#### ABSTRACT

The need for studies of control strategies for induction motor drives is justified with the proliferation of application of these drives in industries and production plants where materials have to be both processed and transported and where a high productivity is one of the key factors. This work is focused on developing effective control strategies and configurations for control scheme of industrial induction motor drives. The work is extended to harmonics and reactive power control of the industrial induction motor drive with a PWM converter. The proposed control strategy is analyzed and confirmed by the simulation studies of the mathematical models used.

The complete mathematical model of field orientation control (FOC) and direct torque control (DTC) of induction motor is described and simulated in MATLAB for studies of 200 hp cage type induction motor drives. The indirect vector controlled induction motor drives involve decoupling of the stator current in to torque and flux producing components. PI control is used for the estimation of the instantaneous magnitude of the rotor speed, current and torque. The direct torque control employs direct control of stator flux linkages and the electromagnetic torque by the selection of an optimum voltage vector.

The pulse width modulated (PWM) converter designed as controllable switching pulses generator offers a flexible solution to the problem of current harmonics and reactive power requirement of the designed industrial drives. The dissertation successfully demonstrates the field oriented control and direct torque control fed with a PWM converter topology. Both motor control strategies are compared to decide the performance of the motor.

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#### LIST OF SYMBOLS

Symbols	Description
d <sup>s</sup> -q <sup>s</sup>	Stationary reference frame direct and quadrature axis
$d^{e}-q^{e}$	Synchronously rotating reference frame direct and quadrature axis
$i_{qs}$	q <sup>e</sup> -axis stator current
$i_{qr}$	q <sup>e</sup> -axis rotor current
i <sub>dr</sub>	d <sup>e</sup> -axis rotor current
i <sub>ds</sub>	d <sup>e</sup> -axis stator current
$i_{qs}$	q <sup>e</sup> -axis stator current
$L_m$	Magnetizing inductance
$L_{ls}$	Stator leakage inductance
$L_{lr}$	Rotor leakage inductance
$v_{qs}$	q <sup>e</sup> -axis stator voltage
$v_{ds}$	d <sup>e</sup> -axis stator voltage
$v_{qr}$	q <sup>e</sup> -axis rotor voltage
$v_{dr}$	d <sup>e</sup> -axis rotor voltage
$R_s$	Stator resistance
$R_r$	Rotor resistance
L <sub>s</sub>	Stator inductance
$L_r$	Rotor inductance
$\omega_e$	Stator or line frequency
$\omega_r$	Rotor electrical speed
$\omega_{sl}$	Slip frequency
S	Laplace operator
p	Number of pole
$\theta_e$	Angle of synchronously rotating frame
$\theta_r$	Rotor angle
$\theta_{sl}$	Slip angle
$v_{qs}^s$	$q^{s}$ -axis stator voltage
$v_{ds}^{s}$	d <sup>s</sup> -axis stator voltage q <sup>s</sup> -axis stator current
i <sub>qs</sub> :s	d <sup>s</sup> -axis stator current
$i^s_{ds}$ K <sub>s</sub>	Slip gain
$\mathbf{R}_{s}$ Q	Reactive power
Q*	Reactive power reference
$i_a^*$ , $i_b^*$ , and $i_c^*$	Stator current reference
i <sub>qs</sub> *	Stator quadrature-axis reference current
$i_{ds}^{qs}$ *	Stator direct-axis reference current
$ \Psi_r ^*$	Sotor flux reference input
$T_e^*$	Torque reference
$ \Psi_r _{est}$	Estimated rotor flux linkage