531	1084.54	0.110554536	0.18	0.290881067	0.147492625
5	0.15	0.18	3.94	0.0656	0.000219559	1113.59	0.1135158	0.18	0.293735359	0.120943953
6	0.15	0.18	3.93	0.055	0.000154337	1123.92	0.114568807	0.18	0.294723144	0.10140118
7	0.15	0.18	3.92	0.0485	0.000120013	1132.58	0.11545158	0.18	0.295571593	0.089417404
8	0.15	0.18	3.91	0.0521	0.00013849	1136.96	0.115898063	0.18	0.296036554	0.096054572
9	0.15	0.18	3.9	0.0501	0.000128062	956.856	0.097538838	0.18	0.2776669	0.092367257
10	0.15	0.18	3.89	0.0501	0.000128062	858.856	0.087549032	0.18	0.267677093	0.092367257
11	0.15	0.18	3.88	0.0568	0.000164604	1177.8	0.120061162	0.18	0.300225766	0.104719764
12	0.15	0.18	3.87	0.1456	0.0010816	1297.2	0.132232416	0.18	0.313314016	0.268436578
13	0.15	0.18	3.86	0.1567	0.001252801	1291.53	0.131654434	0.18	0.312907235	0.28890118
14	0.15	0.18	3.85	0.1697	0.00146929	1265.34	0.128984709	0.18	0.310454	0.312868732
15	0.15	0.18	3.84	0.1771	0.001600225	1248.29	0.127246687	0.18	0.308846912	0.326511799

TABLE-36 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=5cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION horizontal (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.043	0.00219 3878	2764.5	0.28180 4281	0.03	0.31399 8159	0.07927 7286
2	0.15	0.03	3.49	0.0369	0.00188 2653	2771.08	0.28247 5025	0.03	0.31435 7679	0.06803 0973
3	0.15	0.03	3.48	0.0561	0.00286 2245	2777.72	0.28315 1886	0.03	0.31601 4131	0.10342 9204
4	0.15	0.03	3.47	0.0604	0.00308 1633	2788.21	0.28422 1203	0.03	0.31730 2836	0.11135 6932
5	0.15	0.03	3.46	0.0694	0.00354 0816	2798.57	0.28527 7268	0.03	0.31881 8084	0.12794 9853
6	0.15	0.03	3.45	0.0787	0.00401 5306	2808.84	0.28632 4159	0.03	0.32033 9465	0.14509 587
7	0.15	0.03	3.44	0.0845	0.00431 1224	2819.54	0.28741 4883	0.03	0.32172 6107	0.15578 9086
8	0.15	0.03	3.43	0.091	0.00464 2857	2830.13	0.28849 4393	0.03	0.32313 7251	0.16777 2861
9	0.15	0.03	3.42	0.0984	0.00502 0408	2840.53	0.28955 4536	0.03	0.32457 4944	0.18141 5929
10	0.15	0.03	3.41	0.1065	0.00543 3673	2850.73	0.29059 4292	0.03	0.32602 7965	0.19634 9558
11	0.15	0.03	3.4	0.1115	0.00568 8776	2849.9	0.29050 9684	0.03	0.32619 846	0.20556 7847
12	0.15	0.03	3.39	0.1155	0.00589 2857	2845.28	0.29003 8736	0.03	0.32593 1593	0.21294 2478
13	0.15	0.03	3.38	0.1195	0.00609 6939	2840.5	0.28955 1478	0.03	0.32564 8417	0.22031 7109
14	0.15	0.03	3.37	0.1235	0.00630 102	2835.57	0.28904 893	0.03	0.32534 995	0.22769 174
15	0.15	0.03	3.36	0.1276	0.00651 0204	2837.47	0.28924 261	0.03	0.32575 2814	0.23525 0737

TABLE-37 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=5cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION horizontal (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.2164	0.002389233	1174.34	0.119708461	0.18	0.302097693	0.398967552
2	0.15	0.18	3.97	0.1832	0.001712359	1184.53	0.120747197	0.18	0.302459556	0.337758112
3	0.15	0.18	3.96	0.1538	0.001206859	1189.89	0.121293578	0.18	0.302500437	0.283554572
4	0.15	0.18	3.95	0.1295	0.000855625	1204.05	0.122737003	0.18	0.303592628	0.238753687
5	0.15	0.18	3.94	0.1066	0.000579773	1234.69	0.125860347	0.18	0.30644012	0.196533923
6	0.15	0.18	3.93	0.0961	0.000471184	1272.13	0.12967686	0.18	0.310148045	0.177175516
7	0.15	0.18	3.92	0.0474	0.000114631	1198.42	0.122163099	0.18	0.302277729	0.087389381
8	0.15	0.18	3.91	0.0178	1.61653E-05	1084.82	0.110583078	0.18	0.290599244	0.032817109
9	0.15	0.18	3.9	0.0182	0.0000169	976.038	0.09949419	0.18	0.27951109	0.033554572
10	0.15	0.18	3.89	0.0325	5.38903E-05	1296.35	0.13214577	0.18	0.31219966	0.059918879
11	0.15	0.18	3.88	0.1338	0.00091339	1411.6	0.143893986	0.18	0.324807376	0.246681416
12	0.15	0.18	3.87	0.194	0.001920204	1458.75	0.148700306	0.18	0.33062051	0.357669617
13	0.15	0.18	3.86	0.2052	0.002148318	1452.17	0.148029562	0.18	0.33017788	0.378318584
14	0.15	0.18	3.85	0.218	0.002424694	1428.45	0.145611621	0.18	0.328036315	0.401917404
15	0.15	0.18	3.84	0.2251	0.002585205	1423.93	0.145150866	0.18	0.327736071	0.415007375

TABLE-38 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=5cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION horizontal (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0203	0.001035714	3009.79	0.306808359	0.03	0.337844073	0.037426254
2	0.15	0.03	3.49	0.033	0.001683673	3010.93	0.306924567	0.03	0.33860824	0.060840708
3	0.15	0.03	3.48	0.0404	0.002061224	3013.15	0.307150866	0.03	0.339212091	0.074483776
4	0.15	0.03	3.47	0.0479	0.002443878	3015.37	0.307377166	0.03	0.339821044	0.088311209
5	0.15	0.03	3.46	0.0534	0.00272449	3019.14	0.307761468	0.03	0.340485958	0.098451327
6	0.15	0.03	3.45	0.0591	0.003015306	3022.92	0.308146789	0.03	0.341162095	0.108960177
7	0.15	0.03	3.44	0.0642	0.00327551	3027.41	0.308604485	0.03	0.341879995	0.118362832
8	0.15	0.03	3.43	0.0688	0.003510204	3032.82	0.309155963	0.03	0.342666167	0.126843658
9	0.15	0.03	3.42	0.0735	0.00375	3038.21	0.309705403	0.03	0.343455403	0.13550885
10	0.15	0.03	3.41	0.0781	0.003984694	3043.67	0.310261978	0.03	0.344246671	0.143989676
11	0.15	0.03	3.4	0.0823	0.00419898	3049.43	0.310849134	0.03	0.345048113	0.151733038
12	0.15	0.03	3.39	0.0866	0.004418367	3055.18	0.31143527	0.03	0.345853637	0.159660767
13	0.15	0.03	3.38	0.0909	0.004637755	3060.9	0.312018349	0.03	0.346656104	0.167588496
14	0.15	0.03	3.37	0.0952	0.004857143	3066.62	0.312601427	0.03	0.34745857	0.175516224
15	0.15	0.03	3.36	0.0997	0.005086735	3072.43	0.31319368	0.03	0.348280415	0.183812684

TABLE-39 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=5cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION horizontal (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.1944	0.001928131	1207.08	0.123045872	0.18	0.304974002	0.35840708
2	0.15	0.18	3.97	0.15545	0.001232893	1213.71	0.123721713	0.18	0.304954606	0.286596608
3	0.15	0.18	3.96	0.1278	0.000833308	1227.97	0.125175331	0.18	0.306008639	0.235619469
4	0.15	0.18	3.95	0.10475	0.000559825	1284.54	0.130941896	0.18	0.311501721	0.193123156
5	0.15	0.18	3.94	0.0861	0.000378225	1313.59	0.13390316	0.18	0.314281385	0.158738938
6	0.15	0.18	3.93	0.07555	0.000291214	1323.92	0.134956167	0.18	0.315247382	0.139288348
7	0.15	0.18	3.92	0.04795	0.000117306	1332.58	0.13583894	0.18	0.315956246	0.088403392
8	0.15	0.18	3.91	0.03495	6.23216E-05	1336.96	0.136285423	0.18	0.316347745	0.064435841
9	0.15	0.18	3.9	0.03415	5.95011E-05	1356.856	0.138313558	0.18	0.318373059	0.062960914
10	0.15	0.18	3.89	0.0413	0.000087025	1258.856	0.128323751	0.18	0.308410776	0.076143068
11	0.15	0.18	3.88	0.0953	0.000463372	1377.8	0.140448522	0.18	0.320911894	0.17570059
12	0.15	0.18	3.87	0.1698	0.001471022	1597.2	0.162813456	0.18	0.344284478	0.313053097
13	0.15	0.18	3.86	0.18095	0.001670556	1591.53	0.162235474	0.18	0.34390603	0.333609882
14	0.15	0.18	3.85	0.19385	0.001917236	1565.34	0.159565749	0.18	0.341482985	0.357393068
15	0.15	0.18	3.84	0.2011	0.002063327	1548.29	0.157827727	0.18	0.339891054	0.370759587

TABLE-40 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=5cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION horizontal (v=.3461 m/s)(h=5 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0103	0.00052551	3264.5	0.332772681	0.03	0.363298191	0.018989676
2	0.15	0.03	3.49	0.013	0.000663265	3271.08	0.333443425	0.03	0.36410669	0.023967552
3	0.15	0.03	3.48	0.0104	0.000530612	3277.72	0.334120285	0.03	0.364650898	0.019174041
4	0.15	0.03	3.47	0.0189	0.000964286	3288.21	0.335189602	0.03	0.366153888	0.034845133
5	0.15	0.03	3.46	0.0234	0.001193878	3298.57	0.336245668	0.03	0.367439545	0.043141593
6	0.15	0.03	3.45	0.0391	0.001994898	3208.84	0.327098879	0.03	0.359093777	0.072087021
7	0.15	0.03	3.44	0.0442	0.002255102	3219.54	0.328189602	0.03	0.360444704	0.081489676
8	0.15	0.03	3.43	0.0488	0.002489796	3230.13	0.329269113	0.03	0.361758909	0.089970501
9	0.15	0.03	3.42	0.0485	0.00247449	3240.53	0.330329256	0.03	0.362803746	0.089417404
10	0.15	0.03	3.41	0.0511	0.002607143	3250.73	0.331369011	0.03	0.363976154	0.094210914
11	0.15	0.03	3.4	0.0723	0.003688776	3249.9	0.331284404	0.03	0.364973179	0.13329646
12	0.15	0.03	3.39	0.0766	0.003908163	3245.28	0.330813456	0.03	0.364721619	0.141224189
13	0.15	0.03	3.38	0.0809	0.004127551	3240.5	0.330326198	0.03	0.364453749	0.149151917
14	0.15	0.03	3.37	0.0852	0.004346939	3235.57	0.329823649	0.03	0.364170588	0.157079646
15	0.15	0.03	3.36	0.0897	0.004576531	3237.47	0.330017329	0.03	0.36459386	0.165376106

TABLE-41 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=8cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.3412	0.005939665	1498.91	0.152794088	0.18	0.338733753	0.629056047
2	0.15	0.18	3.97	0.3212	0.005263747	1507.74	0.15369419	0.18	0.338957937	0.592182891
3	0.15	0.18	3.96	0.2973	0.004509556	1515.55	0.154490316	0.18	0.338999872	0.548119469
4	0.15	0.18	3.95	0.2744	0.0038416	1523.44	0.155294597	0.18	0.339136197	0.505899705
5	0.15	0.18	3.94	0.2562	0.0033489	1526.67	0.155623853	0.18	0.338972753	0.472345133
6	0.15	0.18	3.93	0.2407	0.002955943	1527.37	0.155695209	0.18	0.338651152	0.443768437
7	0.15	0.18	3.92	0.2258	0.002601308	1528.09	0.155768603	0.18	0.338369912	0.416297935
8	0.15	0.18	3.91	0.2127	0.002308229	1527.5	0.155708461	0.18	0.33801669	0.392146018
9	0.15	0.18	3.9	0.2001	0.002042858	1526.92	0.155649337	0.18	0.337692195	0.368915929
10	0.15	0.18	3.89	0.1883	0.001809025	1526.61	0.155617737	0.18	0.337426762	0.347160767
11	0.15	0.18	3.88	0.1776	0.001609273	1526.67	0.155623853	0.18	0.337233127	0.327433628
12	0.15	0.18	3.87	0.1672	0.001426318	1526.75	0.155632008	0.18	0.337058327	0.308259587
13	0.15	0.18	3.86	0.1591	0.00129147	1527.35	0.15569317	0.18	0.33698464	0.293325959
14	0.15	0.18	3.85	0.1513	0.001167943	1527.96	0.155755352	0.18	0.336923295	0.278945428
15	0.15	0.18	3.84	0.1446	0.001066794	1531.8	0.156146789	0.18	0.337213583	0.26659292

TABLE-42 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=8cm IN NO OBSTRUCTION

WITHOUT OBSTRUCTION VERTICAL (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.05	0.0409	8.53474 E-05	3115.39	0.31757 2885	0.03	0.34765 8232	0.07540 5605
2	0.15	0.03	3.49	0.0519	0.00013 7429	3119.05	0.31794 5973	0.03	0.34808 3403	0.09568 5841
3	0.15	0.03	3.48	0.0672	0.00023 04	3122.79	0.31832 7217	0.03	0.34855 7617	0.12389 3805
4	0.15	0.03	3.47	0.0783	0.00031 2801	3127.18	0.31877 472	0.03	0.34908 752	0.14435 8407
5	0.15	0.03	3.46	0.0872	0.00038 7951	3132	0.31926 6055	0.03	0.34965 4006	0.16076 6962
6	0.15	0.03	3.45	0.0963	0.00047 3147	3136.83	0.31975 841	0.03	0.35023 1557	0.17754 4248
7	0.15	0.03	3.44	0.1033	0.00054 4433	3142.29	0.32031 4985	0.03	0.35085 9418	0.19044 9853
8	0.15	0.03	3.43	0.1103	0.00062 0719	3147.81	0.32087 7676	0.03	0.35149 8395	0.20335 5457
9	0.15	0.03	3.42	0.1173	0.00070 2005	3153.35	0.32144 2406	0.03	0.35214 441	0.21626 1062
10	0.15	0.03	3.41	0.1236	0.00077 9437	3158.93	0.32201 1213	0.03	0.35279 065	0.22787 6106
11	0.15	0.03	3.4	0.1294	0.00085 4304	3164.65	0.32259 4292	0.03	0.35344 8596	0.23856 9322
12	0.15	0.03	3.39	0.1353	0.00093 3984	3170.34	0.32317 4312	0.03	0.35410 8296	0.24944 6903
13	0.15	0.03	3.38	0.1412	0.00101 7216	3176.04	0.32375 5352	0.03	0.35477 2568	0.26032 4484
14	0.15	0.03	3.37	0.1466	0.00109 6508	3181.51	0.32431 2946	0.03	0.35540 9454	0.27028 0236
15	0.15	0.03	3.36	0.1518	0.00117 5676	3186.84	0.32485 6269	0.03	0.35603 1945	0.27986 7257

TABLE-43 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=8cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION horizontal (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.3193	0.005201658	1486.22	0.15150051	0.18	0.336702167	0.588679941
2	0.15	0.18	3.97	0.3062	0.004783594	1485.61	0.151438328	0.18	0.336221922	0.564528024
3	0.15	0.18	3.96	0.2881	0.004234776	1501.94	0.153102956	0.18	0.337337732	0.531157817
4	0.15	0.18	3.95	0.2778	0.00393739	1531.66	0.156132518	0.18	0.340069908	0.512168142
5	0.15	0.18	3.94	0.252	0.00324	1544.77	0.157468909	0.18	0.340708909	0.46460177
6	0.15	0.18	3.93	0.2137	0.002329984	1546.7	0.157665647	0.18	0.339995631	0.393989676
7	0.15	0.18	3.92	0.1462	0.001090533	1583.84	0.16145158	0.18	0.342542113	0.269542773
8	0.15	0.18	3.91	0.0866	0.000382631	1477.27	0.150588175	0.18	0.330970806	0.159660767
9	0.15	0.18	3.9	0.0661	0.000222919	1238.4	0.126238532	0.18	0.306461451	0.121865782
10	0.15	0.18	3.89	0.0682	0.000237308	1388.61	0.141550459	0.18	0.321787767	0.125737463
11	0.15	0.18	3.88	0.1592	0.001293094	1477.17	0.150577982	0.18	0.331871076	0.293510324
12	0.15	0.18	3.87	0.2324	0.0027556	1507.52	0.153671764	0.18	0.336427364	0.428466077
13	0.15	0.18	3.86	0.2442	0.003042533	1517.23	0.15466157	0.18	0.337704102	0.450221239
14	0.15	0.18	3.85	0.2626	0.003518304	1498.09	0.152710499	0.18	0.336228804	0.484144543
15	0.15	0.18	3.84	0.2727	0.003794147	1499.08	0.152811417	0.18	0.336605564	0.502765487

TABLE-44 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=8cm IN 10% OBSTRUCTION

WITH 10% OBSTRUCTION horizontal (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0309	0.00157 6531	3330.24	0.33947 4006	0.03	0.37105 0537	0.05696 9027
2	0.15	0.03	3.49	0.041	0.00209 1837	3332.26	0.33967 9918	0.03	0.37177 1755	0.07558 9971
3	0.15	0.03	3.48	0.051	0.00260 2041	3334.13	0.33987 054	0.03	0.37247 2581	0.09402 6549
4	0.15	0.03	3.47	0.0554	0.00282 6531	3332.87	0.33974 21	0.03	0.37256 8631	0.10213 8643
5	0.15	0.03	3.46	0.0604	0.00308 1633	3331.45	0.33959 735	0.03	0.37267 8982	0.11135 6932
6	0.15	0.03	3.45	0.0656	0.00334 6939	3329.88	0.33943 7309	0.03	0.37278 4248	0.12094 3953
7	0.15	0.03	3.44	0.0666	0.00339 7959	3336.38	0.34009 9898	0.03	0.37349 7857	0.12278 7611
8	0.15	0.03	3.43	0.0677	0.00345 4082	3343.81	0.34085 7288	0.03	0.37431 137	0.12481 5634
9	0.15	0.03	3.42	0.0692	0.00353 0612	3350.99	0.34158 9195	0.03	0.37511 9807	0.12758 1121
10	0.15	0.03	3.41	0.0711	0.00362 7551	3357.99	0.34230 2752	0.03	0.37593 0303	0.13108 4071
11	0.15	0.03	3.4	0.0776	0.00395 9184	3371.58	0.34368 8073	0.03	0.37764 7257	0.14306 7847
12	0.15	0.03	3.39	0.0859	0.00438 2653	3387.34	0.34529 4597	0.03	0.37967 725	0.15837 0206
13	0.15	0.03	3.38	0.0947	0.00483 1633	3303.06	0.33670 3364	0.03	0.37153 4997	0.17459 4395
14	0.15	0.03	3.37	0.1038	0.00529 5918	3318.74	0.33830 1733	0.03	0.37359 7651	0.19137 1681
15	0.15	0.03	3.36	0.1131	0.00577 0408	3334.39	0.33989 7044	0.03	0.37566 7452	0.20851 7699

TABLE-45 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=8cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION horizontal (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.3623	0.006697005	1301	0.132619776	0.18	0.31931678	0.667957227
2	0.15	0.18	3.97	0.3406	0.005918794	1294.11	0.131917431	0.18	0.317836225	0.627949853
3	0.15	0.18	3.96	0.321	0.005257194	1285.44	0.131033639	0.18	0.316290833	0.591814159
4	0.15	0.18	3.95	0.2999	0.004588776	1278.18	0.130293578	0.18	0.314882354	0.552912979
5	0.15	0.18	3.94	0.2718	0.003769145	1287.02	0.131194699	0.18	0.314963844	0.501106195
6	0.15	0.18	3.93	0.2037	0.002117025	1328.35	0.135407747	0.18	0.317524772	0.375553097
7	0.15	0.18	3.92	0.092	0.000431837	1315.4	0.134087666	0.18	0.314519502	0.169616519
8	0.15	0.18	3.91	0.0385	0.000075625	1243.46	0.126754332	0.18	0.306829957	0.070980826
9	0.15	0.18	3.9	0.0398	8.08184E-05	1259.33	0.128372069	0.18	0.308452888	0.073377581
10	0.15	0.18	3.89	0.0806	0.000331447	1284.46	0.130933741	0.18	0.311265188	0.14859882
11	0.15	0.18	3.88	0.1207	0.00074329	1298.97	0.132412844	0.18	0.313156134	0.222529499
12	0.15	0.18	3.87	0.1207	0.00074329	1317.17	0.134268094	0.18	0.315011384	0.222529499
13	0.15	0.18	3.86	0.1268	0.000820318	1327.17	0.135287462	0.18	0.31610778	0.233775811
14	0.15	0.18	3.85	0.1391	0.000987184	1333.29	0.135911315	0.18	0.316898499	0.256452802
15	0.15	0.18	3.84	0.1527	0.001189658	1337.08	0.136297655	0.18	0.317487313	0.281526549

TABLE-46 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=8cm IN 20% OBSTRUCTION

WITH 20% OBSTRUCTION horizontal (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0323	0.001647959	2978.71	0.303640163	0.03	0.335288122	0.059550147
2	0.15	0.03	3.49	0.0438	0.002234694	2980.35	0.303807339	0.03	0.336042033	0.080752212
3	0.15	0.03	3.48	0.0549	0.00280102	2983.01	0.304078491	0.03	0.336879512	0.101216814
4	0.15	0.03	3.47	0.0648	0.003306122	2985.86	0.304369011	0.03	0.337675134	0.119469027
5	0.15	0.03	3.46	0.0724	0.003693878	2989.77	0.304767584	0.03	0.338461462	0.133480826
6	0.15	0.03	3.45	0.0788	0.004020408	2994.24	0.305223242	0.03	0.33924365	0.145280236
7	0.15	0.03	3.44	0.0853	0.004352041	2998.71	0.305678899	0.03	0.34003094	0.157264012
8	0.15	0.03	3.43	0.0913	0.004658163	3004.28	0.306246687	0.03	0.34090485	0.168325959
9	0.15	0.03	3.42	0.0973	0.004964286	3009.99	0.306828746	0.03	0.341793032	0.179387906
10	0.15	0.03	3.41	0.1034	0.00527551	3015.68	0.307408767	0.03	0.342684277	0.190634218
11	0.15	0.03	3.4	0.1097	0.005596939	3021.56	0.308008155	0.03	0.343605094	0.202249263
12	0.15	0.03	3.39	0.1157	0.005903061	3028.05	0.308669725	0.03	0.344572786	0.213311209
13	0.15	0.03	3.38	0.1218	0.006214286	3034.56	0.309333333	0.03	0.345547619	0.224557522
14	0.15	0.03	3.37	0.128	0.006530612	3041.05	0.309994903	0.03	0.346525515	0.235988201
15	0.15	0.03	3.36	0.1343	0.006852041	3047.53	0.310655454	0.03	0.347507494	0.247603245

TABLE-47 UPSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=8cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION horizontal (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEAD	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.18	3.98	0.3465	0.006125625	1487.69	0.151650357	0.18	0.337775982	0.638827434
2	0.15	0.18	3.97	0.3231	0.005326205	1487.23	0.151603466	0.18	0.33692967	0.595685841
3	0.15	0.18	3.96	0.3034	0.004696508	1486.79	0.151558614	0.18	0.336255122	0.559365782
4	0.15	0.18	3.95	0.2745	0.003844401	1487.76	0.151657492	0.18	0.335501893	0.506084071
5	0.15	0.18	3.94	0.2368	0.002860931	1514.37	0.154370031	0.18	0.337230961	0.436578171
6	0.15	0.18	3.93	0.1187	0.000718862	1524.21	0.155373089	0.18	0.33609195	0.218842183
7	0.15	0.18	3.92	0.0089	4.04133E-06	1322.59	0.134820591	0.18	0.314824633	0.016408555
8	0.15	0.18	3.91	0.0092	4.31837E-06	1343.59	0.136961264	0.18	0.316965582	0.016961652
9	0.15	0.18	3.9	0.101	0.000520459	1436.41	0.146423038	0.18	0.326943497	0.18620944
10	0.15	0.18	3.89	0.2106	0.002262876	1495.44	0.152440367	0.18	0.334703242	0.388274336
11	0.15	0.18	3.88	0.267	0.003637194	1505.96	0.153512742	0.18	0.337149936	0.492256637
12	0.15	0.18	3.87	0.2709	0.003744225	1507.26	0.15364526	0.18	0.337389485	0.499446903
13	0.15	0.18	3.86	0.2813	0.004037229	1507.33	0.153652396	0.18	0.337689625	0.518620944
14	0.15	0.18	3.85	0.2965	0.004485319	1507.75	0.153695209	0.18	0.338180528	0.546644543
15	0.15	0.18	3.84	0.3084	0.00485258	1514.29	0.154361876	0.18	0.339214455	0.568584071

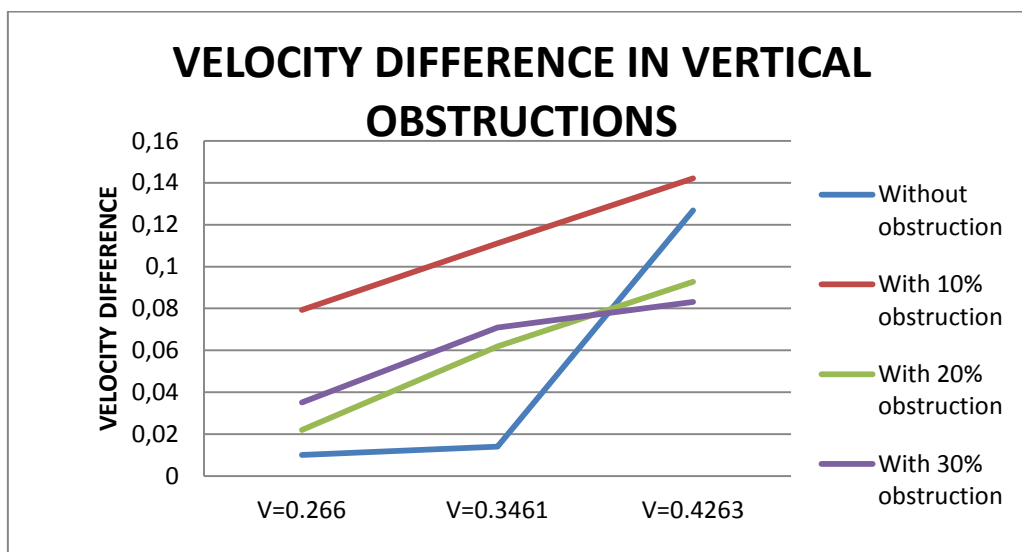
TABLE-48 DOWNSTREAM READING FOR HORIZONTAL OBSTRUCTION AT HEAD=8cm IN 30% OBSTRUCTION

WITH 30% OBSTRUCTION horizontal (v=.4263 m/s)(h=8 cm)										
S. N O.	POSITION			VELO CITY	VELO CITY HEAD	PRESS URE	PRESS URE HEAD	DAT UM HEA D	TOTA L HEAD	FROU DE NO.
	X	Y	Z							
1	0.15	0.03	3.5	0.0401	0.002045918	3030.67	0.308936799	0.03	0.340982718	0.073930678
2	0.15	0.03	3.49	0.0602	0.003071429	3035.47	0.309426096	0.03	0.342497524	0.110988201
3	0.15	0.03	3.48	0.0724	0.003693878	3040.37	0.309925586	0.03	0.343619464	0.133480826
4	0.15	0.03	3.47	0.0847	0.004321429	3045.28	0.310426096	0.03	0.344747524	0.156157817
5	0.15	0.03	3.46	0.0939	0.004790816	3051.3	0.311039755	0.03	0.345830572	0.173119469
6	0.15	0.03	3.45	0.1032	0.005265306	3057.45	0.311666667	0.03	0.346931973	0.190265487
7	0.15	0.03	3.44	0.1123	0.005729592	3063.86	0.312320082	0.03	0.348049673	0.207042773
8	0.15	0.03	3.43	0.1211	0.006178571	3070.74	0.313021407	0.03	0.349199978	0.223266962
9	0.15	0.03	3.42	0.1299	0.006627551	3077.6	0.313720693	0.03	0.350348244	0.23949115
10	0.15	0.03	3.41	0.1388	0.007081633	3084.5	0.314424057	0.03	0.35150569	0.255899705
11	0.15	0.03	3.4	0.1468	0.007489796	3091.7	0.315158002	0.03	0.352647798	0.270648968
12	0.15	0.03	3.39	0.155	0.007908163	3098.89	0.315890928	0.03	0.353799091	0.285766962
13	0.15	0.03	3.38	0.1632	0.008326531	3106.07	0.316622834	0.03	0.354949364	0.300884956
14	0.15	0.03	3.37	0.1714	0.008744898	3113.25	0.31735474	0.03	0.356099638	0.31600295
15	0.15	0.03	3.36	0.1784	0.009102041	3120.36	0.318079511	0.03	0.357181552	0.328908555

CHAPTER-6

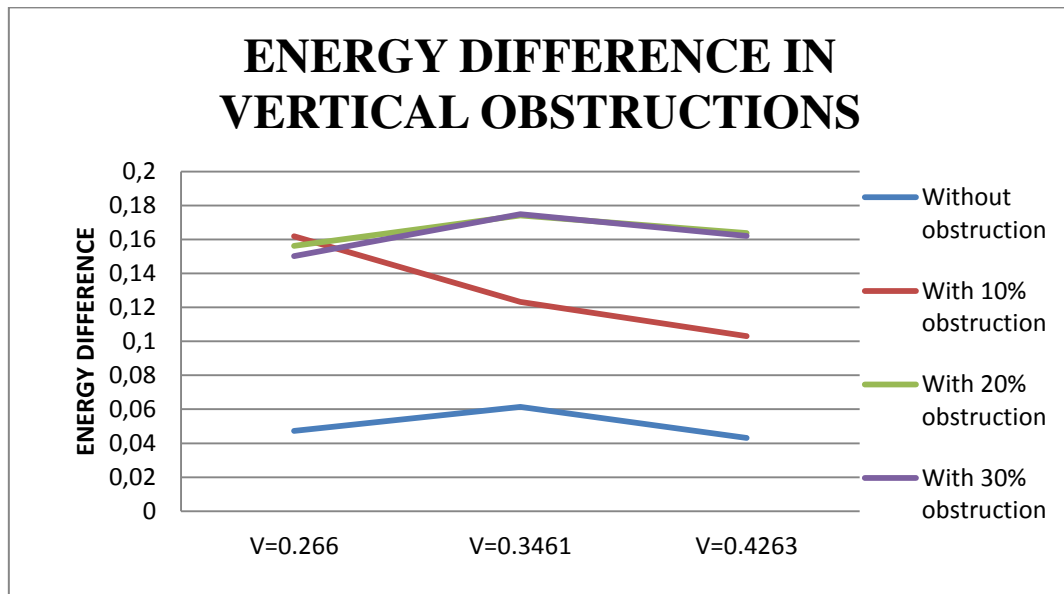
CONCLUSION

In the case of vertical obstructions when we increase the velocity (as head is increased then we observe):



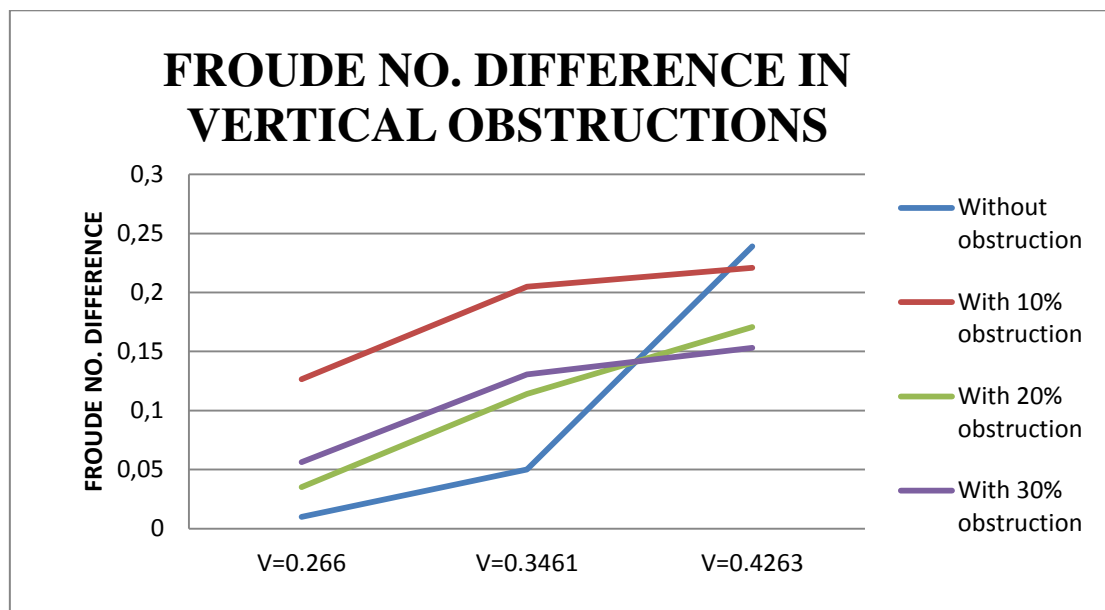
1. In the above case a reduction of 0.1269 in the case of ($v=0.4263$ & without obstruction) is observed due to constant decrease in velocity along the flow through the steps.
2. We can see as the velocity increases respective values of decrease in velocity also increases.
3. When we observe the velocity reduction with respect to % obstruction then we observe that there is a max. reduction of velocity in 10% obstruction case then there is not much significant increase in the velocity as the % obstruction increases.

In the case of vertical obstructions when we observe the ENERGY HEAD



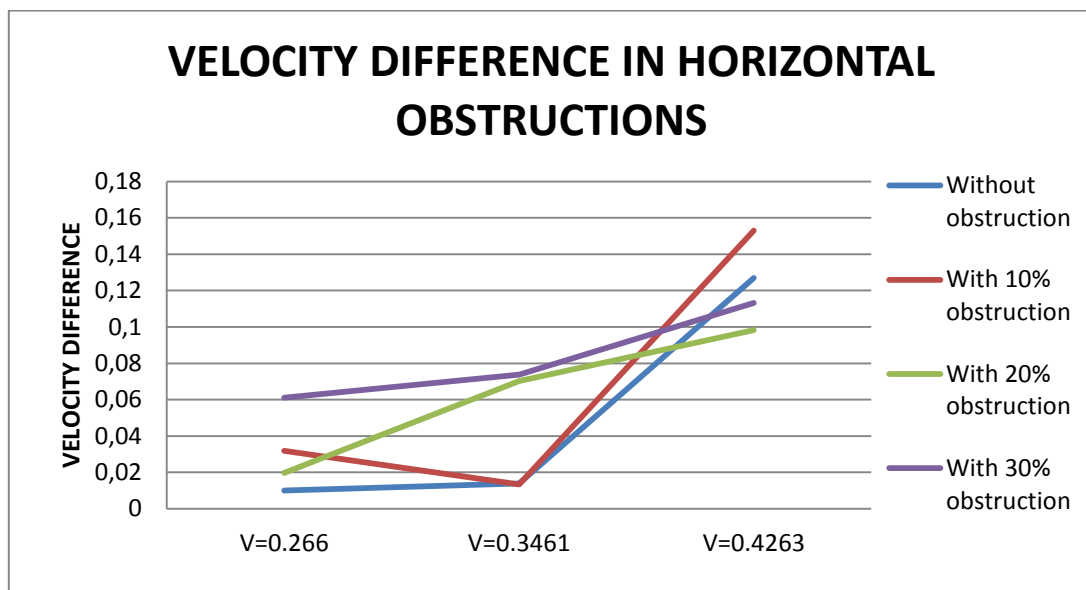
Here also we observe the energy reduction with respect to % obstruction then we observe that there is a max. reduction of energy in 10% obstruction case then there is not much significant increase in the energy as the % obstruction increases.

In the case of vertical obstructions when we observe the FROUDE NO.



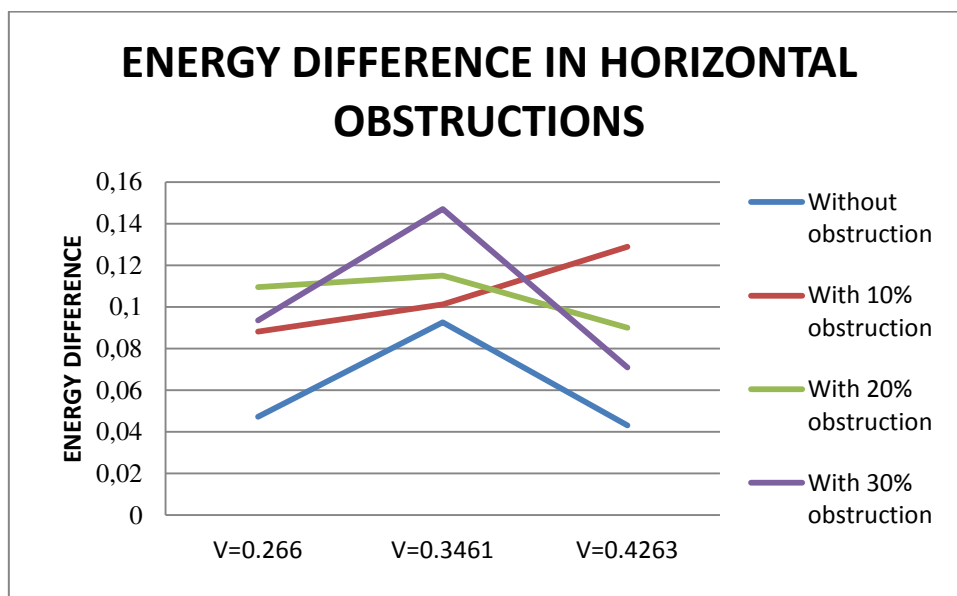
Here also we observe the Froude no. reduction with respect to % obstruction then we observe that there is a max. reduction of Froude no. in 10% obstruction case then there is not much significant increase in the Froude no. as the % obstruction increases.

In the case of horizontal obstructions when we increase the velocity (as head is increased) then we observe:



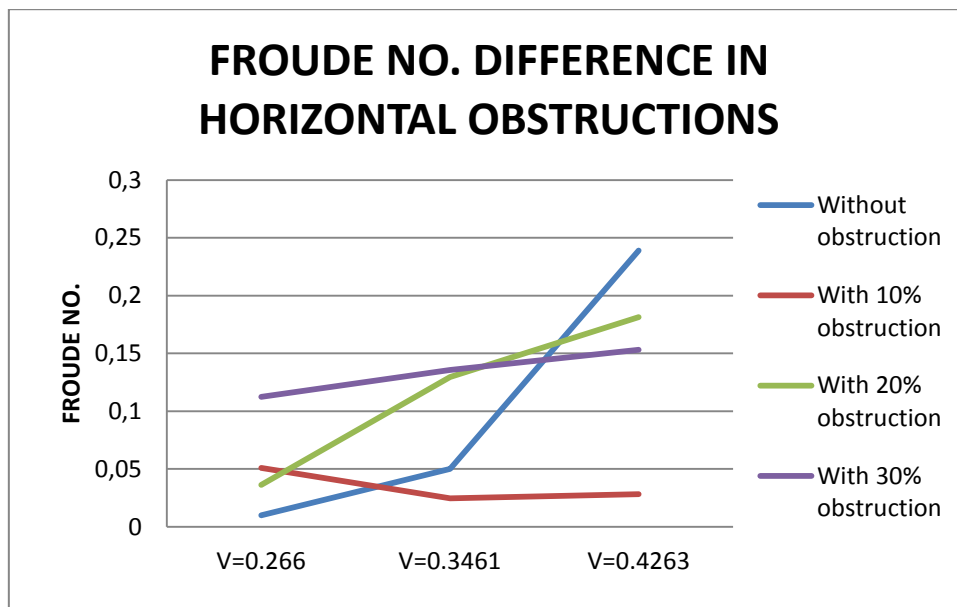
1. Here we observe the velocity reduction with respect to % obstruction then we observe that with increase in % obstruction there is respective increase in difference of velocity. So we can say that in case of horizontal obstruction we can also increase obstruction beyond 30% if possible.
2. Also we observe that except for 10% obstruction case velocity reduction is comparatively higher

In the case of horizontal obstructions when we observe the ENERGY HEAD



Here we observe the energy reduction with respect to % obstruction then we observe that with increase in % obstruction there is approximately not much effect on energy reduction since there was corresponding increase in pressure downstream .

In the case of horizontal obstructions when we observe the FROUDE NO.



.Here we observe the Froude no. reduction with respect to % obstruction then we observe that with increase in % obstruction there is respective increase in difference of Froude no. So we can say that in case of horizontal obstruction we can also increase obstruction beyond 30% if possible.

CHAPTER-7

REFERENCES

1. Chanson H, Yasuda Y, Ohtsu I. Flow resistance in skimming flow: a critical review. In: Minor HE, Hager WH, editors. Proc international workshop on hydraulics of stepped spillways. Zurich (Switzerland): Balkema; 2000.p. 95–102
2. Christodoulou GC. Design of stepped spillways for optimal energy dissipation. *Hydropower Dams* 1999(5):90–3.
3. Asadi Ebrahim, Dalir Ali Hosseinzadeh, Farsadizadeh Davood, Hassanzadeh Yousef, Salmasi Farzin. Energy dissipation of skimming flow with different sill dimensions in stepped spillway model. *Int J Agric Biosci* 2015;4(3):118–21.
4. Fratino U, Piccinni A. Dissipation efficiency of stepped spillways. In: Minor H-E, Hager W, editors. Proceeding of the international workshop on hydraulics of stepped spillways, IAHR. Zurich (Switzerland): A.A. Balkema/Rotterdam/Brookfield; 2000.
5. Hazzab A, Chafi C. Experimental investigation of flow and energy dissipation in stepped spillways. *Jordan J Civ Eng* 2010;4(1).
6. Ohtsu IO, Yasuda Y. Characteristics of flow conditions on stepped channels. In Proc 27th IAHR biennial congress, San Francisco, USA, Theme D; 1997. p. 583–Mazen T, Jean C, Rita A. Computational simulation of flow over stepped spillways. *J. Comput Struct* 2005;83:2215–24.
7. Peruginelli A, Pagliara S. Energy dissipation comparison among stepped channel, drop and ramp structures. In: Minor H-E, Hager W, editors. Proceeding of the international workshop on hydraulics of stepped spillways, IAHR. Zurich (Switzerland):A.A.Balkema/Rotterdam/Brookfield;
8. Peterka AJ. Hydraulic design of stilling basin and energy dissipaters. Engineering monograph 25. Denver (CO): US Bureau of Reclamation; 1958[Appeared Also As 8th Printing In 1984].
9. Peyras L, Royet P, Degoutte G. Flow and energy dissipation over stepped gabion weirs. *J Hyd Energy, ASCE* 1992;118(5):707–17.
10. Tuna MC. Effect of offtake channel base angle of stepped spillway on scour hole. *IJST, Trans Civ Eng* 2012;36(C2):239–51.
11. Tuna MC, Emiroglu ME. Effect of step geometry on local scour downstream of stepped chutes. *Arabian J Sci Eng* 2012;38(3):579–88.

12. Al-Husseini Thulfikar Razzak. Experimental study of increasing energy dissipation on stepped spillway. *J Kerbala Univ* 2015;13(3) [Scientific].
13. Torabi SMR, Roostami Ravari A, Torabi SAR, Boostani F, Roushan A. Energy dissipation on stepped spillways with reverse inclination. *J Water Eng Summer* 2013;6(17):53–62.
14. N.A. Ali, The proper location of sill with scour reach downstream of heading-up structure, *Bulletin of the Faculty of Engineering, Assuit University, Egypt* 23 (2) (1995) 11–19.
15. L. Valle´ Brett, B. Pasternack Gregory, Submerged and unsubmerged natural hydraulic jumps in a bedrock step-pool mountain channel, *Journal of Geomorphology* 82 (2006) 146–159.
16. A. Claudia, S. Giampiero, Scour due to a horizontal turbulent jet: numerical and experimental investigation, *Journal of Hydraulic Research* 44 (5) (2006) 663–673.
17. A.A. El Masry, M.M. Sobeih, Study of scour at double submarine pipelines due to water currents, *Mansora Engineering Journal, Faculty of Engineering, Mansora University, Egypt* 21 (2) (1996) 13–24.
18. I. El-Azizi, A Study of Submerged Hydraulic Jump Stilling Basins of Low Head Irrigation Structures, M.Sc. Thesis, Faculty of Engineering, Ain Shams University, Egypt, 1985.
19. M.M. El-Gamel, Effect of using three-lines of angle baffles on scour downstream heading-up structures, *Mansora Engineering Journal, Faculty of Engineering, Mansora University, Egypt* 26(2) (2001) 73–85.
20. M.M. El-Gamel, O.S. Ragih, M.M. Sobieh, S.M. El Abd, Experimental study of local scour downstream stilling basins, Figure 9 Relationship between D_s/y_1 and Fr for different shapes I, II, III, IV and V at $S = 4.6$.
21. Effect of stilling basin shape on the hydraulic characteristics 399 *Mansora Engineering Journal, Faculty of Engineering, Mansora University, Egypt* 27 (4) (2002) 90–106.
22. C. Flokstra, Modelling of submerged vanes, *Journal of Hydraulic Research* 44 (5) (2006) 591–602.
23. F. Ma, P. Prinos, Characteristics of submerged hydraulic jump, in: *Proc. of XXV III Congress, Graz, 1999*.
24. N.S. Govinda Rao, N. Rajaratnam, The submerged hydraulic jump, *Journal of Hydraulic Division, ASCE* 89 (HY1) (1963)139–163.
25. E. Habib, M. Mosa, A. Petrillo, Scour downstream of hydraulic jump, in: *Proc. of Hydropower and Dams Conf., Budapest, Hungary, 1994*.
26. N.M.K. Hassan, R. Narayanan, Local scour downstream of an apron, *Journal of Hydraulic Engineering* 111 (11) (1986) 1371–1385.
27. A.M. Khalifa, M. Abdellateef, E. Abdel-Hafiz, Characteristics of scour combined by supercritical flow, *Bulletin, Faculty of Engineering, Ain Shams University* (23) (1989) 135–149.

28. D. Long, P.M. Steffler, N. Rajaratnam, A numerical study of flow structure in submerged jumps, *Journal of Hydraulic Research* 29 (3) (1991) 293–307.
29. F. Ma, Y. Hou, P. Prinos, Numerical calculation of submerged hydraulic jumps, *Journal of Hydraulic Research* 39 (5) (2001) 493–503.
30. J.A. McCorquodale, Abdelkawi M. Khalifa, Submerged radial hydraulic jump, *Journal of the Hydraulics Division, ASCE* 106(3) (1980) 355–367.
31. S. Narasimhan, P. Bhargara, Pressure fluctuations in submerged jump, *Journal of the Hydraulics Division, ASCE* 102 (HY3)(1976) 339–350.
32. I. Ohtsu, Y. Yasuda, M. Ishkikawa, Submerged hydraulic jump below abrupt expansion, *Journal of Hydraulic Engineering, ASCE* 125 (5) (1999) 492–499.
33. N. Rajaratnam, Submerged hydraulic jump, *Journal of the Hydraulic Division* 91 (HY4) (1965) 71–96.
34. N. Rajaratnam, The hydraulic jump as a wall jet, *Journal of the Hydraulic Division* 91 (HY5) (1965) 107–132.
35. N. Rajaratnam, S. Beltaos, Erosion by impinging circular turbulent jets, *Journal of the Hydraulic Division* 103 (HY10)(1977) 1191–1205.
36. N. Rajaratnam, R.K. Macdougall, Erosion by plane wall jets with minimum tailwater, *Journal of Hydraulic Engineering* 109(7) (1983) 1061–1064.
37. O.K. Saleh, A.M. Negm, O.S. Waheed-Eldin, N.G. Ahmad, Effect of end sill on scour characteristics downstream of sudden expanding stilling basins, in: *Proc. of Sixth International River Eng. Conf. Pub. on CD ROM and Booklet of Abstracts, Ahvaz, Iran, 2003.*
38. C.D. Smith, The submerged hydraulic jump in an abrupt lateral expansion, *Journal of Hydraulic Research, ASCE* 27 (2) (1989) 257–266.
39. Dey Subhasish, Sarkar Arindam, Characteristics of turbulent flow in submerged jumps on rough beds, *Journal of Engineering Mechanics* 134 (1) (2008) 49–59.