

PERFORMANCE ANALYSIS OF GAS TURBINE CYCLE
AT VARIABLE SPECIFIC HEAT

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**MECHANICAL ENGINEERING
(THERMAL ENGINEERING)**

**SUBMITTED BY
ANKIT MOHTA
04/ME/02**

**UNDER THE GUIDANCE OF
PROF. B.B. ARORA**

**DEPARTMENT OF MECHANICAL ENGINEERING
DELHI COLLEGE OF ENGINEERING
DELHI.**

Certificate's Declaration

I hereby declare that the work which is being present in the major project entitled "*Performance Analysis Of Gas Turbine Cycle At Variable Specific Heat*" in partial fulfillment for the award of Degree of **Master of Engineering** with specialization in "**Thermal Engineering**" submitted to **Delhi College of Engineering, University of Delhi**, is authentic record of my own work carried out under the supervision of **Prof. B.B. Arora**, Deptt. Of Mechanical Engineering, Delhi College of Engineering, University of Delhi. I have not submitted the matter in this dissertation for the award of any other Degree or Diploma or any other propose whatever.

Date

(Ankit Mohta)
Univ. Roll. No.-----
College Roll No, 04/ME/02

Certificate

This is to certify that the above statement made by the candidate is true to the best of my knowledge and belief.

(B. B. Arora)
Asst. Professor
Department of Mechanical Engineering
Delhi college of Engineering, Delhi.

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M.E. (Thermal engineering)

04/ ME (Thermal) / 2002

Delhi College of Engineering

ABSTRACT

The most important thermodynamic property used in heat release calculations is the specific heat ratio. The functions proposed in the literature for the specific heat ratio is temperature dependent. The various models of temperature dependant specific heat ratio is discussed in the literature and with a study of these functions it is a very clear to consider specific heat is a linear function in terms of temperature to a certain limits of temperature.

The thermodynamic performance of gas turbine cycle with temperature dependant variable specific heats of working fluid is studied and temperature dependent specific heat ratio functions were derived. The specific heats are a function of temperature and thus make a difference.

As the specific heats of a working fluid is always a function of temperature, it is necessary to consider this aspect in the practical gas turbine cycles. The thermodynamic performance of Gas turbine cycle with variable specific heats of working fluid with temperature is analyzed. The relations between the specific work ratio and the pressure ratio, between the thermal efficiency and the pressure ratio, as well as the optimal relation between specific work ratio and the efficiency of the cycle, are derived by detailed numerical examples. Also the cycle is analyzed with the intercooler alone, reheat alone and both with intercooler and reheat. The results show that the effects of variable specific heats of working fluid on the cycle performance are obvious, and they should be considered in practical cycle analysis. In the analysis a comparison between a constant and variable specific heat has been also made. The results obtained in this project may provide guidance for the design of practical gas turbines.

Further a computer program has been generated to analyze the gas turbine cycles at variable specific heats as to make the calculation easier as well as faster. With this , any number of intercooler and reheat cycles can be analyze.

GLOSSARY

T₁	- Compressor Inlet Temperature
T₂	. Compressor Exit Temperature
T₃	. Turbine Inlet Temperature (TIT)
T₄	. Turbine Exit Temperature
N₁	. Number of Inter-Cooling
N₂	. Number of Reheating
eth	-Thermal Efficiency of the cycle
ecc	- Combustion Efficiency of the cycle
ec	-Compressor Efficiency
et	-Turbine Efficiency
W_c	-Total Compressor Work Input
W_{ci}	-Compressor Work Input for i th stage
W_t	-Total Turbine Work Output
W_{ti}	-Turbine Work Output for i th stage
W_n	-Net Work Output
M_a	-Mass of air
a	-Constant term of specific heat at constant pressure [$C_p = a+k_1T$]
b	-Constant term of specific heat at constant volume [$C_v = b+k_1T$]
k₁	-Constant of variable term of specific heat
γ	-Isentropic Index
W_s	-Ratio of $W_n / C_p T_1$

Q -Heat Input

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CHAPTER-1

INTRODUCTION AND LITERATURE REVIEW

1.1 INTRODUCTION

In any gas turbine cycle we had always some assumptions in ideal cycle analysis

The assumption of ideal gas turbine cycle may be taken as the following:

1. The change of kinetic energy of the working fluid between inlet and outlet of each component is negligible.
2. Compression and expansion are reversible and adiabatic, i.e. isentropic.
3. There are no pressure losses in the inlet ducting, combustion chambers, heat exchangers, intercoolers, exhaust ducting and ducts connecting the components.
4. The mass flow of gas is constant throughout the cycle.
- 5. Working fluid has the same composition throughout the cycle and is a perfect gas with constant specific heats.**

So these assumption make a considerable difference in practical cycles. In this project , effect of variable specific heats with temperature has been analyzed.

1.2 EFFECT OF VARIABLE SPECIFIC HEAT

The specific heat of air is independent of pressure within the operating limit of gas turbine. However, it varies considerably with temperature. At 300 K the constant pressure specific heat of air is 1.005 kJ /kg K but at 1000K, it is 1.140 kJ/kg K- an increase of about 13.4%.

Further, the internal combustion of fuel causes the expanding exhaust gas which contains products of combustion, principally CO₂ and H₂O vapour, both having higher value of specific heat than that of pure air. At 1000 K, a typical value of Cp for gases after combustion is 1.147. In ideal cycle calculations the specific heat has been taken to be constant throughout the cycle, with a value of 1.005 kJ /kg K.

Thus, this assumption would seem to introduce considerable error, because the difference between the cold air and hot gas values given above is about 15%. Actually the

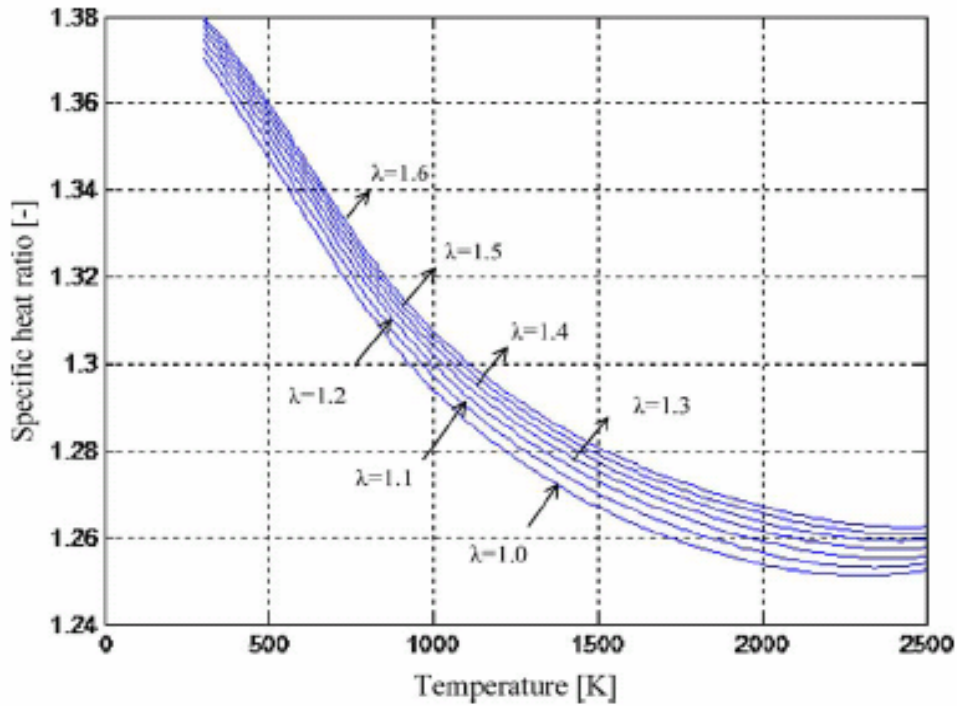
specific heat for air and gases, changes continuously during compression and expansion. For precise calculation, an integration process is required. Keenan and Kaye* have provided tables of air and gas properties at various air-fuel ratios in their 'Gas Tables' which can be used for precise calculations.

1.3 VARIATION OF SPECIFIC HEATS WITH TEMPERATURE

The most important thermodynamic property used in heat release calculations is the specific heat ratio. The functions proposed in the literature for the specific heat ratio is temperature dependent.

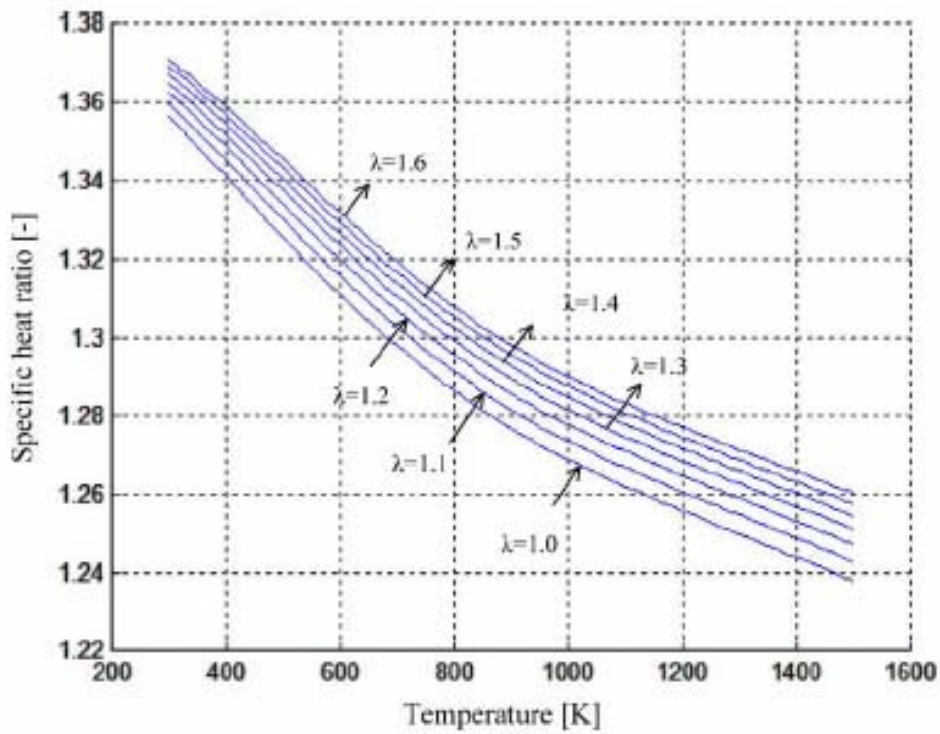
M.A. Ceviz *, I. Kaymaz Faculty of Engineering, University of Ataturk, Erzurum 25240, Turkey has published a paper on 19 February 2005 entitled as '**Temperature and air-fuel ratio dependent specific heat ratio functions for lean burned and unburned mixture**' in which he explained the dependency of the specific heat on temperature. He explained that the specific heats are dependent on charge temperature and composition and, as such, will vary during the engine cycle and with operating conditions. The use of a temperature dependent specific heat ratio function greatly reduces the potential errors in calculated the heat release.

Figs. 1 and 2 show the specific heat ratio against the charge temperature based on the results of the equilibrium combustion model for burned and unburned mixtures at various air-fuel ratios in a gasoline engine. It can be seen from these figures that the specific heat ratio decreases as the temperature increases, whereas it increases as the air-fuel ratio increases. These curves reveal that the relationship between specific heat ratio and temperature is almost linear and the variation with lambda is significant.



Variation of specific heat ratio with temperature and air-fuel ratio for burned mixture.

FIGURE1



Variation of specific heat ratio with temperature and air-fuel ratio for unburned mixture.

FIGURE2

1. Function of Gatowski et al. :

$$\gamma = \gamma_0 - K_1(T - T_{ref}) = 1000$$

where γ_0 is a reference value (1.38), K_1 is a constant (0.08) and T_{ref} is a reference temperature (300 K).

2. Function of Brunt et al. [2]:

$$\gamma = 1.338 - 6.0 \cdot 10^{-5}T + 1.0 \cdot 10^{-8}T^2$$

where T is temperature in K

3. Function of Egnell [4]:

$$\gamma = \gamma_0 - k_1 \exp(-k_2/T)$$

where γ_0 is a reference value (1.38), k_1 and k_2 are constants (0.2- 900) and T_{ref} is a reference temperature (300 K).

4. Derived functions of burned and unburned mixtures:

The specific heat ratios for the unburned and burned mixtures were computed using the equilibrium combustion model. The air–fuel ratio was increased from 1.0 to 1.6 in steps of 0.1, and the ranges of temperature were 300–1500 K and 300–2500 K for the unburned and burned mixtures, respectively. The data of the specific heat ratio was used to derive functions for the unburned and burned mixtures using a least squares approach and choosing the parameters as temperature (T in K) and air–fuel ratio (k). The functions of the specific heat ratio for the unburned and burned mixtures in T and k can be written as:

$$\gamma_u = a_1 + a_2T + a_3T^2 + a_4T^3 + a_5T^4 + a_6T^5 + \frac{a_7}{\lambda}$$

$$\gamma_b = b_1 + b_2T + \frac{b_3}{\lambda} + b_4T^2 + \frac{b_5}{\lambda^2} + \frac{b_6T}{\lambda} + b_7T^3 + \frac{b_8}{\lambda^3} + \frac{b_9T}{\lambda^2} + \frac{b_{10}T^2}{\lambda}$$

With an overall study of the variable specific heats are temperature dependent as with almost linear relationship in some limit of temperature

1.4 THEORY OF DIFFERENT GAS TURBINE CYCLES

1.4.1 Carnot cycle

In this cycle there are two isentropic and two isothermal processes. Compression and expansion are the isentropic process and heat addition and heat rejection are the isothermal processes.

The process of Carnot cycle would have to be non-flow making the cycle totally unsuited for a gas turbine power plant. Furthermore, slow speed of operation accompanies the slow rate of heat transfer. Metallurgical and lubrication complications of great magnitude are involved. Thus it must be concluded that the Carnot cycle can be useful only as a standard of comparison for the gas turbine.

1.4.2 Stirling cycle with regenerator.

Stirling patented and designed a regenerator, an apparatus for storing and restoring heat to gas of an engine cycle. This cycle consisted of adding heat to a gas during an expansion process in such a way that the temperature remained constant at T_1 . This gas then passed at constant volume through the regenerator, which absorbed heat until the temperature was reduced to lower value T_2 . The air was, then, isothermally compressed at T_2 through the same compression ratio as occurred during the expansion by being in contact with refrigerator or heat sink at T_2 . This is followed by passing the air back through the regenerator at constant volume, picking up the heat deposited in it on the first passage so that the temperature increases from T_2 to T_1 .

Stirling cycle reciprocating engines have been built in past, but with very poor results from a thermal efficiency standpoint. The non-flow processes in the Stirling cycle makes it totally unsuited for gas-turbine plant.

1.4.3 Ericsson cycle

Another air cycle of some interest in the general understanding of the fundamentals of the gas turbine. It was patented by Ericsson in about 1830. In this cycle air is heated from temperature T_2 to temperature T_1 at constant pressure p_1 by passing through the regenerator. It enters into working cylinder where an isothermal expansion occurs at temperature T_1 by addition of heat to the cylinder. The air then discharge back through the regenerator at constant pressure p_2 to a compressor cylinder giving up heat to the regenerator sufficient to change the temperature from T_1 to T_2 in the process. The compressor now compresses the air isothermally at temperature T_2 , rejecting heat in the operation, to the original pressure p_1 .

It appear that the Ericsson cycle with regeneration provides an excellent opportunity to improve the efficiency of a gas turbine power plant. But in fact, it will be found that the improvement of gas turbine efficiencies centers on the application of these modification within the bounds of realizing a plant of reasonable first cost and size, which is free from undue complexity.

1.4.4 The Joule Air Cycle.

In 1851 Dr. Joule proposed an air engine consisting of a compression cylinder and an expansion cylinder connected by two large chambers one of these chambers was to be maintained at a high temperature T_1 while the other was to be maintained at a lower temperature T_2 . These chambers were large in comparison with the cylinders volumes and since the cylinders discharge are drew from the chambers, the resulting pressure fluctuations were small.

The operation consisted of the working cylinder drawing a charge of air at a constant pressure p_1 from the hot chambers T_1 , expanding it isentropically to pressure p_2 and then exhausting it to the cold chamber at constant pressure p_2 , while it was cooled to temperature T_2 . The compressor cylinder takes in air at p_2 and T_2 from cold chamber and isentropically compresses it to pressure p_1 and then delivers it at constant pressure p_1 into the hot chamber where its temperature is raised to T_1 . This cycle is most suited to the gas turbine power plant.

1.5 LITERATURE REVIEW

Yanlin Ge (Postgraduate School, Naval University of Engineering, Wuhan 430033, PR China) published a paper **“Performance of an Atkinson cycle with heat transfer, friction and variable specific-heats of the working fluid”** on 23 December **2005**

In this paper he has discussed the performance of an air standard Atkinson cycle with heat-transfer loss, friction-like term loss and variable specific-heats of the working fluid is analyzed . The relations between the power output and the compression ratio, between the thermal efficiency and the compression ratio, as well as the optimal relation between the power output and the efficiency of the cycle are derived by detailed numerical examples. Moreover, the effects of variable specific heats of the working fluid and the friction-like term loss on the irreversible cycle performance are analyzed. The results show that the effects of variable specific-heats of working fluid and friction-like term loss on the irreversible cycle performance should be considered in cycle analysis.

Lingen Chen a, Chih Wu b (a: Postgraduate School, Naval University of Engineering, Wuhan 430033, PR China , b: Mechanical Engineering Department, US Naval Academy, Anapolis, MD 21402, USA) published a paper **“Effects of heat transfer, friction and variable specific heats of working fluid on performance of an irreversible dual cycle”** on 15 February **2006**

In this paper they analyze The thermodynamic performance of an air standard dual cycle with heat transfer loss, friction like term loss and variable specific heats of working fluid is analyzed. According to their analysis, it can be found that the effects of the variable specific heats of the working fluid and the friction loss on the cycle performance are obvious, and they should be considered in practical cycle analysis in order to make the cycle model be closer to practice. the performance characteristics of the cycle were obtained by detailed numerical examples. Their results show that the effects of variable specific heats of the working fluid and the friction loss on the cycle performance are obvious, and they should be considered in practical cycle analysis. The results obtained in this paper may provide guidance for the design of practical engines.

A. Al-Sarkhi a,*, **J.O. Jaber a**, **M. Abu-Qudais a**, **S.D. Probert** (a :Department of Mechanical Engineering, Hashemite University, Zarqa 13115, Jordan , b : School of Engineering, Cranfield University, Bedford MK43 0AL, UK) published a paper “**Effects of friction and temperature-dependent specific-heat of the working fluid on the performance of a Diesel-engine**” on 7 March **2005**

In their paper Using finite-time thermodynamics, the relations between the power output, thermal efficiency and compression ratio have been derived. The effect of the specific heat of the working fluid, being temperature dependent, on the irreversible cycle performance, is significant An air-standard Diesel-cycle model, assuming a temperature-dependent specific heat of the working fluid, and heat resistance and frictional irreversible losses, has been investigated numerically. The performance characteristics of the cycle were obtained by numerical examples. The results show that there are significant effects of the temperature dependence of the specific heat of the working fluid on the performance of the cycle, and this should be considered in practical-cycle analysis. The results obtained from this research are compatible with those in the open literature. They also suggested that Future studies should discuss the possible effects of fuel additives in order to achieve a less temperature-dependent specific heat of the working fluid.

M.A. Ceviz *, **_I. Kaymaz** (Department of Mechanical Engineering, Faculty of Engineering, University of Ataturk, Erzurum 25240, Turkey) published a paper “**Temperature and air–fuel ratio dependent specific heat ratio functions for lean burned and unburned mixture**” on 19 February **2005**

The functions In this study, for burned and unburned mixtures, temperature and air–fuel ratio dependent specific heat ratio functions were derived by using the equilibrium combustion model and the variations of gases thermodynamic properties with mean temperature. Then, the global specific heat ratio was calculated by using the variation of the mass fraction burned. The results show that implementation of a $c = c(T,k)$ function reduces notably the error deriving from temperature only dependent specific heat ratio under lean operation of engine. The experiments performed at four different air–fuel ratios show that as the air–fuel ratio increases, the results of the equilibrium combustion

model and the c function are in reasonable agreement. Additionally, the derived functions for burned and unburned mixtures have a great simplicity in the mathematical formulation and only need the global air–fuel ratio, temperature and mass fraction burned, which can be determined from experimental pressure measurements.

Chih Wub ,Yanlin Ge (Faculty 306, Naval University of Engineering, Wuhan 430033, PR China) published a paper “**Thermodynamic simulation of performance of an Otto cycle with heat transfer and variable specific heats of working fluid**” on 4 October 2004.

In this paper the performance of an air-standard Otto cycle with heat transfer loss and variable specific heats of working fluid is analyzed by using finite-time thermodynamics. The relations between the power output and the compression ratio, between the thermal efficiency and the compression ratio, as well as the optimal relation between power output and the efficiency of the cycle are derived by detailed numerical examples. Moreover, the effects of heat transfer loss and variable specific heats of working fluid on the cycle performance are analyzed. The results show that the effects of heat transfer loss and variable specific heats of working fluid on the cycle performance are obvious, and they should be considered in practice cycle analysis.

Cai Ruixian *, **Jiang Lixia** (Institute of Engineering Thermophysics, Chinese Academy of Sciences) published a paper “**Analysis of the recuperative gas turbine cycle with a recuperator located between turbines**” on 15 April 2005

A recuperative gas turbine cycle with a recuperator located between a high-pressure turbine and a low-pressure turbine (alternative recuperative cycle) is analyzed and compared with the simple cycle and conventional recuperative cycle in detail. The result based on the ideal cycle analysis shows that the alternative recuperative cycle can achieve the highest efficiency among the abovementioned three cycles, but its specific work is much lower. When all irreversible factors are taken into account, however, the alternative recuperative cycle does not exhibit the highest efficiency.

CHAPTER – 2

ANALYSIS OF GAS TURBINE CYCLE

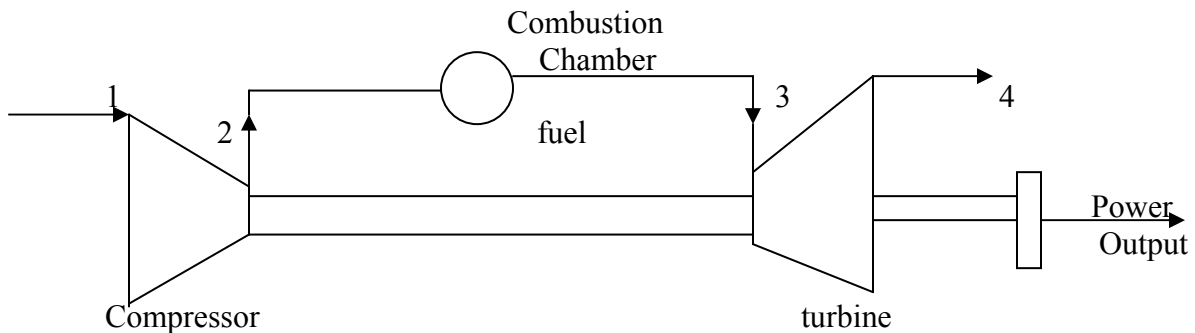
2.1 SIMPLE GAS TURBINE THEROY

In a simple gas turbine , air is first of all compresses in the compressor then it is sent in the combustion chamber for heat addition. Further this air expands in the turbine where the work output gets and further the heat rejection takes place and complete the cycle.

From the thermodynamic analysis the relevant steady flows energy equation

$$W_s = \Delta h = h_2 - h_1$$

Where W_s is the work transfer per unit mass flow, and h stands for enthalpies.



Block Diagram of a simple gas turbine

Compressor work [W_C]

$$W_{12} = (h_2 - h_1) = C_p (T_2 - T_1)$$

Heat addition [Q]

$$Q_{23} = (h_3 - h_2) = C_p (T_3 - T_2)$$

Turbine work [W_T]

$$W_{34} = (h_3 - h_4) = C_p (T_3 - T_4)$$

Network output [W_N]

$$\begin{aligned} &= W_T - W_C \\ &= C_p (T_3 - T_4) - C_p (T_2 - T_1) \end{aligned}$$

Efficiency

$$\eta = \frac{\text{Net work output}}{\text{Heat input}} = \frac{W_N}{Q}$$

In the ideal cycles, the assumption compression and expansion are reversible and adiabatic, i.e. isentropic. During compression process a considerable amount of energy supplied to the compressor is wasted in churning up the working fluid. The energy does not contribute to the pressure rise but is converted into heat by friction.

The compressor efficiency may be defined as the ratio of the work required for isentropic compression to the actual work input.

$$\eta_c = \frac{\text{Isentropic compressor work input}}{\text{Actual compressor work input}}$$

The expansion process of the gas turbine cycle, a similar effect of wasteful heating of the working fluid will occur, as in the case of compressor.

The efficiency of the turbine can be written as

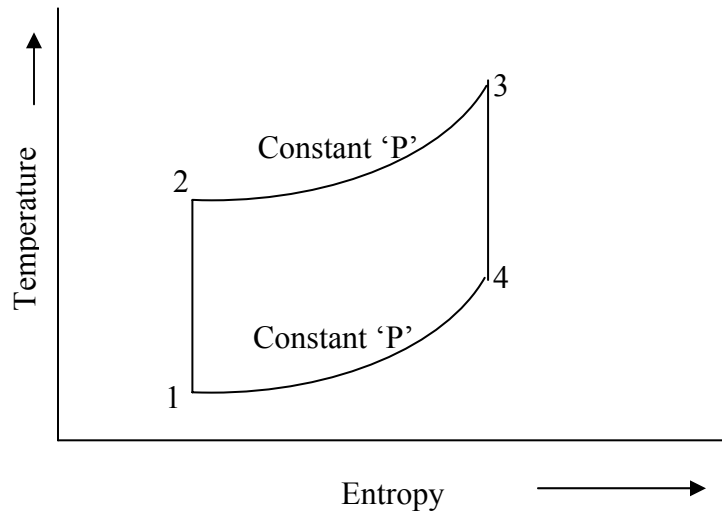
$$\begin{aligned} \eta_T &= \frac{\text{Actual turbine work output}}{\text{Isentropic turbine work output}} \\ &= \frac{h_{03} - h_{04}}{h_{03} - h_{04'}} = \frac{(T_{03} - T_{04})}{(T_{03} - T_{04'})} \end{aligned}$$

For the constant value of C_p

Also during heat transfer all the heat, containing the fuel, is never being transferred to the air. So it is always considered the combustion efficiency η_{cc} , which should be used in the calculation of heat addition.

2.2 EFFECTS OF TEMPERATURE-DEPENDENT SPECIFIC-HEAT OF THE WORKING FLUID ON THE PERFORMANCE OF A GAS TURBINE CYCLE

The compression process $1 \rightarrow 2$ is isentropic, the heat addition $2 \rightarrow 3$ an isobaric process, the expansion $3 \rightarrow 4$ an isentropic process, and the heat rejection $4 \rightarrow 1$ an isochoric process.



In a real cycle, the specific heat of the working fluid varies with temperature and this will have a significant influence on the performance of the cycle. Assuming that the specific heat of the working fluid is a function of temperature alone, over the temperature range generally encountered for gases in heat engines (i.e., 300–2200 K), the specific-heat curve is nearly linear, i.e., to a close approximation:

$$C_{pm} = a + k_1 T \quad (4)$$

$$C_{vm} = b + k_1 T \quad (5)$$

where a , b and k_1 are constants, C_{pm} and C_{vm} are the mole specific heats with respect to constant pressure and volume, respectively. Accordingly, the constant, R , of the working fluid is

$$R = C_{pm} - C_{vm} = a - b \quad (6)$$

The heat added to the working fluid, during process $2 \rightarrow 3$, is

$$\begin{aligned}
Q_{in} &= M \int_{T_2}^{T_3} C_p dT = M \int_{T_2}^{T_3} (a + k_1 T) dT \\
&= M[a(T_3 - T_2) + 0.5k_1(T_3^2 - T_2^2)].
\end{aligned}$$

The heat rejected by the working fluid, during process 4 \rightarrow 1, is

$$\begin{aligned}
Q_{out} &= M \int_{T_1}^{T_4} C_{pm} dT = M \int_{T_1}^{T_4} (a_p + k_1 T) dT \\
&= M[a_p(T_4 - T_1) + 0.5K_1(T_4^2 - T_1^2)]
\end{aligned}$$

The work output of the cycle is

$$W = Q_{in} - Q_{out}$$

Since C_{pm} and C_{vm} are dependent on temperature, the adiabatic exponent 'k'

$k = C_{pm} / C_{vm}$ will vary with temperature as well. Therefore, the equation often used in reversible adiabatic- processes with constant k cannot be used in reversible adiabatic- processes with variable k. However, a suitable engineering approximation for a reversible adiabatic-process with variable k can be made, i.e., this process can be broken up into infinitesimally-small processes, and for each of these processes, the adiabatic exponent k can be regarded as a constant. For example, any reversible adiabatic-process between states i and j can be regarded as consisting of numerous infinitesimally-small processes with constant k. For any of these processes, when small changes in temperature dT and in volume dV of the working fluid take place, the equation for a reversible adiabatic process with variable k can be written as follows:

$$T(P)^{(1-\gamma)/\gamma} = A$$

$$T(P)^{(1-\gamma)/\gamma} = (T+dT)(P+dP)^{(1-\gamma)/\gamma}$$

$$\{T/(T+dT)\} = \{(P+dP)/P\}^{(1-\gamma)/\gamma}$$

$$(1+dT/T)^{-1} = (1+dP/P)^{(1-\gamma)/\gamma}$$

$$-\ln(1+dT/T) = \{(1-\gamma)/\gamma\} \ln(1+dP/P)$$

With the expansion of the 'ln' series and leaving the higher degree terms, we get

$$-(dT/T) = (1-\gamma)/\gamma(dP/P)$$

As 'γ' is expressed as the ratio of c_p and c_v ,

Thus we get,

$$(1-\gamma)/\gamma = \{-R/(a+k_1 T)\}$$

$$-dT/T = \{-R / (a+k_1T)\} (dP/P)$$

$$\{(a+ k_1T)/T\} dT = R (dP/P)$$

$$[+a \ln T + K_1 T = R \ln P$$

$$\boxed{a_v \ln T + k_1 T = R \ln P}$$

This is the equation used for the process 1 → 2 and 3 → 4.

$$a_v \ln T_j + K_1 T_j = R \ln P$$

$$a_v \ln (T_j/T_i) + K_1 (T_j - T_i) = R \ln P_j/P_i$$

$$a_v \ln (T_j/T_i) + K_1 (T_j - T_i) = R \ln P_j/P_i$$

$$a_v \ln T_j + K_1 T_j = K_1 T_i + a_v \ln T_i + R \ln P_j/P_i$$

$$\text{Say } B = R \ln P_j/P_i$$

$$a_v \ln T_j + K_1 T_j = B + K_1 T_i + a_v \ln T_i$$

$$\ln T_j + K_1 T_j / a_v = \{(B + K_1 T_i + a_v \ln T_i) / a_v\}$$

$$\text{Say } \{(B + K_1 T_i + a_v \ln T_i) / a_v\} = X$$

$$\text{Say } K_1 / a_v = Y$$

$$\ln T_j + Y T_j = X$$

$$\text{Or } \ln T_j - X + Y T_j = 0$$

Or

$$\boxed{f(t) = \ln T_j - X + Y T_j}$$

With the above equations, temperatures of the cycle have to be calculated.

CHAPTER –3

RESULTS AND DISCUSSION

3.1 RESULTS AND DISCUSSION-1

A computer program has been generated for the analysis of: -

1. Thermal efficiency of gas turbine cycle
2. Total compressor work input required of the gas turbine cycle
3. Total turbine work output of the gas turbine cycle
4. Net work output of the gas turbine cycle
5. Ratio of $W_n / C_p T_1$ of gas turbine

The following variables have been varied: -

1. The value of constant term of the specific heat of the working fluid (a and b). The value of 'a' varies from 28.182 to 32.182.
2. The constant of variable term of the variable specific heats (k_1). The value of ' k_1 ' varies from 0.004 to 0.008.
3. Number of intercoolers used in the cycle (N_1).
4. Number of reheat in the cycle (N_2).

Assumptions: -

1. Mass of the working fluid =1 kmol
2. Efficiency of combustion $\eta_{cc}=0.95$
3. Efficiency of the compressor $\eta_c =0.95$
4. Efficiency of the turbine $\eta_t = 0.95$

5. Ambient temperature $T_1 = 300 \text{ k}$
6. Temperature after inter cooler = 300k
7. Temperature after reheat = Temperature at the turbine inlet of first stage (T_3)
8. Compression pressure ratio after intercooler = Compression pressure ratio before intercooler .
9. Expansion pressure ratio after reheat = Expansion pressure ratio before reheat

The results starts from Next page:-

**** (for program code , refer to annexure -1)**

3.2 RESULTS OH COMPUTER PROGRAM FOR THE ANALYSIS OF GAS TURBINE

3.2.1 For simple gas turbine

TIT	a	k ₁	b	r _p	W _c	W _t	eth	W _n	W _s
1000	28.182	0.004	19.868	2	2009.993	5009.415	0.145846	2999.423	0.340279
1000	28.182	0.004	19.868	4	4451.196	9182.17	0.26289	4730.974	0.53672
1000	28.182	0.004	19.868	6	6112.997	11288.42	0.318551	5175.418	0.587142
1000	28.182	0.004	19.868	8	7409.877	12647.04	0.351922	5237.162	0.594146
1000	28.182	0.004	19.868	10	8488.554	13630.12	0.374036	5141.562	0.583301
1000	28.182	0.004	19.868	12	9419.856	14390.01	0.389333	4970.159	0.563855
1000	28.182	0.004	19.868	14	10243.95	15003.49	0.400016	4759.539	0.539961
1000	28.182	0.004	19.868	16	10988.13	15514.26	0.407208	4526.126	0.513481
1000	28.182	0.004	19.868	18	11665.85	15949.42	0.411817	4283.569	0.485963
1000	28.182	0.004	19.868	20	12290.58	16326.84	0.414229	4036.256	0.457906
1000	28.182	0.004	19.868	22	12871.17	16658.89	0.414735	3787.717	0.429709
1000	28.182	0.004	19.868	24	13414.33	16954.45	0.413511	3540.123	0.40162
1000	28.182	0.005	19.868	2	2007.816	5022.097	0.143217	3014.282	0.338508
1000	28.182	0.005	19.868	4	4440.66	9225.715	0.258847	4785.055	0.537369
1000	28.182	0.005	19.868	6	6093.309	11355.01	0.314199	5261.699	0.590897
1000	28.182	0.005	19.868	8	7381.163	12731.23	0.347615	5350.07	0.600821
1000	28.182	0.005	19.868	10	8451.11	13728.42	0.369961	5277.308	0.59265
1000	28.182	0.005	19.868	12	9374.004	14500.03	0.385617	5126.026	0.57566
1000	28.182	0.005	19.868	14	10190	15123.48	0.39677	4933.482	0.554037
1000	28.182	0.005	19.868	16	10924.28	15642.92	0.404645	4718.64	0.52991
1000	28.182	0.005	19.868	18	11596.09	16085.73	0.409862	4489.638	0.504193
1000	28.182	0.005	19.868	20	12213.39	16469.98	0.413091	4256.585	0.478021
1000	28.182	0.005	19.868	22	12786.76	16808.19	0.414551	4021.426	0.451612
1000	28.182	0.005	19.868	24	13322.88	17109.34	0.41444	3786.463	0.425225
1000	28.182	0.006	19.868	2	2005.691	5034.139	0.140674	3028.448	0.336696
1000	28.182	0.006	19.868	4	4430.426	9267.377	0.254902	4836.951	0.537762
1000	28.182	0.006	19.868	6	6074.241	11418.97	0.309922	5344.732	0.594216
1000	28.182	0.006	19.868	8	7353.416	12812.33	0.343351	5458.911	0.60691
1000	28.182	0.006	19.868	10	8414.993	13823.29	0.365883	5408.298	0.601283
1000	28.182	0.006	19.868	12	9329.845	14606.38	0.381846	5276.531	0.586633
1000	28.182	0.006	19.868	14	10138.11	15239.62	0.393402	5101.512	0.567175
1000	28.182	0.006	19.868	16	10864.94	15767.58	0.40177	4902.637	0.545065
1000	28.182	0.006	19.868	18	11529.19	16217.92	0.407595	4688.723	0.521282
1000	28.182	0.006	19.868	20	12139.45	16608.9	0.411514	4469.45	0.496904
1000	28.182	0.006	19.868	22	12705.98	16953.19	0.41377	4247.212	0.472196
1000	28.182	0.006	19.868	24	13235.45	17259.88	0.414577	4024.432	0.447428
1000	28.182	0.007	19.868	2	2003.617	5045.586	0.138213	3041.968	0.334849

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	28.182	0.007	19.868	4	4420.478	9307.261	0.251053	4886.782	0.537919
1000	28.182	0.007	19.868	6	6055.761	11480.44	0.305722	5424.676	0.597129
1000	28.182	0.007	19.868	8	7326.583	12890.45	0.339134	5563.872	0.612451
1000	28.182	0.007	19.868	10	8380.125	13914.87	0.361816	5534.745	0.609245
1000	28.182	0.007	19.868	12	9287.273	14709.18	0.378038	5421.908	0.596824
1000	28.182	0.007	19.868	14	10088.15	15352.03	0.38994	5263.887	0.57943
1000	28.182	0.007	19.868	16	10807.87	15888.37	0.398733	5080.494	0.559242
1000	28.182	0.007	19.868	18	11463.33	16346.11	0.405155	4882.781	0.537479
1000	28.182	0.007	19.868	20	12068.52	16743.73	0.409581	4675.203	0.51463
1000	28.182	0.007	19.868	22	12628.56	17094.01	0.412509	4465.453	0.491541
1000	28.182	0.007	19.868	24	13151.73	17406.17	0.414082	4254.442	0.468314
1000	28.182	0.008	19.868	2	2001.591	5056.477	0.135831	3054.886	0.332972
1000	28.182	0.008	19.868	4	4410.805	9345.465	0.247298	4934.661	0.537861
1000	28.182	0.008	19.868	6	6037.84	11539.52	0.3016	5501.682	0.599665
1000	28.182	0.008	19.868	8	7300.614	12965.75	0.334969	5665.132	0.61748
1000	28.182	0.008	19.868	10	8346.437	14003.29	0.357767	5656.849	0.616577
1000	28.182	0.008	19.868	12	9246.198	14808.58	0.374208	5562.382	0.606281
1000	28.182	0.008	19.868	14	10040	15460.85	0.386408	5420.853	0.590854
1000	28.182	0.008	19.868	16	10752.93	16005.4	0.395566	5252.476	0.572502
1000	28.182	0.008	19.868	18	11401.85	16470.43	0.402418	5068.587	0.552459
1000	28.182	0.008	19.868	20	11998.66	16874.58	0.407444	4875.922	0.531459
1000	28.182	0.008	19.868	22	12554.28	17230.78	0.41086	4676.503	0.509723
1000	28.182	0.008	19.868	24	13071.46	17548.33	0.413078	4476.87	0.487964
1000	29.182	0.004	20.868	2	2003.364	5022.819	0.141695	3019.456	0.331277
1000	29.182	0.004	20.868	4	4421.283	9230.712	0.256307	4809.429	0.527662
1000	29.182	0.004	20.868	6	6059.402	11365.14	0.311369	5305.734	0.582114
1000	29.182	0.004	20.868	8	7334.036	12745.92	0.344744	5411.881	0.59376
1000	29.182	0.004	20.868	10	8391.957	13747.35	0.367193	5355.394	0.587562
1000	29.182	0.004	20.868	12	9303.828	14522.88	0.383055	5219.056	0.572604
1000	29.182	0.004	20.868	14	10109.64	15149.95	0.394496	5040.314	0.552993
1000	29.182	0.004	20.868	16	10834.44	15672.74	0.402734	4838.3	0.53083
1000	29.182	0.004	20.868	18	11497.38	16118.66	0.408392	4621.283	0.50702
1000	29.182	0.004	20.868	20	12106.34	16505.82	0.412137	4399.482	0.482685
1000	29.182	0.004	20.868	22	12671.82	16846.76	0.414199	4174.937	0.458049
1000	29.182	0.004	20.868	24	13200.47	17150.49	0.414784	3950.02	0.433373
1000	29.182	0.005	20.868	2	2001.339	5034.806	0.13921	3033.467	0.32956
1000	29.182	0.005	20.868	4	4411.542	9272.037	0.252447	4860.495	0.528051
1000	29.182	0.005	20.868	6	6041.26	11428.49	0.307174	5387.227	0.585275
1000	29.182	0.005	20.868	8	7307.64	12826.15	0.340544	5518.512	0.599538
1000	29.182	0.005	20.868	10	8357.597	13841.15	0.363154	5483.556	0.595741
1000	29.182	0.005	20.868	12	9261.813	14627.97	0.379288	5366.161	0.582987

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	29.182	0.005	20.868	14	10060.26	15264.68	0.391089	5204.416	0.565415
1000	29.182	0.005	20.868	16	10777.97	15795.85	0.399766	5017.875	0.545149
1000	29.182	0.005	20.868	18	11431.74	16249.17	0.40606	4817.433	0.523372
1000	29.182	0.005	20.868	20	12035.93	16642.95	0.41032	4607.019	0.500513
1000	29.182	0.005	20.868	22	12594.89	16989.87	0.413082	4394.979	0.477476
1000	29.182	0.005	20.868	24	13117.19	17299.04	0.414468	4181.853	0.454322
1000	29.182	0.006	20.868	2	1999.361	5046.203	0.136804	3046.841	0.327808
1000	29.182	0.006	20.868	4	4402.068	9311.612	0.24868	4909.544	0.528215
1000	29.182	0.006	20.868	6	6023.664	11489.38	0.303053	5465.717	0.588053
1000	29.182	0.006	20.868	8	7282.092	12903.48	0.336391	5621.386	0.604801
1000	29.182	0.006	20.868	10	8324.398	13931.73	0.359129	5607.332	0.603289
1000	29.182	0.006	20.868	12	9221.274	14729.6	0.375493	5508.329	0.592638
1000	29.182	0.006	20.868	14	10012.68	15375.76	0.387602	5363.081	0.57701
1000	29.182	0.006	20.868	16	10723.61	15915.16	0.396659	5191.556	0.558556
1000	29.182	0.006	20.868	18	11370.84	16375.78	0.403399	5004.932	0.538477
1000	29.182	0.006	20.868	20	11968.34	16776.08	0.408198	4807.743	0.517262
1000	29.182	0.006	20.868	22	12521.09	17128.9	0.411554	4607.802	0.49575
1000	29.182	0.006	20.868	24	13037.37	17443.45	0.413612	4406.074	0.474047
1000	29.182	0.007	20.868	2	1996.362	5057.05	0.134514	3060.687	0.326139
1000	29.182	0.007	20.868	4	4392.848	9349.532	0.245003	4956.684	0.528172
1000	29.182	0.007	20.868	6	6006.588	11547.94	0.299008	5541.35	0.590473
1000	29.182	0.007	20.868	8	7257.348	12978.02	0.332291	5720.674	0.609581
1000	29.182	0.007	20.868	10	8292.295	14019.21	0.355126	5726.912	0.610246
1000	29.182	0.007	20.868	12	9182.126	14827.9	0.371683	5645.769	0.601599
1000	29.182	0.007	20.868	14	9966.779	15483.32	0.384058	5516.541	0.587829
1000	29.182	0.007	20.868	16	10671.23	16030.82	0.393443	5359.591	0.571105
1000	29.182	0.007	20.868	18	11312.22	16498.6	0.400568	5186.377	0.552648
1000	29.182	0.007	20.868	20	11901.59	16905.33	0.405911	5003.737	0.533186
1000	29.182	0.007	20.868	22	12450.22	17263.96	0.409691	4813.734	0.51294
1000	29.182	0.007	20.868	24	12960.77	17583.81	0.412321	4623.036	0.492619
1000	29.182	0.008	20.868	2	1994.535	5067.384	0.132253	3072.849	0.324325
1000	29.182	0.008	20.868	4	4383.872	9385.889	0.241416	5002.017	0.52794
1000	29.182	0.008	20.868	6	5990.006	11604.27	0.29504	5614.262	0.592559
1000	29.182	0.008	20.868	8	7233.366	13049.9	0.328246	5816.537	0.613908
1000	29.182	0.008	20.868	10	8261.229	14103.71	0.351151	5842.479	0.616647
1000	29.182	0.008	20.868	12	9144.291	14922.97	0.367869	5778.684	0.609913
1000	29.182	0.008	20.868	14	9922.467	15587.48	0.380473	5665.015	0.597916
1000	29.182	0.008	20.868	16	10620.7	16142.92	0.390141	5522.218	0.582844
1000	29.182	0.008	20.868	18	11255.72	16617.75	0.3976	5362.024	0.565937
1000	29.182	0.008	20.868	20	11839.34	17030.8	0.403325	5191.462	0.547935
1000	29.182	0.008	20.868	22	12380.22	17395.16	0.407642	5014.937	0.529303
1000	29.182	0.008	20.868	24	12887.18	17720.24	0.410673	4833.067	0.510108

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	30.182	0.004	21.868	2	1997.18	5035.469	0.137773	3038.289	0.322721
1000	30.182	0.004	21.868	4	4393.478	9276.64	0.250028	4883.162	0.51868
1000	30.182	0.004	21.868	6	6009.68	11436.01	0.304351	5426.328	0.576374
1000	30.182	0.004	21.868	8	7263.772	12839.76	0.337752	5575.983	0.59227
1000	30.182	0.004	21.868	10	8302.555	13858.7	0.360423	5556.142	0.590162
1000	30.182	0.004	21.868	12	9196.528	14649.16	0.376704	5452.634	0.579168
1000	30.182	0.004	21.868	14	9985.513	15289.23	0.388719	5303.722	0.563351
1000	30.182	0.004	21.868	16	10694.41	15823.53	0.397671	5129.114	0.544804
1000	30.182	0.004	21.868	18	11339.93	16279.76	0.404295	4939.831	0.524699
1000	30.182	0.004	21.868	20	11936.37	16676.27	0.408945	4739.896	0.503462
1000	30.182	0.004	21.868	22	12488	17025.74	0.412151	4537.743	0.48199
1000	30.182	0.004	21.868	24	13003.34	17337.33	0.414045	4333.982	0.460347
1000	30.182	0.005	21.868	2	1994.19	5046.816	0.135462	3052.626	0.321174
1000	30.182	0.005	21.868	4	4384.446	9315.911	0.24634	4931.465	0.51885
1000	30.182	0.005	21.868	6	5992.912	11496.3	0.300308	5503.385	0.579023
1000	30.182	0.005	21.868	8	7239.43	12916.3	0.333666	5676.873	0.597276
1000	30.182	0.005	21.868	10	8270.923	13948.3	0.356443	5677.377	0.597329
1000	30.182	0.005	21.868	12	9157.901	14749.65	0.372927	5591.748	0.58832
1000	30.182	0.005	21.868	14	9940.169	15399.03	0.38522	5458.857	0.574338
1000	30.182	0.005	21.868	16	10642.61	15941.43	0.394511	5298.82	0.557501
1000	30.182	0.005	21.868	18	11281.89	16404.83	0.401534	5122.938	0.538996
1000	30.182	0.005	21.868	20	11871.93	16807.76	0.406665	4935.83	0.51931
1000	30.182	0.005	21.868	22	12417.63	17163.03	0.410398	4745.402	0.499274
1000	30.182	0.005	21.868	24	12927.22	17479.9	0.412886	4552.684	0.478998
1000	30.182	0.006	21.868	2	1992.408	5057.619	0.133179	3065.211	0.319473
1000	30.182	0.006	21.868	4	4375.651	9353.552	0.24274	4977.901	0.518823
1000	30.182	0.006	21.868	6	5976.628	11554.3	0.29634	5577.668	0.581334
1000	30.182	0.006	21.868	8	7215.836	12990.12	0.329631	5774.284	0.601826
1000	30.182	0.006	21.868	10	8240.311	14034.87	0.352487	5794.555	0.603939
1000	30.182	0.006	21.868	12	9120.568	14846.87	0.369142	5726.299	0.596825
1000	30.182	0.006	21.868	14	9896.394	15505.37	0.381672	5608.978	0.584597
1000	30.182	0.006	21.868	16	10592.64	16055.74	0.391258	5463.095	0.569393
1000	30.182	0.006	21.868	18	11225.97	16526.2	0.398626	5300.229	0.552418
1000	30.182	0.006	21.868	20	11808.14	16935.44	0.404252	5127.308	0.534395
1000	30.182	0.006	21.868	22	12349.99	17296.44	0.408357	4946.453	0.515545
1000	30.182	0.006	21.868	24	12854.1	17618.53	0.41135	4764.431	0.496574
1000	30.182	0.007	21.868	2	1990.662	5067.912	0.130966	3077.251	0.317747
1000	30.182	0.007	21.868	4	4367.083	9389.652	0.239226	5022.569	0.518614
1000	30.182	0.007	21.868	6	5960.804	11610.11	0.292446	5649.308	0.583329
1000	30.182	0.007	21.868	8	7192.952	13061.32	0.32565	5868.37	0.605949
1000	30.182	0.007	21.868	10	8210.665	14118.51	0.348562	5907.847	0.610025

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	30.182	0.007	21.868	12	9084.46	14940.94	0.365358	5856.479	0.604721
1000	30.182	0.007	21.868	14	9854.099	15608.39	0.378093	5754.289	0.594169
1000	30.182	0.007	21.868	16	10544.41	16166.58	0.387933	5622.163	0.580526
1000	30.182	0.007	21.868	18	11172.03	16643.97	0.395601	5471.941	0.565015
1000	30.182	0.007	21.868	20	11748.69	17059.44	0.40157	5310.748	0.54837
1000	30.182	0.007	21.868	22	12283.02	17426.08	0.406165	5143.061	0.531056
1000	30.182	0.007	21.868	24	12783.79	17753.32	0.409507	4969.526	0.513137
1000	30.182	0.008	21.868	2	1988.951	5077.731	0.128821	3088.78	0.316001
1000	30.182	0.008	21.868	4	4358.732	9424.293	0.235796	5065.561	0.518237
1000	30.182	0.008	21.868	6	5945.42	11663.85	0.288626	5718.431	0.58503
1000	30.182	0.008	21.868	8	7170.743	13130.02	0.321727	5959.279	0.60967
1000	30.182	0.008	21.868	10	8181.936	14199.36	0.344672	6017.42	0.615618
1000	30.182	0.008	21.868	12	9049.509	15031.98	0.361584	5982.468	0.612042
1000	30.182	0.008	21.868	14	9813.203	15708.19	0.374493	5894.99	0.603093
1000	30.182	0.008	21.868	16	10497.82	16274.05	0.384554	5776.236	0.590943
1000	30.182	0.008	21.868	18	11119.96	16758.27	0.392483	5638.303	0.576832
1000	30.182	0.008	21.868	20	11691.36	17179.86	0.398751	5488.505	0.561507
1000	30.182	0.008	21.868	22	12220.59	17552.05	0.403679	5331.46	0.54544
1000	30.182	0.008	21.868	24	12714.18	17884.37	0.407499	5170.186	0.528941
1000	31.182	0.004	22.868	2	1990.327	5047.426	0.134101	3057.1	0.314691
1000	31.182	0.004	22.868	4	4367.566	9320.159	0.244035	4952.594	0.509809
1000	31.182	0.004	22.868	6	5963.431	11504.76	0.297685	5541.326	0.570412
1000	31.182	0.004	22.868	8	7198.501	12928.94	0.330959	5730.435	0.589879
1000	31.182	0.004	22.868	10	8219.587	13964.59	0.353761	5745.006	0.591379
1000	31.182	0.004	22.868	12	9097.027	14769.33	0.370347	5672.306	0.583895
1000	31.182	0.004	22.868	14	9870.483	15421.85	0.3828	5551.371	0.571446
1000	31.182	0.004	22.868	16	10564.72	15967.17	0.3923	5402.456	0.556117
1000	31.182	0.004	22.868	18	11196.33	16433.3	0.399574	5236.977	0.539083
1000	31.182	0.004	22.868	20	11779.13	16838.78	0.405001	5059.65	0.520829
1000	31.182	0.004	22.868	22	12318	17196.45	0.409071	4878.45	0.502177
1000	31.182	0.004	22.868	24	12821.11	17515.59	0.411937	4694.474	0.483239
1000	31.182	0.005	22.868	2	1988.623	5058.184	0.131867	3069.562	0.313074
1000	31.182	0.005	22.868	4	4359.169	9357.526	0.24051	4998.358	0.509797
1000	31.182	0.005	22.868	6	5947.89	11562.25	0.293791	5614.356	0.572625
1000	31.182	0.005	22.868	8	7175.988	13002.05	0.326989	5826.058	0.594217
1000	31.182	0.005	22.868	10	8190.378	14050.27	0.349855	5859.894	0.597668
1000	31.182	0.005	22.868	12	9061.405	14865.51	0.366591	5804.106	0.591978
1000	31.182	0.005	22.868	14	9828.711	15527.02	0.379257	5698.31	0.581187
1000	31.182	0.005	22.868	16	10517.04	16080.18	0.389021	5563.148	0.567402
1000	31.182	0.005	22.868	18	11142.95	16553.26	0.396606	5410.308	0.551813
1000	31.182	0.005	22.868	20	11718.15	16964.96	0.402485	5246.811	0.535138

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	31.182	0.005	22.868	22	12253.42	17328.26	0.406879	5074.843	0.517598
1000	31.182	0.005	22.868	24	12751.29	17652.54	0.410196	4901.243	0.499892
1000	31.182	0.006	22.868	2	1986.953	5068.438	0.129701	3081.485	0.311431
1000	31.182	0.006	22.868	4	4350.983	9393.374	0.237067	5042.39	0.50961
1000	31.182	0.006	22.868	6	5932.779	11617.59	0.289969	5684.812	0.574537
1000	31.182	0.006	22.868	8	7154.136	13072.59	0.323073	5918.45	0.59815
1000	31.182	0.006	22.868	10	8162.07	14133.09	0.345981	5971.017	0.603462
1000	31.182	0.006	22.868	12	9026.924	14958.6	0.362841	5931.677	0.599486
1000	31.182	0.006	22.868	14	9788.32	15628.93	0.375689	5840.607	0.590282
1000	31.182	0.006	22.868	16	10470.97	16189.79	0.385682	5718.82	0.577974
1000	31.182	0.006	22.868	18	11091.43	16669.7	0.393537	5578.268	0.563769
1000	31.182	0.006	22.868	20	11661.36	17087.53	0.399724	5426.163	0.548396
1000	31.182	0.006	22.868	22	12189.33	17456.39	0.404566	5267.054	0.532316
1000	31.182	0.006	22.868	24	12684.1	17785.73	0.408188	5101.625	0.515597
1000	31.182	0.007	22.868	2	1985.316	5078.22	0.1276	3092.904	0.309767
1000	31.182	0.007	22.868	4	4343.001	9427.782	0.233705	5084.781	0.509262
1000	31.182	0.007	22.868	6	5918.077	11670.89	0.28622	5752.812	0.576169
1000	31.182	0.007	22.868	8	7132.915	13140.67	0.319213	6007.753	0.601702
1000	31.182	0.007	22.868	10	8134.617	14213.15	0.342142	6078.533	0.608791
1000	31.182	0.007	22.868	12	8993.525	15048.72	0.359103	6055.194	0.606453
1000	31.182	0.007	22.868	14	9749.235	15727.68	0.372107	5978.448	0.598767
1000	31.182	0.007	22.868	16	10426.44	16296.11	0.382298	5869.673	0.587873
1000	31.182	0.007	22.868	18	11041.66	16782.73	0.390389	5741.072	0.574993
1000	31.182	0.007	22.868	20	11606.55	17206.59	0.396845	5600.042	0.560868
1000	31.182	0.007	22.868	22	12129.64	17580.92	0.401988	5451.273	0.545968
1000	31.182	0.007	22.868	24	12617.42	17915.26	0.406047	5297.84	0.530601
1000	31.182	0.008	22.868	2	1983.71	5087.561	0.125562	3103.85	0.308087
1000	31.182	0.008	22.868	4	4335.214	9460.828	0.230423	5125.614	0.508766
1000	31.182	0.008	22.868	6	5903.767	11722.24	0.282542	5818.471	0.577539
1000	31.182	0.008	22.868	8	7112.294	13206.4	0.315411	6094.101	0.604898
1000	31.182	0.008	22.868	10	8107.978	14290.57	0.338344	6182.593	0.613681
1000	31.182	0.008	22.868	12	8961.151	15135.97	0.355385	6174.819	0.61291
1000	31.182	0.008	22.868	14	9711.387	15823.4	0.36852	6112.011	0.606675
1000	31.182	0.008	22.868	16	10383.35	16399.25	0.378884	6015.897	0.597135
1000	31.182	0.008	22.868	18	10993.54	16892.46	0.387179	5898.923	0.585524
1000	31.182	0.008	22.868	20	11553.59	17322.25	0.39387	5768.666	0.572595
1000	31.182	0.008	22.868	22	12072.01	17701.96	0.399276	5629.953	0.558826
1000	31.182	0.008	22.868	24	12555.27	18041.23	0.403625	5485.96	0.544534
1000	32.182	0.004	23.868	2	1984.996	5058.747	0.130579	3073.75	0.306927
1000	32.182	0.004	23.868	4	4343.362	9361.456	0.238311	5018.095	0.501078

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	32.182	0.004	23.868	6	5920.309	11570.09	0.291272	5649.779	0.564154
1000	32.182	0.004	23.868	8	7137.717	13013.81	0.324369	5876.088	0.586752
1000	32.182	0.004	23.868	10	8142.394	14065.43	0.347231	5923.04	0.59144
1000	32.182	0.004	23.868	12	9004.521	14883.84	0.364035	5879.315	0.587074
1000	32.182	0.004	23.868	14	9763.604	15548.28	0.376818	5784.678	0.577624
1000	32.182	0.004	23.868	16	10444.28	16104.18	0.386741	5659.9	0.565165
1000	32.182	0.004	23.868	18	11063.03	16579.81	0.394519	5516.777	0.550873
1000	32.182	0.004	23.868	20	11631.48	16993.89	0.400623	5362.417	0.53546
1000	32.182	0.004	23.868	22	12160.37	17359.45	0.405277	5199.081	0.51915
1000	32.182	0.004	23.868	24	12652.19	17685.85	0.408883	5033.656	0.502632
1000	32.182	0.005	23.868	2	1983.398	5068.961	0.128458	3085.563	0.305362
1000	32.182	0.005	23.868	4	4335.536	9397.056	0.234938	5061.52	0.500912
1000	32.182	0.005	23.868	6	5905.867	11624.97	0.287521	5719.103	0.56599
1000	32.182	0.005	23.868	8	7116.837	13083.7	0.320517	5966.864	0.59051
1000	32.182	0.005	23.868	10	8115.346	14147.44	0.343409	6032.094	0.596965
1000	32.182	0.005	23.868	12	8971.575	14975.97	0.360321	6004.399	0.594224
1000	32.182	0.005	23.868	14	9725.01	15649.11	0.373267	5924.098	0.586277
1000	32.182	0.005	23.868	16	10400.26	16212.59	0.383396	5812.332	0.575216
1000	32.182	0.005	23.868	18	11013.79	16694.95	0.391417	5681.156	0.562235
1000	32.182	0.005	23.868	20	11577.21	17115.08	0.397799	5537.866	0.548054
1000	32.182	0.005	23.868	22	12099.02	17486.1	0.402863	5387.082	0.533132
1000	32.182	0.005	23.868	24	12587.96	17817.49	0.406736	5229.535	0.51754
1000	32.182	0.006	23.868	2	1981.83	5078.706	0.1264	3096.877	0.303776
1000	32.182	0.006	23.868	4	4327.9	9431.235	0.231643	5103.335	0.500592
1000	32.182	0.006	23.868	6	5891.808	11677.84	0.28384	5786.03	0.567558
1000	32.182	0.006	23.868	8	7096.546	13151.18	0.31672	6054.635	0.593906
1000	32.182	0.006	23.868	10	8089.098	14226.74	0.339624	6137.647	0.602049
1000	32.182	0.006	23.868	12	8939.64	15065.19	0.356622	6125.554	0.600863
1000	32.182	0.006	23.868	14	9687.637	15746.85	0.369707	6059.208	0.594355
1000	32.182	0.006	23.868	16	10357.67	16317.78	0.380014	5960.11	0.584634
1000	32.182	0.006	23.868	18	10966.2	16806.76	0.388248	5840.561	0.572907
1000	32.182	0.006	23.868	20	11524.78	17232.83	0.394873	5708.042	0.559908
1000	32.182	0.006	23.868	22	12041.93	17609.24	0.400208	5567.309	0.546104
1000	32.182	0.006	23.868	24	12524.06	17945.55	0.404483	5421.491	0.5318
1000	32.182	0.007	23.868	2	1980.292	5088.014	0.124403	3107.722	0.302172
1000	32.182	0.007	23.868	4	4320.446	9464.07	0.228424	5143.624	0.500129
1000	32.182	0.007	23.868	6	5878.115	11728.79	0.280229	5850.671	0.568877
1000	32.182	0.007	23.868	8	7076.817	13216.34	0.312979	6139.527	0.596963
1000	32.182	0.007	23.868	10	8063.609	14303.45	0.335879	6239.842	0.606717
1000	32.182	0.007	23.868	12	8908.664	15151.6	0.352945	6242.937	0.607018
1000	32.182	0.007	23.868	14	9651.421	15841.6	0.366146	6190.179	0.601888
1000	32.182	0.007	23.868	16	10316.44	16419.85	0.376608	6103.413	0.593452
1000	32.182	0.007	23.868	18	10920.14	16915.33	0.385027	5995.184	0.582928

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	32.182	0.007	23.868	20	11474.09	17347.24	0.391865	5873.148	0.571062
1000	32.182	0.007	23.868	22	11986.76	17728.96	0.397438	5742.196	0.55833
1000	32.182	0.007	23.868	24	12464.56	18070.12	0.401974	5605.559	0.545044
1000	32.182	0.008	23.868	2	1978.783	5096.911	0.122463	3118.128	0.300554
1000	32.182	0.008	23.868	4	4313.168	9495.629	0.225281	5182.461	0.499534
1000	32.182	0.008	23.868	6	5864.773	11777.9	0.276687	5913.13	0.569962
1000	32.182	0.008	23.868	8	7057.624	13279.29	0.309296	6221.665	0.599702
1000	32.182	0.008	23.868	10	8038.846	14377.66	0.332176	6338.817	0.610994
1000	32.182	0.008	23.868	12	8878.601	15235.3	0.349293	6356.698	0.612717
1000	32.182	0.008	23.868	14	9616.304	15933.48	0.362593	6317.172	0.608907
1000	32.182	0.008	23.868	16	10276.49	16518.91	0.373188	6242.415	0.601702
1000	32.182	0.008	23.868	18	10875.56	17020.77	0.381769	6145.208	0.592332
1000	32.182	0.008	23.868	20	11425.04	17458.42	0.388792	6033.38	0.581553
1000	32.182	0.008	23.868	22	11933.41	17845.36	0.394573	5911.948	0.569848
1000	32.182	0.008	23.868	24	12407.06	18191.3	0.399338	5784.246	0.557539
1200	28.182	0.004	19.868	2	2009.993	6023.558	0.146347	4013.566	0.455332
1200	28.182	0.004	19.868	4	4451.196	11060.6	0.265914	6609.4	0.749824
1200	28.182	0.004	19.868	6	6112.997	13608.67	0.324402	7495.675	0.85037
1200	28.182	0.004	19.868	8	7409.877	15256.83	0.360929	7846.957	0.890223
1200	28.182	0.004	19.868	10	8488.554	16450.47	0.386397	7961.913	0.903264
1200	28.182	0.004	19.868	12	9419.856	17375.16	0.405362	7955.308	0.902515
1200	28.182	0.004	19.868	14	10243.95	18120.55	0.419912	7876.602	0.893586
1200	28.182	0.004	19.868	16	10988.13	18741.57	0.43136	7753.436	0.879613
1200	28.182	0.004	19.868	18	11665.85	19270.95	0.440595	7605.103	0.862785
1200	28.182	0.004	19.868	20	12290.58	19730.31	0.448085	7439.729	0.844023
1200	28.182	0.004	19.868	22	12871.17	20134.62	0.454186	7263.443	0.824024
1200	28.182	0.004	19.868	24	13414.33	20494.61	0.459148	7080.289	0.803246
1200	28.182	0.005	19.868	2	2007.816	6040.985	0.143336	4033.169	0.452931
1200	28.182	0.005	19.868	4	4440.66	11120.86	0.26118	6680.195	0.750196
1200	28.182	0.005	19.868	6	6093.309	13701.09	0.319154	7607.78	0.854365
1200	28.182	0.005	19.868	8	7381.163	15373.99	0.355526	7992.827	0.897606
1200	28.182	0.005	19.868	10	8451.11	16587.53	0.380999	8136.418	0.913732
1200	28.182	0.005	19.868	12	9374.004	17528.93	0.400065	8154.925	0.91581
1200	28.182	0.005	19.868	14	10190	18288.43	0.414771	8098.43	0.909466
1200	28.182	0.005	19.868	16	10924.28	18921.73	0.426482	7997.446	0.898125
1200	28.182	0.005	19.868	18	11596.09	19461.96	0.435904	7865.869	0.883349
1200	28.182	0.005	19.868	20	12213.39	19931.02	0.443665	7717.624	0.866701
1200	28.182	0.005	19.868	22	12786.76	20344.08	0.450065	7557.318	0.848698
1200	28.182	0.005	19.868	24	13322.88	20712.05	0.455355	7389.167	0.829815
1200	28.182	0.006	19.868	2	2005.691	6057.384	0.140437	4051.692	0.450458
1200	28.182	0.006	19.868	4	4430.426	11178.04	0.25658	6747.616	0.750185

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1200	28.182	0.006	19.868	6	6074.241	13789.2	0.314025	7714.955	0.857732
1200	28.182	0.006	19.868	8	7353.416	15486.02	0.35022	8132.609	0.904166
1200	28.182	0.006	19.868	10	8414.993	16718.9	0.375674	8303.904	0.92321
1200	28.182	0.006	19.868	12	9329.845	17676.58	0.394812	8346.732	0.927971
1200	28.182	0.006	19.868	14	10138.11	18449.87	0.409644	8311.76	0.924083
1200	28.182	0.006	19.868	16	10864.94	19095.19	0.421521	8230.245	0.915021
1200	28.182	0.006	19.868	18	11529.19	19646.06	0.431154	8116.865	0.902415
1200	28.182	0.006	19.868	20	12139.45	20124.65	0.439145	7985.197	0.887777
1200	28.182	0.006	19.868	22	12705.98	20546.32	0.445799	7840.347	0.871673
1200	28.182	0.006	19.868	24	13235.45	20922.15	0.451366	7686.699	0.85459
1200	28.182	0.007	19.868	2	2003.617	6072.838	0.137644	4069.22	0.447925
1200	28.182	0.007	19.868	4	4420.478	11232.36	0.252112	6811.882	0.749827
1200	28.182	0.007	19.868	6	6055.761	13873.24	0.309017	7817.482	0.86052
1200	28.182	0.007	19.868	8	7326.583	15593.21	0.345014	8266.624	0.90996
1200	28.182	0.007	19.868	10	8380.125	16844.85	0.370427	8464.72	0.931766
1200	28.182	0.007	19.868	12	9287.273	17816.59	0.389532	8529.32	0.938877
1200	28.182	0.007	19.868	14	10088.15	18605.13	0.404544	8516.985	0.937519
1200	28.182	0.007	19.868	16	10807.87	19262.22	0.416558	8454.34	0.930623
1200	28.182	0.007	19.868	18	11463.33	19823.51	0.426415	8360.18	0.920259
1200	28.182	0.007	19.868	20	12068.52	20311.45	0.434554	8242.925	0.907351
1200	28.182	0.007	19.868	22	12628.56	20741.59	0.441425	8113.033	0.893053
1200	28.182	0.007	19.868	24	13151.73	21125.15	0.447229	7973.415	0.877685
1200	28.182	0.008	19.868	2	2001.591	6087.423	0.134953	4085.832	0.445342
1200	28.182	0.008	19.868	4	4410.805	11284	0.247772	6873.194	0.749155
1200	28.182	0.008	19.868	6	6037.84	13953.46	0.304127	7915.624	0.862776
1200	28.182	0.008	19.868	8	7300.614	15695.79	0.339912	8395.174	0.915045
1200	28.182	0.008	19.868	10	8346.437	16965.63	0.365263	8619.198	0.939463
1200	28.182	0.008	19.868	12	9246.198	17952.68	0.38439	8706.481	0.948977
1200	28.182	0.008	19.868	14	10040	18754.47	0.39948	8714.479	0.949848
1200	28.182	0.008	19.868	16	10752.93	19423.06	0.411607	8670.128	0.945014
1200	28.182	0.008	19.868	18	11401.85	19994.56	0.421604	8592.715	0.936577
1200	28.182	0.008	19.868	20	11998.66	20491.67	0.429965	8493.01	0.925709
1200	28.182	0.008	19.868	22	12554.28	20930.13	0.436972	8375.851	0.912939
1200	28.182	0.008	19.868	24	13071.46	21321.28	0.442978	8249.815	0.899202
1400	28.182	0.004	19.868	2	2009.993	7041.256	0.146033	5031.263	0.570787
1400	28.182	0.004	19.868	4	4451.196	12951.32	0.266602	8500.129	0.964324
1400	28.182	0.004	19.868	6	6112.997	15949.24	0.326418	9836.246	1.115904
1400	28.182	0.004	19.868	8	7409.877	17891.44	0.364338	10481.57	1.189114
1400	28.182	0.004	19.868	10	8488.554	19299.57	0.391231	10811.01	1.22649
1400	28.182	0.004	19.868	12	9419.856	20389.72	0.411581	10969.86	1.24451
1400	28.182	0.004	19.868	14	10243.95	21270.92	0.427642	11026.97	1.250989
1400	28.182	0.004	19.868	16	10988.13	22005.38	0.440651	11017.24	1.249886

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1400	28.182	0.004	19.868	18	11665.85	22631.68	0.451477	10965.83	1.244054
1400	28.182	0.004	19.868	20	12290.58	23175.33	0.460609	10884.74	1.234854
1400	28.182	0.004	19.868	22	12871.17	23655.37	0.46847	10784.2	1.223447
1400	28.182	0.004	19.868	24	13414.33	24081.37	0.475183	10667.05	1.210157
1400	28.182	0.005	19.868	2	2007.816	7063.902	0.142669	5056.087	0.567806
1400	28.182	0.005	19.868	4	4440.66	13030.18	0.261251	8589.523	0.964616
1400	28.182	0.005	19.868	6	6093.309	16070.61	0.320413	9977.297	1.120465
1400	28.182	0.005	19.868	8	7381.163	18045.65	0.358071	10664.49	1.197638
1400	28.182	0.005	19.868	10	8451.11	19480.28	0.384869	11029.17	1.238593
1400	28.182	0.005	19.868	12	9374.004	20592.55	0.405214	11218.54	1.259859
1400	28.182	0.005	19.868	14	10190	21492.66	0.421324	11302.66	1.269306
1400	28.182	0.005	19.868	16	10924.28	22243.6	0.434463	11319.32	1.271177
1400	28.182	0.005	19.868	18	11596.09	22884.48	0.445364	11288.4	1.267704
1400	28.182	0.005	19.868	20	12213.39	23441.17	0.454628	11227.78	1.260897
1400	28.182	0.005	19.868	22	12786.76	23933.25	0.462642	11146.49	1.251767
1400	28.182	0.005	19.868	24	13322.88	24369.96	0.469514	11047.08	1.240604
1400	28.182	0.006	19.868	2	2005.691	7085.03	0.139443	5079.339	0.56471
1400	28.182	0.006	19.868	4	4430.426	13104.43	0.256071	8674.008	0.964357
1400	28.182	0.006	19.868	6	6074.241	16185.45	0.314569	10111.21	1.124143
1400	28.182	0.006	19.868	8	7353.416	18192.08	0.351943	10838.66	1.205019
1400	28.182	0.006	19.868	10	8414.993	19652.32	0.378627	11237.33	1.249342
1400	28.182	0.006	19.868	12	9329.845	20786.03	0.398945	11456.18	1.273673
1400	28.182	0.006	19.868	14	10138.11	21704.53	0.415083	11566.42	1.28593
1400	28.182	0.006	19.868	16	10864.94	22471.54	0.428283	11606.59	1.290395
1400	28.182	0.006	19.868	18	11529.19	23126.66	0.43928	11597.46	1.289381
1400	28.182	0.006	19.868	20	12139.45	23696.11	0.448651	11556.66	1.284844
1400	28.182	0.006	19.868	22	12705.98	24198.08	0.456718	11492.11	1.277667
1400	28.182	0.006	19.868	24	13235.45	24647.21	0.463799	11411.76	1.268735
1400	28.182	0.007	19.868	2	2003.617	7104.78	0.13635	5101.163	0.561518
1400	28.182	0.007	19.868	4	4420.478	13174.43	0.251059	8753.95	0.963603
1400	28.182	0.007	19.868	6	6055.761	16294.23	0.308883	10238.47	1.127014
1400	28.182	0.007	19.868	8	7326.583	18331.2	0.345958	11004.62	1.211349
1400	28.182	0.007	19.868	10	8380.125	19816.16	0.372508	11436.04	1.258838
1400	28.182	0.007	19.868	12	9287.273	20970.64	0.392782	11683.37	1.286063
1400	28.182	0.007	19.868	14	10088.15	21907.01	0.408927	11818.86	1.300978
1400	28.182	0.007	19.868	16	10807.87	22689.65	0.42217	11881.78	1.307903
1400	28.182	0.007	19.868	18	11463.33	23358.66	0.433273	11895.33	1.309395
1400	28.182	0.007	19.868	20	12068.52	23940.59	0.442698	11872.07	1.306834
1400	28.182	0.007	19.868	22	12628.56	24453.87	0.450865	11825.31	1.301688
1400	28.182	0.007	19.868	24	13151.73	24911.79	0.457994	11760.06	1.294505
1400	28.182	0.008	19.868	2	2001.591	7123.278	0.133382	5121.687	0.558246
1400	28.182	0.008	19.868	4	4410.805	13240.49	0.246209	8829.685	0.962405

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1400	28.182	0.008	19.868	6	6037.84	16397.33	0.303354	10359.49	1.129149
1400	28.182	0.008	19.868	8	7300.614	18463.46	0.340117	11162.85	1.216712
1400	28.182	0.008	19.868	10	8346.437	19972.28	0.366517	11625.84	1.267177
1400	28.182	0.008	19.868	12	9246.198	21146.86	0.386729	11900.66	1.297131
1400	28.182	0.008	19.868	14	10040	22100.56	0.402864	12060.56	1.31456
1400	28.182	0.008	19.868	16	10752.93	22898.41	0.416132	12145.48	1.323816
1400	28.182	0.008	19.868	18	11401.85	23580.95	0.427284	12179.11	1.327481
1400	28.182	0.008	19.868	20	11998.66	24175.06	0.436817	12176.4	1.327186
1400	28.182	0.008	19.868	22	12554.28	24699.4	0.445032	12145.13	1.323777
1400	28.182	0.008	19.868	24	13071.46	25167.44	0.452253	12095.97	1.31842
1600	28.182	0.004	19.868	2	2009.993	8062.361	0.145318	6052.368	0.68663
1600	28.182	0.004	19.868	4	4451.196	14853.74	0.26619	10402.54	1.180149
1600	28.182	0.004	19.868	6	6112.997	18307.93	0.326678	12194.93	1.383492
1600	28.182	0.004	19.868	8	7409.877	20549.2	0.365337	13139.32	1.490632
1600	28.182	0.004	19.868	10	8488.554	22175.92	0.392982	13687.37	1.552806
1600	28.182	0.004	19.868	12	9419.856	23436.34	0.414086	14016.48	1.590144
1600	28.182	0.004	19.868	14	10243.95	24455.85	0.430902	14211.9	1.612314
1600	28.182	0.004	19.868	16	10988.13	25306.05	0.444678	14317.92	1.624341
1600	28.182	0.004	19.868	18	11665.85	26031.39	0.456266	14365.55	1.629745
1600	28.182	0.004	19.868	20	12290.58	26661.26	0.466166	14370.68	1.630326
1600	28.182	0.004	19.868	22	12871.17	27215.99	0.474739	14344.82	1.627393
1600	28.182	0.004	19.868	24	13414.33	27710.22	0.482245	14295.9	1.621843
1600	28.182	0.005	19.868	2	2007.816	8090.607	0.14162	6082.791	0.683107
1600	28.182	0.005	19.868	4	4440.66	14952.81	0.260263	10512.15	1.18053
1600	28.182	0.005	19.868	6	6093.309	18460.91	0.319983	12367.6	1.3889
1600	28.182	0.005	19.868	8	7381.163	20744.02	0.3583	13362.85	1.500669
1600	28.182	0.005	19.868	10	8451.11	22404.61	0.385787	13953.5	1.566999
1600	28.182	0.005	19.868	12	9374.004	23693.34	0.406829	14319.34	1.608083
1600	28.182	0.005	19.868	14	10190	24737.12	0.423638	14547.12	1.633663
1600	28.182	0.005	19.868	16	10924.28	25608.5	0.437478	14684.22	1.64906
1600	28.182	0.005	19.868	18	11596.09	26352.6	0.449094	14756.51	1.657178
1600	28.182	0.005	19.868	20	12213.39	26999.27	0.459065	14785.87	1.660476
1600	28.182	0.005	19.868	22	12786.76	27569.2	0.467723	14782.45	1.660091
1600	28.182	0.005	19.868	24	13322.88	28077.31	0.475324	14754.42	1.656944
1600	28.182	0.006	19.868	2	2005.691	8116.745	0.138092	6111.054	0.679414
1600	28.182	0.006	19.868	4	4430.426	15045.39	0.254548	10614.96	1.180148
1600	28.182	0.006	19.868	6	6074.241	18604.64	0.313488	12530.4	1.393103
1600	28.182	0.006	19.868	8	7353.416	20927.73	0.351444	13574.32	1.509163
1600	28.182	0.006	19.868	10	8414.993	22620.85	0.378753	14205.86	1.579377
1600	28.182	0.006	19.868	12	9329.845	23936.91	0.399712	14607.06	1.623982
1600	28.182	0.006	19.868	14	10138.11	25004.17	0.416496	14866.05	1.652775
1600	28.182	0.006	19.868	16	10864.94	25896.09	0.430346	15031.14	1.67113

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1600	28.182	0.006	19.868	18	11529.19	26658.43	0.442002	15129.23	1.682035
1600	28.182	0.006	19.868	20	12139.45	27321.47	0.452028	15182.02	1.687904
1600	28.182	0.006	19.868	22	12705.98	27906.25	0.460752	15200.28	1.689934
1600	28.182	0.006	19.868	24	13235.45	28427.91	0.468429	15192.46	1.689065
1600	28.182	0.007	19.868	2	2003.617	8140.994	0.134722	6137.377	0.67558
1600	28.182	0.007	19.868	4	4420.478	15132.02	0.249038	10711.55	1.179088
1600	28.182	0.007	19.868	6	6055.761	18739.83	0.307192	12684.07	1.396216
1600	28.182	0.007	19.868	8	7326.583	21101.11	0.344771	13774.53	1.51625
1600	28.182	0.007	19.868	10	8380.125	22825.47	0.371884	14445.34	1.590091
1600	28.182	0.007	19.868	12	9287.273	24167.84	0.392743	14880.57	1.637999
1600	28.182	0.007	19.868	14	10088.15	25257.79	0.409484	15169.64	1.669819
1600	28.182	0.007	19.868	16	10807.87	26169.62	0.423327	15361.74	1.690965
1600	28.182	0.007	19.868	18	11463.33	26949.66	0.435032	15486.33	1.70468
1600	28.182	0.007	19.868	20	12068.52	27628.64	0.445069	15560.12	1.712802
1600	28.182	0.007	19.868	22	12628.56	28227.89	0.453843	15599.33	1.717118
1600	28.182	0.007	19.868	24	13151.73	28762.78	0.46158	15611.05	1.718408
1600	28.182	0.008	19.868	2	2001.591	8163.543	0.131503	6161.952	0.671632
1600	28.182	0.008	19.868	4	4410.805	15213.23	0.243727	10802.42	1.177427
1600	28.182	0.008	19.868	6	6037.84	18867.11	0.301092	12829.28	1.398347
1600	28.182	0.008	19.868	8	7300.614	21264.88	0.338282	13964.26	1.522057
1600	28.182	0.008	19.868	10	8346.437	23019.19	0.365184	14672.75	1.59928
1600	28.182	0.008	19.868	12	9246.198	24386.9	0.385927	15140.7	1.650285
1600	28.182	0.008	19.868	14	10040	25498.75	0.402609	15458.76	1.684951
1600	28.182	0.008	19.868	16	10752.93	26429.85	0.41643	15676.92	1.70873
1600	28.182	0.008	19.868	18	11401.85	27227.07	0.428138	15825.22	1.724895
1600	28.182	0.008	19.868	20	11998.66	27921.53	0.438228	15922.87	1.735538
1600	28.182	0.008	19.868	22	12554.28	28534.85	0.447011	15980.57	1.741828
1600	28.182	0.008	19.868	24	13071.46	29082.64	0.454793	16011.18	1.745164
1800	28.182	0.004	19.868	2	2009.993	9086.76	0.144383	7076.767	0.802846
1800	28.182	0.004	19.868	4	4451.196	16767.27	0.265181	12316.07	1.397236
1800	28.182	0.004	19.868	6	6112.997	20683.89	0.326009	14570.89	1.65304
1800	28.182	0.004	19.868	8	7409.877	23229.09	0.36509	15819.21	1.79466
1800	28.182	0.004	19.868	10	8488.554	25078.37	0.393178	16589.82	1.882084
1800	28.182	0.004	19.868	12	9419.856	26512.41	0.414728	17092.55	1.939118
1800	28.182	0.004	19.868	14	10243.95	27673.11	0.431988	17429.16	1.977306
1800	28.182	0.004	19.868	16	10988.13	28641.59	0.446211	17653.45	2.002751
1800	28.182	0.004	19.868	18	11665.85	29468.22	0.458238	17802.37	2.019646
1800	28.182	0.004	19.868	20	12290.58	30186.33	0.468573	17895.74	2.030239
1800	28.182	0.004	19.868	22	12871.17	30819	0.477579	17947.83	2.036148
1800	28.182	0.004	19.868	24	13414.33	31382.86	0.485516	17968.53	2.038496
1800	28.182	0.005	19.868	2	2007.816	9120.894	0.14037	7113.078	0.798809

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1800	28.182	0.005	19.868	4	4440.66	16887.93	0.258709	12447.27	1.397847
1800	28.182	0.005	19.868	6	6093.309	20870.81	0.318664	14777.5	1.659536
1800	28.182	0.005	19.868	8	7381.163	23467.63	0.357336	16086.47	1.806535
1800	28.182	0.005	19.868	10	8451.11	25358.83	0.385217	16907.72	1.898763
1800	28.182	0.005	19.868	12	9374.004	26828	0.406663	17453.99	1.960109
1800	28.182	0.005	19.868	14	10190	28018.85	0.42388	17828.85	2.002207
1800	28.182	0.005	19.868	16	10924.28	29013.68	0.438126	18089.4	2.031467
1800	28.182	0.005	19.868	18	11596.09	29863.68	0.450152	18267.6	2.051479
1800	28.182	0.005	19.868	20	12213.39	30602.76	0.460527	18389.37	2.065154
1800	28.182	0.005	19.868	22	12786.76	31254.42	0.469585	18467.66	2.073946
1800	28.182	0.005	19.868	24	13322.88	31835.61	0.477584	18512.73	2.079008
1800	28.182	0.006	19.868	2	2005.691	9152.242	0.136557	7146.55	0.794538
1800	28.182	0.006	19.868	4	4430.426	16999.85	0.252491	12569.42	1.397441
1800	28.182	0.006	19.868	6	6074.241	21045.2	0.311562	14970.95	1.664438
1800	28.182	0.006	19.868	8	7353.416	23691.06	0.349806	16337.65	1.816384
1800	28.182	0.006	19.868	10	8414.993	25622.3	0.377458	17207.31	1.913071
1800	28.182	0.006	19.868	12	9329.845	27125.17	0.39878	17795.32	1.978445
1800	28.182	0.006	19.868	14	10138.11	28345.05	0.415935	18206.94	2.024208
1800	28.182	0.006	19.868	16	10864.94	29365.33	0.430157	18500.39	2.056832
1800	28.182	0.006	19.868	18	11529.19	30237.96	0.442191	18708.76	2.08
1800	28.182	0.006	19.868	20	12139.45	30997.37	0.452588	18857.92	2.096583
1800	28.182	0.006	19.868	22	12705.98	31667.5	0.461682	18961.52	2.1081
1800	28.182	0.006	19.868	24	13235.45	32265.57	0.469726	19030.12	2.115727
1800	28.182	0.007	19.868	2	2003.617	9181.117	0.132931	7177.5	0.790073
1800	28.182	0.007	19.868	4	4420.478	17103.86	0.246518	12683.38	1.396141
1800	28.182	0.007	19.868	6	6055.761	21208.11	0.3047	15152.35	1.667916
1800	28.182	0.007	19.868	8	7326.583	23900.55	0.342501	16573.97	1.824402
1800	28.182	0.007	19.868	10	8380.125	25870.01	0.369906	17489.88	1.925223
1800	28.182	0.007	19.868	12	9287.273	27405.17	0.391087	18117.9	1.994353
1800	28.182	0.007	19.868	14	10088.15	28652.97	0.408161	18564.82	2.043548
1800	28.182	0.007	19.868	16	10807.87	29697.78	0.422343	18889.9	2.079333
1800	28.182	0.007	19.868	18	11463.33	30592.27	0.434388	19128.94	2.105645
1800	28.182	0.007	19.868	20	12068.52	31371.38	0.444772	19302.86	2.124789
1800	28.182	0.007	19.868	22	12628.56	32059.42	0.453887	19430.85	2.138878
1800	28.182	0.007	19.868	24	13151.73	32673.89	0.461962	19522.16	2.148929
1800	28.182	0.008	19.868	2	2001.591	9207.792	0.129482	7206.201	0.785451
1800	28.182	0.008	19.868	4	4410.805	17200.71	0.240782	12789.9	1.394055
1800	28.182	0.008	19.868	6	6037.84	21360.53	0.298075	15322.69	1.67012
1800	28.182	0.008	19.868	8	7300.614	24097.18	0.33542	16796.57	1.830768
1800	28.182	0.008	19.868	10	8346.437	26103.09	0.362563	17756.66	1.935415
1800	28.182	0.008	19.868	12	9246.198	27669.18	0.383587	18422.98	2.008042
1800	28.182	0.008	19.868	14	10040	28943.78	0.400566	18903.79	2.060448
1800	28.182	0.008	19.868	16	10752.93	30012.22	0.414694	19259.29	2.099196

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1800	28.182	0.008	19.868	18	11401.85	30927.8	0.426712	19525.96	2.128263
1800	28.182	0.008	19.868	20	11998.66	31725.96	0.437113	19727.3	2.150209
1800	28.182	0.008	19.868	22	12554.28	32431.34	0.446214	19877.06	2.166532
1800	28.182	0.008	19.868	24	13071.46	33061.73	0.454308	19990.27	2.178871
2000	28.182	0.004	19.868	2	2009.993	10114.36	0.143322	8104.369	0.919426
2000	28.182	0.004	19.868	4	4451.196	18691.41	0.26382	14240.21	1.615526
2000	28.182	0.004	19.868	6	6112.997	23076.34	0.324795	16963.34	1.924459
2000	28.182	0.004	19.868	8	7409.877	25930.14	0.364123	18520.26	2.101089
2000	28.182	0.004	19.868	10	8488.554	28005.83	0.392487	19517.28	2.214199
2000	28.182	0.004	19.868	12	9419.856	29616.73	0.414321	20196.87	2.291298
2000	28.182	0.004	19.868	14	10243.95	30921.44	0.431866	20677.49	2.345822
2000	28.182	0.004	19.868	16	10988.13	32010.65	0.446375	21022.52	2.384965
2000	28.182	0.004	19.868	18	11665.85	32940.76	0.458682	21274.92	2.4136
2000	28.182	0.004	19.868	20	12290.58	33749.1	0.469294	21458.51	2.434429
2000	28.182	0.004	19.868	22	12871.17	34461.52	0.478574	21590.34	2.449384
2000	28.182	0.004	19.868	24	13414.33	35096.64	0.486782	21682.32	2.459818
2000	28.182	0.005	19.868	2	2007.816	10154.59	0.139007	8146.771	0.914895
2000	28.182	0.005	19.868	4	4440.66	18834.81	0.256827	14394.15	1.616485
2000	28.182	0.005	19.868	6	6093.309	23299.19	0.31683	17205.88	1.932247
2000	28.182	0.005	19.868	8	7381.163	26215.13	0.355688	18833.96	2.115082
2000	28.182	0.005	19.868	10	8451.11	28341.4	0.383801	19890.29	2.23371
2000	28.182	0.005	19.868	12	9374.004	29994.79	0.405498	20620.79	2.315746
2000	28.182	0.005	19.868	14	10190	31336.03	0.42297	21146.03	2.374731
2000	28.182	0.005	19.868	16	10924.28	32457.22	0.437473	21532.94	2.418182
2000	28.182	0.005	19.868	18	11596.09	33415.74	0.44976	21819.65	2.45038
2000	28.182	0.005	19.868	20	12213.39	34249.57	0.460389	22036.18	2.474696
2000	28.182	0.005	19.868	22	12786.76	34985.11	0.4697	22198.35	2.492908
2000	28.182	0.005	19.868	24	13322.88	35641.36	0.477949	22318.48	2.506399
2000	28.182	0.006	19.868	2	2005.691	10191.27	0.134926	8185.575	0.910054
2000	28.182	0.006	19.868	4	4430.426	18966.87	0.250134	14536.45	1.616131
2000	28.182	0.006	19.868	6	6074.241	23505.68	0.309154	17431.44	1.937989
2000	28.182	0.006	19.868	8	7353.416	26480.29	0.347522	19126.87	2.126484
2000	28.182	0.006	19.868	10	8414.993	28654.62	0.375361	20239.63	2.250198
2000	28.182	0.006	19.868	12	9329.845	30348.55	0.396898	21018.71	2.336814
2000	28.182	0.006	19.868	14	10138.11	31724.79	0.414279	21586.68	2.39996
2000	28.182	0.006	19.868	16	10864.94	32876.71	0.428732	22011.76	2.44722
2000	28.182	0.006	19.868	18	11529.19	33862.58	0.441002	22333.39	2.482977
2000	28.182	0.006	19.868	20	12139.45	34721.05	0.451632	22581.6	2.510573
2000	28.182	0.006	19.868	22	12705.98	35478.96	0.460958	22772.98	2.53185
2000	28.182	0.006	19.868	24	13235.45	36155.69	0.469232	22920.24	2.548223
2000	28.182	0.007	19.868	2	2003.617	10224.83	0.131063	8221.215	0.904962

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
2000	28.182	0.007	19.868	4	4420.478	19088.79	0.243728	14668.31	1.614634
2000	28.182	0.007	19.868	6	6055.761	23697.33	0.301763	17641.57	1.94192
2000	28.182	0.007	19.868	8	7326.583	26727.33	0.339625	19400.75	2.135564
2000	28.182	0.007	19.868	10	8380.125	28947.27	0.367172	20567.14	2.263957
2000	28.182	0.007	19.868	12	9287.273	30679.85	0.388531	21392.58	2.354818
2000	28.182	0.007	19.868	14	10088.15	32089.55	0.405802	22001.4	2.421835
2000	28.182	0.007	19.868	16	10807.87	33270.95	0.420189	22463.08	2.472654
2000	28.182	0.007	19.868	18	11463.33	34283.13	0.432443	22819.8	2.511921
2000	28.182	0.007	19.868	20	12068.52	35165.33	0.44304	23096.81	2.542413
2000	28.182	0.007	19.868	22	12628.56	35944.85	0.452366	23316.29	2.566573
2000	28.182	0.007	19.868	24	13151.73	36641.41	0.460652	23489.67	2.585658
2000	28.182	0.008	19.868	2	2001.591	10255.65	0.127403	8254.06	0.899664
2000	28.182	0.008	19.868	4	4410.805	19201.59	0.237599	14790.78	1.612145
2000	28.182	0.008	19.868	6	6037.84	23875.52	0.29465	17837.69	1.944247
2000	28.182	0.008	19.868	8	7300.614	26957.81	0.331995	19657.2	2.142567
2000	28.182	0.008	19.868	10	8346.437	29221.01	0.359235	20874.57	2.275257
2000	28.182	0.008	19.868	12	9246.198	30990.39	0.380401	21744.19	2.370043
2000	28.182	0.008	19.868	14	10040	32432.06	0.397546	22392.07	2.440659
2000	28.182	0.008	19.868	16	10752.93	33641.7	0.411852	22888.77	2.494798
2000	28.182	0.008	19.868	18	11401.85	34679.14	0.424055	23277.29	2.537145
2000	28.182	0.008	19.868	20	11998.66	35584.18	0.434644	23585.52	2.570741
2000	28.182	0.008	19.868	22	12554.28	36384.53	0.443939	23830.25	2.597416
2000	28.182	0.008	19.868	24	13071.46	37100.21	0.452224	24028.75	2.619051
1000	28.182	0	19.868	2	2019.263	4951.222	0.157293	2931.959	0.346789
1000	28.182	0	19.868	4	4496.658	8986.785	0.280066	4490.127	0.531087
1000	28.182	0	19.868	6	6198.685	10993.02	0.336663	4794.332	0.567068
1000	28.182	0	19.868	8	7535.651	12276.43	0.369409	4740.781	0.560734
1000	28.182	0	19.868	10	8653.402	13199.8	0.39002	4546.395	0.537742
1000	28.182	0	19.868	12	9624.636	13910.49	0.403014	4285.849	0.506925
1000	28.182	0	19.868	14	10486.49	14482.28	0.410782	3995.786	0.472617
1000	28.182	0	19.868	16	11265.42	14957.02	0.414444	3691.601	0.436638
1000	28.182	0	19.868	18	11978.41	15360.53	0.414636	3382.118	0.400033
1000	28.182	0	19.868	20	12637.54	15709.79	0.411664	3072.253	0.363382
1000	28.182	0	19.868	22	13251.7	16016.53	0.405606	2764.822	0.32702
1000	28.182	0	19.868	24	13827.67	16289.12	0.396353	2461.448	0.291137
1000	29.182	0	20.868	2	2011.967	4968.019	0.152494	2956.052	0.337657
1000	29.182	0	20.868	4	4463.175	9045.742	0.2727	4582.567	0.523447
1000	29.182	0	20.868	6	6138.042	11084.62	0.328864	4946.581	0.565026
1000	29.182	0	20.868	8	7449.14	12393.26	0.361906	4944.119	0.564745
1000	29.182	0	20.868	10	8542.5	13337.24	0.38326	4794.738	0.547682
1000	29.182	0	20.868	12	9488.641	14065.3	0.39747	4576.657	0.522772
1000	29.182	0	20.868	14	10330.12	14652.08	0.40663	4321.958	0.493679
1000	29.182	0	20.868	16	11088.02	15139.97	0.412164	4051.951	0.462837

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	29.182	0	20.868	18	11780.89	15555.19	0.414686	3774.298	0.431122
1000	29.182	0	20.868	20	12420.7	15915	0.414601	3494.303	0.399139
1000	29.182	0	20.868	22	13016.25	16231.31	0.412123	3215.061	0.367242
1000	29.182	0	20.868	24	13574.25	16512.68	0.407332	2938.429	0.335644
1000	30.182	0	21.868	2	2005.183	4983.77	0.147977	2978.587	0.328958
1000	30.182	0	21.868	4	4432.198	9101.277	0.265683	4669.079	0.515658
1000	30.182	0	21.868	6	6082.096	11171.17	0.321338	5089.075	0.562043
1000	30.182	0	21.868	8	7369.484	12503.79	0.354529	5134.301	0.567038
1000	30.182	0	21.868	10	8440.536	13467.42	0.376416	5026.883	0.555175
1000	30.182	0	21.868	12	9365.64	14212.08	0.391448	4846.437	0.535246
1000	30.182	0	21.868	14	10186.74	14813.2	0.401725	4626.459	0.510951
1000	30.182	0	21.868	16	10925.52	15313.7	0.408627	4388.174	0.484635
1000	30.182	0	21.868	18	11600.12	15740.16	0.412818	4140.038	0.45723
1000	30.182	0	21.868	20	12222.4	16110.1	0.414746	3887.701	0.429362
1000	30.182	0	21.868	22	12801.08	16435.63	0.414687	3634.546	0.401403
1000	30.182	0	21.868	24	13342.82	16725.45	0.412803	3382.627	0.373581
1000	31.182	0	22.868	2	1998.862	4998.576	0.143719	2999.714	0.320667
1000	31.182	0	22.868	4	4403.462	9153.675	0.258994	4750.213	0.507794
1000	31.182	0	22.868	6	6030.324	11251.15	0.313969	5220.826	0.558103
1000	31.182	0	22.868	8	7295.908	12608.52	0.347313	5312.608	0.567914
1000	31.182	0	22.868	10	8346.483	13590.9	0.369574	5244.417	0.560624
1000	31.182	0	22.868	12	9252.318	14351.43	0.385219	5099.111	0.545091
1000	31.182	0	22.868	14	10053.12	14966.28	0.396415	4913.163	0.525214
1000	31.182	0	22.868	16	10776.15	15478.88	0.404261	4702.727	0.502718
1000	31.182	0	22.868	18	11434.08	15916.13	0.409681	4482.046	0.479127
1000	31.182	0	22.868	20	12040.39	16295.81	0.413063	4255.419	0.454901
1000	31.182	0	22.868	22	12603.72	16630.2	0.414711	4026.482	0.430428
1000	31.182	0	22.868	24	13130.66	16928.16	0.414825	3797.496	0.40595
1000	32.182	0	23.868	2	1992.953	5012.512	0.139696	3019.56	0.312759
1000	32.182	0	23.868	4	4376.725	9203.193	0.252616	4826.468	0.499914
1000	32.182	0	23.868	6	5982.28	11328.41	0.306968	5346.125	0.553739
1000	32.182	0	23.868	8	7227.743	12707.89	0.340278	5480.147	0.56762
1000	32.182	0	23.868	10	8259.465	13708.18	0.362791	5448.716	0.564365
1000	32.182	0	23.868	12	9147.579	14483.9	0.378892	5336.321	0.552723
1000	32.182	0	23.868	14	9931.649	15111.92	0.390707	5180.267	0.536559
1000	32.182	0	23.868	16	10636.4	15636.11	0.399439	4999.712	0.517858
1000	32.182	0	23.868	18	11281.06	16083.73	0.405691	4802.67	0.497449
1000	32.182	0	23.868	20	11872.76	16472.77	0.410151	4600.008	0.476458
1000	32.182	0	23.868	22	12422.07	16815.7	0.413044	4393.63	0.455082
1000	32.182	0	23.868	24	12935.5	17121.49	0.414588	4185.989	0.433575
1200	28.182	0	19.868	2	2019.263	5941.511	0.159615	3922.248	0.463919

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1200	28.182	0	19.868	4	4496.658	10784.15	0.286245	6287.489	0.743677
1200	28.182	0	19.868	6	6198.685	13190.38	0.346573	6991.696	0.826969
1200	28.182	0	19.868	8	7535.651	14731.25	0.383428	7195.596	0.851086
1200	28.182	0	19.868	10	8653.402	15840.99	0.408621	7187.591	0.85014
1200	28.182	0	19.868	12	9624.636	16693.3	0.426658	7068.668	0.836074
1200	28.182	0	19.868	14	10486.49	17379.18	0.440137	6892.685	0.815259
1200	28.182	0	19.868	16	11265.42	17948.7	0.450344	6683.284	0.790491
1200	28.182	0	19.868	18	11978.41	18432.81	0.458088	6454.401	0.763419
1200	28.182	0	19.868	20	12637.54	18851.87	0.463892	6214.33	0.735023
1200	28.182	0	19.868	22	13251.7	19219.91	0.46811	5968.203	0.705912
1200	28.182	0	19.868	24	13827.67	19547	0.470986	5719.324	0.676475
1400	28.182	0	19.868	2	2019.263	6931.931	0.161038	4912.668	0.581065
1400	28.182	0	19.868	4	4496.658	12581.53	0.289796	8084.869	0.956269
1400	28.182	0	19.868	6	6198.685	15388.78	0.352019	9190.097	1.086994
1400	28.182	0	19.868	8	7535.651	17186.46	0.390728	9650.806	1.141486
1400	28.182	0	19.868	10	8653.402	18479.49	0.417723	9826.083	1.162217
1400	28.182	0	19.868	12	9624.636	19474.57	0.437763	9849.935	1.165039
1400	28.182	0	19.868	14	10486.49	20275.14	0.453317	9788.647	1.15779
1400	28.182	0	19.868	16	11265.42	20939.8	0.465709	9674.385	1.144275
1400	28.182	0	19.868	18	11978.41	21505.91	0.475829	9527.495	1.126901
1400	28.182	0	19.868	20	12637.54	21994.55	0.484089	9357.012	1.106736
1400	28.182	0	19.868	22	13251.7	22423.75	0.49094	9172.048	1.084859
1400	28.182	0	19.868	24	13827.67	22805.22	0.496646	8977.552	1.061854
1600	28.182	0	19.868	2	2019.263	7922.653	0.162006	5903.39	0.698246
1600	28.182	0	19.868	4	4496.658	14378.97	0.292104	9882.314	1.168868
1600	28.182	0	19.868	6	6198.685	17587.21	0.355448	11388.52	1.347021
1600	28.182	0	19.868	8	7535.651	19641.68	0.395201	12106.03	1.431886
1600	28.182	0	19.868	10	8653.402	21119.42	0.423208	12466.01	1.474465
1600	28.182	0	19.868	12	9624.636	22256.66	0.444263	12632.02	1.4941
1600	28.182	0	19.868	14	10486.49	23171.59	0.460833	12685.1	1.500378
1600	28.182	0	19.868	16	11265.42	23931.2	0.474258	12665.79	1.498094
1600	28.182	0	19.868	18	11978.41	24576.83	0.485376	12598.42	1.490126
1600	28.182	0	19.868	20	12637.54	25135.66	0.494737	12498.12	1.478263
1600	28.182	0	19.868	22	13251.7	25626.44	0.502718	12374.73	1.463669
1600	28.182	0	19.868	24	13827.67	26062.59	0.509589	12234.92	1.447132
1800	28.182	0	19.868	2	2019.263	8913.939	0.162716	6894.676	0.815494
1800	28.182	0	19.868	4	4496.658	16176.56	0.293726	11679.9	1.381484
1800	28.182	0	19.868	6	6198.685	19785.68	0.357807	13587	1.607054
1800	28.182	0	19.868	8	7535.651	22096.92	0.398223	14561.27	1.72229
1800	28.182	0	19.868	10	8653.402	23759.36	0.426854	15105.96	1.786715

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1800	28.182	0	19.868	12	9624.636	25038.75	0.448519	15414.11	1.823163
1800	28.182	0	19.868	14	10486.49	26068.05	0.465684	15581.55	1.842968
1800	28.182	0	19.868	16	11265.42	26922.61	0.4797	15657.19	1.851914
1800	28.182	0	19.868	18	11978.41	27648.94	0.491408	15670.53	1.853491
1800	28.182	0	19.868	20	12637.54	28277.62	0.501361	15640.08	1.84989
1800	28.182	0	19.868	22	13251.7	28829.75	0.509941	15578.04	1.842552
1800	28.182	0	19.868	24	13827.67	29320.42	0.517417	15492.74	1.832463
2000	28.182	0	19.868	2	2019.263	9906.106	0.16327	7886.843	0.932846
2000	28.182	0	19.868	4	4496.658	17974.39	0.294933	13477.73	1.59413
2000	28.182	0	19.868	6	6198.685	21984.27	0.359531	15785.59	1.8671
2000	28.182	0	19.868	8	7535.651	24552.22	0.400402	17016.57	2.012699
2000	28.182	0	19.868	10	8653.402	26399.34	0.429454	17745.94	2.098968
2000	28.182	0	19.868	12	9624.636	27820.86	0.451522	18196.22	2.152228
2000	28.182	0	19.868	14	10486.49	28964.51	0.469074	18478.02	2.185558
2000	28.182	0	19.868	16	11265.42	29914.02	0.483467	18648.6	2.205735
2000	28.182	0	19.868	18	11978.41	30721.05	0.495547	18742.64	2.216857
2000	28.182	0	19.868	20	12637.54	31419.59	0.505869	18782.05	2.221518
2000	28.182	0	19.868	22	13251.7	32033.05	0.514814	18781.35	2.221436
2000	28.182	0	19.868	24	13827.67	32578.24	0.522657	18750.57	2.217795

3.2.2 For the one inter cooler used in compression process

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	28.182	0.004	19.868	2	1911.75	9182.17	0.335424	7270.42	0.824816
1000	28.182	0.004	19.868	4	4019.985	15514.26	0.558905	11494.27	1.304004
1000	28.182	0.004	19.868	6	5351.587	18241.04	0.648858	12889.46	1.462285
1000	28.182	0.004	19.868	8	6343.236	19833.31	0.697416	13490.07	1.530424
1000	28.182	0.004	19.868	10	7140.309	20902.23	0.727243	13761.92	1.561264
1000	28.182	0.004	19.868	12	7810.211	21681.2	0.746923	13870.99	1.573638
1000	28.182	0.004	19.868	14	8390.012	22278.56	0.760363	13888.55	1.57563
1000	28.182	0.004	19.868	16	8902.391	22755.66	0.769797	13853.27	1.571628
1000	28.182	0.004	19.868	18	9362.289	23147.31	0.776448	13785.02	1.563885
1000	28.182	0.004	19.868	20	9780.093	23476.03	0.781105	13695.94	1.553779
1000	28.182	0.004	19.868	22	10163.33	23756.42	0.784261	13593.09	1.542111
1000	28.182	0.004	19.868	24	10517.64	23999.48	0.786303	13481.85	1.52949
1000	28.182	0.005	19.868	2	1910.77	9225.715	0.330175	7314.945	0.821479
1000	28.182	0.005	19.868	4	4015.632	15642.92	0.552446	11627.29	1.305762
1000	28.182	0.005	19.868	6	5343.899	18421.65	0.642709	13077.75	1.468651
1000	28.182	0.005	19.868	8	6332.464	20048.83	0.691783	13716.37	1.540369
1000	28.182	0.005	19.868	10	7126.69	21143.04	0.722137	14016.35	1.574057

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	28.182	0.005	19.868	12	7793.946	21941.16	0.742311	14147.22	1.588754
1000	28.182	0.005	19.868	14	8371.27	22554.35	0.75625	14183.08	1.592782
1000	28.182	0.005	19.868	16	8881.321	23044.2	0.766139	14162.88	1.590513
1000	28.182	0.005	19.868	18	9339.015	23446.54	0.773221	14107.53	1.584297
1000	28.182	0.005	19.868	20	9754.723	23784.37	0.778285	14029.64	1.57555
1000	28.182	0.005	19.868	22	10135.96	24073.11	0.781857	13937.15	1.565163
1000	28.182	0.005	19.868	24	10488.36	24322.83	0.784257	13834.48	1.553633
1000	28.182	0.006	19.868	2	1909.812	9267.377	0.325064	7357.565	0.817998
1000	28.182	0.006	19.868	4	4011.383	15767.58	0.546086	11756.2	1.307029
1000	28.182	0.006	19.868	6	5336.406	18597.67	0.63662	13261.26	1.474358
1000	28.182	0.006	19.868	8	6321.974	20259.68	0.68618	13937.7	1.549564
1000	28.182	0.006	19.868	10	7113.437	21379.27	0.71704	14265.84	1.586045
1000	28.182	0.006	19.868	12	7778.128	22196.67	0.737687	14418.54	1.603022
1000	28.182	0.006	19.868	14	8353.056	22825.66	0.752096	14472.61	1.609033
1000	28.182	0.006	19.868	16	8860.851	23328.38	0.762422	14467.53	1.608468
1000	28.182	0.006	19.868	18	9316.414	23741.54	0.769915	14425.13	1.603754
1000	28.182	0.006	19.868	20	9730.099	24088.6	0.77537	14358.5	1.596347
1000	28.182	0.006	19.868	22	10109.41	24385.31	0.779311	14275.91	1.587164
1000	28.182	0.006	19.868	24	10459.95	24642.72	0.782103	14182.76	1.576809
1000	28.182	0.007	19.868	2	1908.874	9307.261	0.320087	7398.387	0.814388
1000	28.182	0.007	19.868	4	4007.234	15888.37	0.539825	11881.13	1.307832
1000	28.182	0.007	19.868	6	5329.098	18769.2	0.63059	13440.1	1.479438
1000	28.182	0.007	19.868	8	6311.755	20465.93	0.680609	14154.17	1.55804
1000	28.182	0.007	19.868	10	7100.535	21610.64	0.711936	14510.1	1.59722
1000	28.182	0.007	19.868	12	7762.739	22447.68	0.73305	14684.94	1.616465
1000	28.182	0.007	19.868	14	8335.344	23092.48	0.747905	14757.14	1.624413
1000	28.182	0.007	19.868	16	8840.956	23608.18	0.758648	14767.23	1.625523
1000	28.182	0.007	19.868	18	9294.456	24032.28	0.766537	14737.82	1.622287
1000	28.182	0.007	19.868	20	9706.183	24388.7	0.772366	14682.52	1.616199
1000	28.182	0.007	19.868	22	10083.62	24693.52	0.776662	14609.9	1.608205
1000	28.182	0.007	19.868	24	10432.39	24957.99	0.77979	14525.6	1.598926
1000	28.182	0.008	19.868	2	1907.955	9345.465	0.315241	7437.51	0.810663
1000	28.182	0.008	19.868	4	4003.182	16005.4	0.533662	12002.22	1.308201
1000	28.182	0.008	19.868	6	5321.97	18936.32	0.62462	13614.35	1.483918
1000	28.182	0.008	19.868	8	6301.795	20667.66	0.675071	14365.86	1.56583
1000	28.182	0.008	19.868	10	7087.969	21837.49	0.706843	14749.53	1.607648
1000	28.182	0.008	19.868	12	7747.759	22694.17	0.7284	14946.41	1.629107
1000	28.182	0.008	19.868	14	8318.112	23355.2	0.743699	15037.09	1.638991
1000	28.182	0.008	19.868	16	8821.609	23883.6	0.754824	15061.99	1.641706
1000	28.182	0.008	19.868	18	9273.112	24318.74	0.763091	15045.63	1.639922
1000	28.182	0.008	19.868	20	9682.943	24684.64	0.769279	15001.7	1.635133
1000	28.182	0.008	19.868	22	10058.58	24997.68	0.773916	14939.1	1.628311
1000	28.182	0.008	19.868	24	10405.62	25269.36	0.777367	14863.74	1.620097

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	29.182	0.004	20.868	2	1908.646	9230.712	0.326677	7322.066	0.803334
1000	29.182	0.004	20.868	4	4006.727	15672.74	0.547456	11666.01	1.279926
1000	29.182	0.004	20.868	6	5328.643	18475.71	0.637781	13147.06	1.442418
1000	29.182	0.004	20.868	8	6311.55	20123.53	0.687285	13811.98	1.515368
1000	29.182	0.004	20.868	10	7100.698	21235.63	0.718198	14134.93	1.550801
1000	29.182	0.004	20.868	12	7763.342	22047.96	0.738897	14284.62	1.567224
1000	29.182	0.004	20.868	14	8336.434	22674.22	0.753402	14337.78	1.573057
1000	29.182	0.004	20.868	16	8842.566	23175.45	0.763837	14332.89	1.57252
1000	29.182	0.004	20.868	18	9296.607	23587.92	0.771445	14291.31	1.567958
1000	29.182	0.004	20.868	20	9708.888	23934.81	0.777017	14225.92	1.560784
1000	29.182	0.004	20.868	22	10086.89	24231.71	0.781075	14144.82	1.551886
1000	29.182	0.004	20.868	24	10436.23	24489.58	0.783984	14053.35	1.54185
1000	29.182	0.005	20.868	2	1907.732	9272.037	0.321681	7364.305	0.800068
1000	29.182	0.005	20.868	4	4002.678	15795.85	0.541205	11793.17	1.281225
1000	29.182	0.005	20.868	6	5321.506	18649.31	0.631755	13327.81	1.447951
1000	29.182	0.005	20.868	8	6301.561	20331.44	0.681703	14029.88	1.524225
1000	29.182	0.005	20.868	10	7088.08	21468.37	0.713071	14380.29	1.562294
1000	29.182	0.005	20.868	12	7748.284	22299.91	0.734218	14551.63	1.580908
1000	29.182	0.005	20.868	14	8319.097	22941.71	0.749156	14622.62	1.588621
1000	29.182	0.005	20.868	16	8823.085	23455.68	0.759995	14632.6	1.589705
1000	29.182	0.005	20.868	18	9275.098	23878.86	0.767987	14603.77	1.586573
1000	29.182	0.005	20.868	20	9685.454	24234.93	0.773923	14549.48	1.580675
1000	29.182	0.005	20.868	22	10061.62	24539.78	0.778326	14478.16	1.572926
1000	29.182	0.005	20.868	24	10409.2	24804.56	0.78156	14395.35	1.56393
1000	29.182	0.006	20.868	2	1906.837	9311.612	0.316814	7404.775	0.796675
1000	29.182	0.006	20.868	4	3998.723	15915.16	0.535051	11916.44	1.282082
1000	29.182	0.006	20.868	6	5314.541	18818.53	0.625791	13503.99	1.452885
1000	29.182	0.006	20.868	8	6291.823	20534.88	0.676157	14243.06	1.532401
1000	29.182	0.006	20.868	10	7075.788	21696.06	0.707931	14620.27	1.572985
1000	29.182	0.006	20.868	12	7733.624	22547.43	0.729533	14813.8	1.593807
1000	29.182	0.006	20.868	14	8302.226	23205.27	0.744906	14903.04	1.603408
1000	29.182	0.006	20.868	16	8804.136	23731.61	0.75611	14927.47	1.606037
1000	29.182	0.006	20.868	18	9254.186	24165.62	0.76447	14911.43	1.604311
1000	29.182	0.006	20.868	20	9662.678	24530.97	0.770754	14868.3	1.59967
1000	29.182	0.006	20.868	22	10037.07	24843.89	0.775488	14806.81	1.593055
1000	29.182	0.006	20.868	24	10382.95	25115.72	0.779037	14732.77	1.585089
1000	29.182	0.007	20.868	2	1905.96	9349.532	0.312073	7443.572	0.793169
1000	29.182	0.007	20.868	4	3992.725	16030.82	0.52906	12038.09	1.28275
1000	29.182	0.007	20.868	6	5307.743	18983.45	0.619887	13675.7	1.457249
1000	29.182	0.007	20.868	8	6282.327	20733.91	0.670649	14451.58	1.539925
1000	29.182	0.007	20.868	10	7063.808	21919.76	0.702829	14855.95	1.583014

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	29.182	0.007	20.868	12	7719.345	22790.5	0.724841	15071.15	1.605945
1000	29.182	0.007	20.868	14	8285.801	23463.72	0.740596	15177.92	1.617322
1000	29.182	0.007	20.868	16	8785.696	24003.23	0.752185	15217.53	1.621543
1000	29.182	0.007	20.868	18	9233.844	24448.16	0.760897	15214.32	1.621201
1000	29.182	0.007	20.868	20	9640.53	24822.91	0.767516	15182.38	1.617797
1000	29.182	0.007	20.868	22	10013.2	25143.99	0.772568	15130.78	1.612299
1000	29.182	0.007	20.868	24	10357.44	25423	0.77642	15065.56	1.605349
1000	29.182	0.008	20.868	2	1905.101	9385.889	0.307454	7480.788	0.789562
1000	29.182	0.008	20.868	4	3989.07	16142.92	0.523093	12153.85	1.282783
1000	29.182	0.008	20.868	6	5301.106	19144.16	0.614045	13843.05	1.46107
1000	29.182	0.008	20.868	8	6273.062	20927.44	0.665126	14654.38	1.546702
1000	29.182	0.008	20.868	10	7052.129	22139.01	0.697741	15086.88	1.59235
1000	29.182	0.008	20.868	12	7705.431	23029.13	0.720146	15323.7	1.617346
1000	29.182	0.008	20.868	14	8269.804	23717.91	0.73627	15448.11	1.630476
1000	29.182	0.008	20.868	16	8767.744	24270.54	0.748223	15502.8	1.636249
1000	29.182	0.008	20.868	18	9214.046	24726.49	0.757273	15512.45	1.637267
1000	29.182	0.008	20.868	20	9618.983	25110.71	0.764213	15491.73	1.63508
1000	29.182	0.008	20.868	22	9989.992	25440.06	0.769571	15450.07	1.630683
1000	29.182	0.008	20.868	24	10332.64	25726.35	0.773714	15393.72	1.624735
1000	30.182	0.004	21.868	2	1905.745	9276.64	0.318368	7370.895	0.782922
1000	30.182	0.004	21.868	4	3994.36	15823.53	0.536401	11829.17	1.256471
1000	30.182	0.004	21.868	6	5307.263	18699.73	0.626933	13392.47	1.422521
1000	30.182	0.004	21.868	8	6282.045	20401.44	0.677228	14119.4	1.499734
1000	30.182	0.004	21.868	10	7063.832	21554.2	0.709014	14490.37	1.539138
1000	30.182	0.004	21.868	12	7719.742	22400.44	0.730669	14680.7	1.559354
1000	30.182	0.004	21.868	14	8286.614	23055.21	0.746123	14768.59	1.56869
1000	30.182	0.004	21.868	16	8786.955	23579.54	0.757412	14792.59	1.571239
1000	30.182	0.004	21.868	18	9235.568	24012.47	0.765868	14776.9	1.569573
1000	30.182	0.004	21.868	20	9642.735	24377.3	0.772251	14734.57	1.565076
1000	30.182	0.004	21.868	22	10015.9	24690.09	0.777085	14674.19	1.558663
1000	30.182	0.004	21.868	24	10360.63	24962.08	0.780734	14601.45	1.550937
1000	30.182	0.005	21.868	2	1904.89	9315.911	0.313607	7411.021	0.77973
1000	30.182	0.005	21.868	4	3988.38	15941.43	0.530422	11953.05	1.257606
1000	30.182	0.005	21.868	6	5300.619	18866.72	0.621036	13566.1	1.427319
1000	30.182	0.005	21.868	8	6272.757	20602.18	0.671713	14329.42	1.50763
1000	30.182	0.005	21.868	10	7052.11	21779.28	0.703893	14727.17	1.549479
1000	30.182	0.005	21.868	12	7705.764	22644.57	0.725945	14938.81	1.571745
1000	30.182	0.005	21.868	14	8270.53	23314.42	0.741766	15043.89	1.582801
1000	30.182	0.005	21.868	16	8768.891	23851.73	0.75343	15082.84	1.586899
1000	30.182	0.005	21.868	18	9215.634	24295.38	0.762228	15079.74	1.586573
1000	30.182	0.005	21.868	20	9621.025	24669.42	0.768936	15048.39	1.583275

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	30.182	0.005	21.868	22	9992.497	24990.22	0.77408	14997.72	1.577943
1000	30.182	0.005	21.868	24	10335.61	25269.24	0.778024	14933.63	1.5712
1000	30.182	0.006	21.868	2	1904.052	9353.552	0.308968	7449.5	0.776426
1000	30.182	0.006	21.868	4	3984.816	16055.74	0.524463	12070.92	1.258095
1000	30.182	0.006	21.868	6	5294.129	19029.5	0.6152	13735.37	1.431573
1000	30.182	0.006	21.868	8	6263.694	20797.55	0.66619	14533.86	1.514795
1000	30.182	0.006	21.868	10	7040.679	21999.96	0.698789	14959.28	1.559135
1000	30.182	0.006	21.868	12	7692.14	22884.34	0.721221	15192.2	1.583412
1000	30.182	0.006	21.868	14	8254.861	23569.45	0.737399	15314.59	1.596168
1000	30.182	0.006	21.868	16	8751.301	24119.69	0.749418	15368.38	1.601774
1000	30.182	0.006	21.868	18	9196.23	24574.14	0.758544	15377.91	1.602767
1000	30.182	0.006	21.868	20	9599.901	24957.49	0.765564	15357.58	1.600649
1000	30.182	0.006	21.868	22	9969.733	25286.39	0.771005	15316.66	1.596383
1000	30.182	0.006	21.868	24	10311.28	25572.55	0.775232	15261.27	1.590611
1000	30.182	0.007	21.868	2	1903.23	9389.652	0.304446	7486.422	0.773023
1000	30.182	0.007	21.868	4	3981.323	16166.58	0.518597	12185.25	1.258209
1000	30.182	0.007	21.868	6	5287.79	19188.17	0.609427	13900.39	1.435308
1000	30.182	0.007	21.868	8	6254.846	20989.29	0.660738	14734.44	1.52143
1000	30.182	0.007	21.868	10	7029.528	22216.28	0.693704	15186.75	1.568134
1000	30.182	0.007	21.868	12	7678.857	23119.78	0.7165	15440.93	1.594379
1000	30.182	0.007	21.868	14	8239.59	23820.26	0.733023	15580.67	1.608809
1000	30.182	0.007	21.868	16	8734.165	24383.94	0.745402	15649.77	1.615944
1000	30.182	0.007	21.868	18	9177.334	24848.76	0.75482	15671.43	1.61818
1000	30.182	0.007	21.868	20	9579.335	25241.49	0.76214	15662.16	1.617223
1000	30.182	0.007	21.868	22	9947.578	25578.59	0.767866	15631.01	1.614007
1000	30.182	0.007	21.868	24	10287.61	25871.98	0.772365	15584.38	1.609192
1000	30.182	0.008	21.868	2	1902.425	9424.293	0.300039	7521.869	0.769532
1000	30.182	0.008	21.868	4	3977.902	16274.05	0.512824	12296.15	1.25797
1000	30.182	0.008	21.868	6	5281.594	19342.83	0.603715	14061.23	1.438548
1000	30.182	0.008	21.868	8	6246.206	21176.77	0.655324	14930.56	1.527486
1000	30.182	0.008	21.868	10	7018.645	22428.3	0.68864	15409.65	1.5765
1000	30.182	0.008	21.868	12	7665.901	23350.85	0.711779	15684.95	1.604664
1000	30.182	0.008	21.868	14	8224.701	24066.84	0.728637	15842.14	1.620745
1000	30.182	0.008	21.868	16	8717.464	24643.19	0.741324	15925.73	1.629297
1000	30.182	0.008	21.868	18	9158.924	25119.24	0.751057	15960.31	1.632836
1000	30.182	0.008	21.868	20	9559.305	25521.43	0.758665	15962.12	1.63302
1000	30.182	0.008	21.868	22	9926.007	25866.8	0.764666	15940.79	1.630838
1000	30.182	0.008	21.868	24	10264.56	26167.5	0.769427	15902.94	1.626966
1000	31.182	0.004	22.868	2	1903.027	9320.159	0.310465	7417.132	0.763504
1000	31.182	0.004	22.868	4	3980.653	15967.17	0.525796	11986.52	1.233867

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	31.182	0.004	22.868	6	5287.292	18913.81	0.616328	13626.52	1.402685
1000	31.182	0.004	22.868	8	6254.503	20667.91	0.667283	14413.41	1.483685
1000	31.182	0.004	22.868	10	7029.439	21860.44	0.69983	14831	1.526671
1000	31.182	0.004	22.868	12	7679.083	22739.25	0.722297	15060.16	1.550261
1000	31.182	0.004	22.868	14	8240.172	23420.82	0.738535	15180.65	1.562663
1000	31.182	0.004	22.868	16	8735.131	23968.72	0.750624	15233.59	1.568113
1000	31.182	0.004	22.868	18	9178.703	24421.74	0.759831	15243.04	1.569086
1000	31.182	0.004	22.868	20	9581.119	24804.24	0.766934	15223.12	1.567035
1000	31.182	0.004	22.868	22	9949.786	25132.71	0.772461	15182.93	1.562898
1000	31.182	0.004	22.868	24	10290.24	25418.75	0.776774	15128.51	1.557296
1000	31.182	0.005	22.868	2	1902.225	9357.526	0.305924	7455.302	0.760388
1000	31.182	0.005	22.868	4	3977.245	16080.18	0.519938	12102.94	1.234414
1000	31.182	0.005	22.868	6	5281.091	19074.54	0.610561	13793.44	1.406834
1000	31.182	0.005	22.868	8	6245.846	20860.44	0.661783	14614.59	1.490585
1000	31.182	0.005	22.868	10	7018.522	22078.19	0.694731	15059.67	1.53598
1000	31.182	0.005	22.868	12	7666.074	22976.14	0.717564	15310.06	1.561518
1000	31.182	0.005	22.868	14	8225.211	23672.52	0.734122	15447.31	1.575516
1000	31.182	0.005	22.868	16	8718.337	24233.76	0.746568	15515.43	1.582464
1000	31.182	0.005	22.868	18	9160.178	24696.86	0.75605	15536.68	1.584631
1000	31.182	0.005	22.868	20	9560.953	25088.56	0.763445	15527.61	1.583707
1000	31.182	0.005	22.868	22	9928.057	25425.08	0.769249	15497.03	1.580587
1000	31.182	0.005	22.868	24	10267.02	25718.22	0.773827	15451.2	1.575913
1000	31.182	0.006	22.868	2	1901.439	9393.374	0.301497	7491.935	0.757174
1000	31.182	0.006	22.868	4	3973.905	16189.79	0.514172	12215.89	1.234602
1000	31.182	0.006	22.868	6	5275.031	19231.24	0.604857	13956.21	1.410487
1000	31.182	0.006	22.868	8	6237.39	21049.69	0.656368	14812.3	1.497009
1000	31.182	0.006	22.868	10	7007.865	22291.69	0.689655	15283.82	1.544663
1000	31.182	0.006	22.868	12	7653.382	23208.86	0.712841	15555.48	1.572118
1000	31.182	0.006	22.868	14	8210.621	23920.05	0.729703	15709.43	1.587677
1000	31.182	0.006	22.868	16	8701.967	24493.73	0.742446	15791.76	1.595998
1000	31.182	0.006	22.868	18	9142.127	24967.89	0.752238	15825.77	1.599435
1000	31.182	0.006	22.868	20	9541.309	25368.89	0.759913	15827.58	1.599618
1000	31.182	0.006	22.868	22	9906.896	25713.54	0.765984	15806.64	1.597502
1000	31.182	0.006	22.868	24	10244.41	26013.85	0.770816	15769.44	1.593742
1000	31.182	0.007	22.868	2	1900.667	9427.782	0.29718	7527.115	0.753872
1000	31.182	0.007	22.868	4	3970.631	16296.11	0.508497	12325.48	1.234449
1000	31.182	0.007	22.868	6	5269.105	19384.01	0.599216	14114.9	1.413667
1000	31.182	0.007	22.868	8	6229.128	21234.78	0.650994	15005.65	1.50288
1000	31.182	0.007	22.868	10	6997.46	22500.99	0.684604	15503.53	1.552744
1000	31.182	0.007	22.868	12	7640.995	23436.19	0.708074	15795.2	1.581956
1000	31.182	0.007	22.868	14	8196.388	24163.41	0.725281	15967.03	1.599165
1000	31.182	0.007	22.868	16	8686.003	24749.69	0.738314	16063.68	1.608846
1000	31.182	0.007	22.868	18	9124.53	25234.86	0.748397	16110.33	1.613517

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	31.182	0.007	22.868	20	9522.165	25645.22	0.756341	16123.05	1.614792
1000	31.182	0.007	22.868	22	9886.278	25998.06	0.762668	16111.78	1.613663
1000	31.182	0.007	22.868	24	10222.38	26305.62	0.767746	16083.23	1.610804
1000	31.182	0.008	22.868	2	1899.911	9460.828	0.29297	7560.918	0.750493
1000	31.182	0.008	22.868	4	3967.421	16399.25	0.502912	12431.83	1.233977
1000	31.182	0.008	22.868	6	5263.308	19532.93	0.593637	14269.62	1.416396
1000	31.182	0.008	22.868	8	6221.053	21415.77	0.645662	15194.71	1.50822
1000	31.182	0.008	22.868	10	6987.296	22706.16	0.67958	15718.86	1.560247
1000	31.182	0.008	22.868	12	7628.901	23660.07	0.70335	16031.16	1.591246
1000	31.182	0.008	22.868	14	8182.498	24402.61	0.720855	16220.11	1.610001
1000	31.182	0.008	22.868	16	8670.429	25001.59	0.73417	16331.16	1.621024
1000	31.182	0.008	22.868	18	9107.369	25498.22	0.74455	16390.86	1.626949
1000	31.182	0.008	22.868	20	9503.499	25917.54	0.752732	16414.04	1.629249
1000	31.182	0.008	22.868	22	9866.182	26278.63	0.759306	16412.45	1.629092
1000	31.182	0.008	22.868	24	10200.92	26593.51	0.76462	16392.59	1.627121
1000	32.182	0.004	23.868	2	1900.475	9361.456	0.30294	7460.981	0.74501
1000	32.182	0.004	23.868	4	3969.993	16104.18	0.515485	12134.19	1.21165
1000	32.182	0.004	23.868	6	5268.595	19118.59	0.60597	13850	1.382981
1000	32.182	0.004	23.868	8	6228.736	20921.86	0.657394	14693.13	1.467171
1000	32.182	0.004	23.868	10	6997.278	22154.56	0.69066	15157.28	1.513518
1000	32.182	0.004	23.868	12	7641.08	23065.26	0.713844	15424.18	1.54017
1000	32.182	0.004	23.868	14	8196.778	23773.04	0.730774	15576.26	1.555355
1000	32.182	0.004	23.868	16	8686.723	24344.13	0.743577	15657.41	1.563458
1000	32.182	0.004	23.868	18	9125.599	24816.46	0.753431	15690.86	1.566799
1000	32.182	0.004	23.868	20	9523.594	25216.32	0.761176	15692.72	1.566985
1000	32.182	0.004	23.868	22	9888.077	25560.26	0.767319	15672.18	1.564933
1000	32.182	0.004	23.868	24	10224.56	25860.19	0.772225	15635.63	1.561283
1000	32.182	0.005	23.868	2	1899.722	9397.056	0.298604	7497.334	0.741972
1000	32.182	0.005	23.868	4	3966.795	16212.59	0.509817	12245.8	1.211903
1000	32.182	0.005	23.868	6	5262.796	19273.39	0.600337	14010.59	1.386556
1000	32.182	0.005	23.868	8	6220.648	21108.72	0.65202	14888.07	1.473396
1000	32.182	0.005	23.868	10	6987.086	22365.34	0.685599	15378.25	1.521906
1000	32.182	0.005	23.868	12	7628.943	23294.35	0.709081	15665.41	1.550324
1000	32.182	0.005	23.868	14	8182.828	24017.39	0.726322	15834.57	1.567065
1000	32.182	0.005	23.868	16	8671.072	24600.85	0.739404	15929.78	1.576488
1000	32.182	0.005	23.868	18	9108.342	25084.04	0.749543	15975.7	1.581032
1000	32.182	0.005	23.868	20	9504.815	25493.09	0.75755	15988.28	1.582277
1000	32.182	0.005	23.868	22	9867.848	25845.08	0.763942	15977.23	1.581184
1000	32.182	0.005	23.868	24	10202.95	26152.13	0.769087	15949.19	1.578409
1000	32.182	0.006	23.868	2	1898.983	9431.235	0.294375	7532.253	0.738847

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	32.182	0.006	23.868	4	3963.66	16317.78	0.504238	12354.13	1.21183
1000	32.182	0.006	23.868	6	5257.123	19424.33	0.594765	14167.21	1.389678
1000	32.182	0.006	23.868	8	6212.74	21291.5	0.646689	15078.76	1.479093
1000	32.182	0.006	23.868	10	6977.129	22572.02	0.680567	15594.89	1.529721
1000	32.182	0.006	23.868	12	7617.091	23519.5	0.70434	15902.41	1.559886
1000	32.182	0.006	23.868	14	8169.211	24257.65	0.72187	16088.44	1.578133
1000	32.182	0.006	23.868	16	8655.8	24853.59	0.735226	16197.8	1.58886
1000	32.182	0.006	23.868	18	9091.509	25348.17	0.745659	16256.66	1.594635
1000	32.182	0.006	23.868	20	9486.502	25765.92	0.753892	16279.42	1.596867
1000	32.182	0.006	23.868	22	9848.128	26126.03	0.760525	16277.9	1.596718
1000	32.182	0.006	23.868	24	10181.88	26440.27	0.765899	16258.39	1.594804
1000	32.182	0.007	23.868	2	1898.257	9464.07	0.290249	7565.812	0.735645
1000	32.182	0.007	23.868	4	3960.584	16419.85	0.498747	12459.27	1.211449
1000	32.182	0.007	23.868	6	5251.572	19571.51	0.589257	14319.94	1.392367
1000	32.182	0.007	23.868	8	6205.008	21470.26	0.6414	15265.25	1.484282
1000	32.182	0.007	23.868	10	6967.398	22774.67	0.675564	15807.27	1.536985
1000	32.182	0.007	23.868	12	7605.514	23740.54	0.699613	16135.03	1.568853
1000	32.182	0.007	23.868	14	8155.915	24494.02	0.71743	16338.11	1.588599
1000	32.182	0.007	23.868	16	8640.892	25102.34	0.73104	16461.45	1.600592
1000	32.182	0.007	23.868	18	9075.084	25607.47	0.741718	16532.39	1.60749
1000	32.182	0.007	23.868	20	9468.638	26034.81	0.750205	16566.18	1.610775
1000	32.182	0.007	23.868	22	9828.895	26403.1	0.757069	16574.2	1.611555
1000	32.182	0.007	23.868	24	10161.34	26724.59	0.762664	16563.25	1.61049
1000	32.182	0.008	23.868	2	1897.545	9495.629	0.286224	7598.084	0.732374
1000	32.182	0.008	23.868	4	3957.566	16518.91	0.493342	12561.34	1.210778
1000	32.182	0.008	23.868	6	5246.138	19715.02	0.583811	14468.88	1.394644
1000	32.182	0.008	23.868	8	6197.445	21645.07	0.636155	15447.63	1.488985
1000	32.182	0.008	23.868	10	6957.885	22973.34	0.670591	16015.46	1.543718
1000	32.182	0.008	23.868	12	7594.2	23957.52	0.694902	16363.32	1.577248
1000	32.182	0.008	23.868	14	8142.927	24726.73	0.713009	16583.8	1.5985
1000	32.182	0.008	23.868	16	8626.336	25347.08	0.726848	16720.75	1.6117
1000	32.182	0.008	23.868	18	9059.049	25862.89	0.737764	16803.84	1.61971
1000	32.182	0.008	23.868	20	9451.205	26300.44	0.746522	16849.24	1.624085
1000	32.182	0.008	23.868	22	9810.131	26676.29	0.753579	16866.15	1.625716
1000	32.182	0.008	23.868	24	10141.31	27005.09	0.759387	16863.78	1.625487
1200	28.182	0.004	19.868	2	1911.75	11060.6	0.320622	9148.846	1.03792
1200	28.182	0.004	19.868	4	4019.985	18741.57	0.536793	14721.58	1.670136
1200	28.182	0.004	19.868	6	5351.587	22063.11	0.625332	16711.52	1.895891
1200	28.182	0.004	19.868	8	6343.236	24007.25	0.67414	17664.01	2.00395
1200	28.182	0.004	19.868	10	7140.309	25314.73	0.704905	18174.42	2.061854
1200	28.182	0.004	19.868	12	7810.211	26267.04	0.725784	18456.83	2.093893
1200	28.182	0.004	19.868	14	8390.012	26999.47	0.740673	18609.45	2.111208

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1200	28.182	0.004	19.868	16	8902.391	27584.39	0.751628	18682	2.119438
1200	28.182	0.004	19.868	18	9362.289	28064.41	0.759837	18702.12	2.12172
1200	28.182	0.004	19.868	20	9780.093	28467.49	0.766083	18687.39	2.12005
1200	28.182	0.004	19.868	22	10163.33	28811.81	0.770862	18648.48	2.115636
1200	28.182	0.004	19.868	24	10517.64	29110.19	0.774521	18592.56	2.109291
1200	28.182	0.005	19.868	2	1910.77	11120.86	0.314921	9210.085	1.034306
1200	28.182	0.005	19.868	4	4015.632	18921.73	0.529752	14906.1	1.673977
1200	28.182	0.005	19.868	6	5343.899	22317.25	0.618589	16973.35	1.906132
1200	28.182	0.005	19.868	8	6332.464	24311.42	0.667903	17978.95	2.019064
1200	28.182	0.005	19.868	10	7126.69	25655.84	0.699201	18529.15	2.080852
1200	28.182	0.005	19.868	12	7793.946	26635.89	0.720553	18841.94	2.115979
1200	28.182	0.005	19.868	14	8371.27	27391.24	0.735912	19019.97	2.135971
1200	28.182	0.005	19.868	16	8881.321	27994.11	0.747265	19112.79	2.146395
1200	28.182	0.005	19.868	18	9339.015	28490.35	0.755891	19151.33	2.150723
1200	28.182	0.005	19.868	20	9754.723	28906.26	0.762484	19151.53	2.150746
1200	28.182	0.005	19.868	22	10135.96	29262.17	0.767607	19126.21	2.147902
1200	28.182	0.005	19.868	24	10488.36	29570.72	0.771591	19082.37	2.142978
1200	28.182	0.006	19.868	2	1909.812	11178.04	0.309387	9268.23	1.030422
1200	28.182	0.006	19.868	4	4011.383	19095.19	0.522824	15083.81	1.676985
1200	28.182	0.006	19.868	6	5336.406	22563.62	0.611908	17227.21	1.915284
1200	28.182	0.006	19.868	8	6321.974	24607.54	0.661692	18285.56	2.032949
1200	28.182	0.006	19.868	10	7113.437	25987.65	0.693447	18874.21	2.098394
1200	28.182	0.006	19.868	12	7778.128	26996.87	0.715298	19218.74	2.136698
1200	28.182	0.006	19.868	14	8353.056	27774.37	0.731071	19421.31	2.159219
1200	28.182	0.006	19.868	16	8860.851	28396.35	0.742843	19535.5	2.171914
1200	28.182	0.006	19.868	18	9316.414	28908.09	0.751834	19591.67	2.178159
1200	28.182	0.006	19.868	20	9730.099	29337.84	0.75879	19607.74	2.179946
1200	28.182	0.006	19.868	22	10109.41	29705.52	0.764244	19596.11	2.178653
1200	28.182	0.006	19.868	24	10459.95	30024.42	0.76854	19564.47	2.175135
1200	28.182	0.007	19.868	2	1908.874	11232.36	0.304016	9323.486	1.026296
1200	28.182	0.007	19.868	4	4007.234	19262.22	0.51601	15254.98	1.679213
1200	28.182	0.007	19.868	6	5329.098	22802.42	0.605291	17473.33	1.923401
1200	28.182	0.007	19.868	8	6311.755	24895.74	0.655509	18583.98	2.045658
1200	28.182	0.007	19.868	10	7100.535	26312.34	0.687725	19211.81	2.114766
1200	28.182	0.007	19.868	12	7762.739	27350.05	0.710026	19587.32	2.156101
1200	28.182	0.007	19.868	14	8335.344	28150.21	0.726208	19814.87	2.181149
1200	28.182	0.007	19.868	16	8840.956	28791.05	0.738365	19950.09	2.196034
1200	28.182	0.007	19.868	18	9294.456	29318.6	0.747711	20024.15	2.204186
1200	28.182	0.007	19.868	20	9706.183	29762.63	0.755026	20056.45	2.207741
1200	28.182	0.007	19.868	22	10083.62	30141.8	0.760781	20058.18	2.207932
1200	28.182	0.007	19.868	24	10432.39	30471.22	0.765376	20038.84	2.205803
1200	28.182	0.008	19.868	2	1907.955	11284	0.298802	9376.043	1.021957

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1200	28.182	0.008	19.868	4	4003.182	19423.06	0.50931	15419.87	1.680713
1200	28.182	0.008	19.868	6	5321.97	23033.86	0.598741	17711.89	1.930535
1200	28.182	0.008	19.868	8	6301.795	25176.16	0.649358	18874.37	2.057241
1200	28.182	0.008	19.868	10	7087.969	26629.16	0.682008	19541.19	2.129923
1200	28.182	0.008	19.868	12	7747.759	27695.54	0.70474	19947.78	2.17424
1200	28.182	0.008	19.868	14	8318.112	28518.36	0.721309	20200.25	2.201758
1200	28.182	0.008	19.868	16	8821.609	29178.31	0.733839	20356.7	2.21881
1200	28.182	0.008	19.868	18	9273.112	29721.79	0.743525	20448.68	2.228836
1200	28.182	0.008	19.868	20	9682.943	30179.45	0.751155	20496.51	2.234049
1200	28.182	0.008	19.868	22	10058.58	30570.99	0.757224	20512.41	2.235782
1200	28.182	0.008	19.868	24	10405.62	30911.07	0.762106	20505.46	2.235025
1400	28.182	0.004	19.868	2	1911.75	12951.32	0.310428	11039.57	1.252419
1400	28.182	0.004	19.868	4	4019.985	22005.38	0.522029	17985.39	2.040409
1400	28.182	0.004	19.868	6	5351.587	25939.27	0.609969	20587.68	2.335634
1400	28.182	0.004	19.868	8	6343.236	28246.12	0.659128	21902.88	2.484841
1400	28.182	0.004	19.868	10	7140.309	29799.39	0.690603	22659.08	2.57063
1400	28.182	0.004	19.868	12	7810.211	30932.77	0.712384	23122.56	2.623211
1400	28.182	0.004	19.868	14	8390.012	31805.03	0.728241	23415.02	2.65639
1400	28.182	0.004	19.868	16	8902.391	32501.34	0.74017	23598.94	2.677256
1400	28.182	0.004	19.868	18	9362.289	33073.94	0.749394	23711.65	2.690042
1400	28.182	0.004	19.868	20	9780.093	33554.28	0.756629	23774.19	2.697138
1400	28.182	0.004	19.868	22	10163.33	33965.17	0.762403	23801.85	2.700275
1400	28.182	0.004	19.868	24	10517.64	34320.95	0.767031	23803.31	2.700442
1400	28.182	0.005	19.868	2	1910.77	13030.18	0.304248	11119.41	1.248727
1400	28.182	0.005	19.868	4	4015.632	22243.6	0.514343	18227.97	2.047028
1400	28.182	0.005	19.868	6	5343.899	26277.31	0.602569	20933.41	2.350854
1400	28.182	0.005	19.868	8	6332.464	28651.91	0.652235	22319.45	2.506508
1400	28.182	0.005	19.868	10	7126.69	30254.9	0.684227	23128.21	2.597333
1400	28.182	0.005	19.868	12	7793.946	31426.69	0.706493	23632.75	2.653993
1400	28.182	0.005	19.868	14	8371.27	32330.17	0.72281	23958.9	2.690621
1400	28.182	0.005	19.868	16	8881.321	33051.52	0.735138	24170.2	2.71435
1400	28.182	0.005	19.868	18	9339.015	33645.19	0.74473	24306.17	2.72962
1400	28.182	0.005	19.868	20	9754.723	34144.15	0.752324	24389.42	2.738969
1400	28.182	0.005	19.868	22	10135.96	34570.84	0.75842	24434.88	2.744074
1400	28.182	0.005	19.868	24	10488.36	34941.12	0.76337	24452.77	2.746082
1400	28.182	0.006	19.868	2	1909.812	13104.43	0.29827	11194.62	1.244594
1400	28.182	0.006	19.868	4	4011.383	22471.54	0.506788	18460.15	2.05236
1400	28.182	0.006	19.868	6	5336.406	26603.28	0.595237	21266.88	2.364405
1400	28.182	0.006	19.868	8	6321.974	29045.1	0.645366	22723.13	2.526308
1400	28.182	0.006	19.868	10	7113.437	30697.74	0.677844	23584.31	2.622052
1400	28.182	0.006	19.868	12	7778.128	31908.09	0.700571	24129.96	2.682717
1400	28.182	0.006	19.868	14	8353.056	32841.91	0.717292	24488.85	2.722617

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1400	28.182	0.006	19.868	16	8860.851	33589.8	0.730039	24728.95	2.749311
1400	28.182	0.006	19.868	18	9316.414	34204.99	0.73999	24888.57	2.767057
1400	28.182	0.006	19.868	20	9730.099	34722.74	0.747926	24992.64	2.778627
1400	28.182	0.006	19.868	22	10109.41	35165.44	0.754329	25056.04	2.785675
1400	28.182	0.006	19.868	24	10459.95	35549.83	0.759567	25089.88	2.789438
1400	28.182	0.007	19.868	2	1908.874	13174.43	0.292486	11265.55	1.240072
1400	28.182	0.007	19.868	4	4007.234	22689.65	0.499367	18682.42	2.056493
1400	28.182	0.007	19.868	6	5329.098	26917.56	0.587978	21588.46	2.37638
1400	28.182	0.007	19.868	8	6311.755	29425.95	0.638526	23114.19	2.544327
1400	28.182	0.007	19.868	10	7100.535	31128.09	0.671458	24027.56	2.644867
1400	28.182	0.007	19.868	12	7762.739	32377.07	0.694621	24614.33	2.709457
1400	28.182	0.007	19.868	14	8335.344	33342.1	0.711749	25006.76	2.752653
1400	28.182	0.007	19.868	16	8840.956	34116.24	0.724882	25275.29	2.782213
1400	28.182	0.007	19.868	18	9294.456	34753.06	0.735172	25458.61	2.802392
1400	28.182	0.007	19.868	20	9706.183	35289.45	0.743424	25583.26	2.816113
1400	28.182	0.007	19.868	22	10083.62	35749.15	0.750145	25665.52	2.825168
1400	28.182	0.007	19.868	24	10432.39	36147.66	0.755653	25715.27	2.830645
1400	28.182	0.008	19.868	2	1907.955	13240.49	0.28689	11332.53	1.235207
1400	28.182	0.008	19.868	4	4003.182	22898.41	0.492082	18895.23	2.059515
1400	28.182	0.008	19.868	6	5321.97	27220.51	0.580795	21898.54	2.386866
1400	28.182	0.008	19.868	8	6301.795	29794.73	0.631722	23492.93	2.560649
1400	28.182	0.008	19.868	10	7087.969	31546.14	0.665077	24458.18	2.665857
1400	28.182	0.008	19.868	12	7747.759	32833.75	0.688651	25085.99	2.734287
1400	28.182	0.008	19.868	14	8318.112	33830.11	0.706165	25512	2.780721
1400	28.182	0.008	19.868	16	8821.609	34629.72	0.71964	25808.11	2.812996
1400	28.182	0.008	19.868	18	9273.112	35289.47	0.730286	26016.36	2.835694
1400	28.182	0.008	19.868	20	9682.943	35844.79	0.738843	26161.85	2.851552
1400	28.182	0.008	19.868	22	10058.58	36320.8	0.745843	26262.22	2.862493
1400	28.182	0.008	19.868	24	10405.62	36734.42	0.751632	26328.8	2.869749
1600	28.182	0.004	19.868	2	1911.75	14853.74	0.302675	12941.99	1.468244
1600	28.182	0.004	19.868	4	4019.985	25306.05	0.511082	21286.07	2.414865
1600	28.182	0.004	19.868	6	5351.587	29868.54	0.598731	24516.96	2.781403
1600	28.182	0.004	19.868	8	6343.236	32548.33	0.648219	26205.09	2.972919
1600	28.182	0.004	19.868	10	7140.309	34355.75	0.680271	27215.45	3.087542
1600	28.182	0.004	19.868	12	7810.211	35676.06	0.702721	27865.85	3.161329
1600	28.182	0.004	19.868	14	8390.012	36692.69	0.719272	28302.67	3.210886
1600	28.182	0.004	19.868	16	8902.391	37505.32	0.731919	28602.93	3.244949
1600	28.182	0.004	19.868	18	9362.289	38173.75	0.74185	28811.46	3.268607
1600	28.182	0.004	19.868	20	9780.093	38734.61	0.749779	28954.52	3.284836
1600	28.182	0.004	19.868	22	10163.33	39214.31	0.756226	29050.98	3.29578
1600	28.182	0.004	19.868	24	10517.64	39630.28	0.761528	29112.65	3.302776

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1600	28.182	0.005	19.868	2	1910.77	14952.81	0.296012	13042.04	1.464641
1600	28.182	0.005	19.868	4	4015.632	25608.5	0.502728	21592.87	2.424911
1600	28.182	0.005	19.868	6	5343.899	30298.11	0.590601	24954.21	2.802396
1600	28.182	0.005	19.868	8	6332.464	33067.81	0.640644	26735.35	3.00242
1600	28.182	0.005	19.868	10	7126.69	34940.08	0.67322	27813.39	3.123486
1600	28.182	0.005	19.868	12	7793.946	36310.67	0.696162	28516.73	3.202471
1600	28.182	0.005	19.868	14	8371.27	37367.72	0.713163	28996.45	3.256345
1600	28.182	0.005	19.868	16	8881.321	38213.76	0.726222	29332.44	3.294077
1600	28.182	0.005	19.868	18	9339.015	38909.98	0.73652	29570.97	3.320864
1600	28.182	0.005	19.868	20	9754.723	39495.65	0.744812	29740.92	3.33995
1600	28.182	0.005	19.868	22	10135.96	39996.25	0.751578	29860.28	3.353355
1600	28.182	0.005	19.868	24	10488.36	40430.75	0.757179	29942.39	3.362575
1600	28.182	0.006	19.868	2	1909.812	15045.39	0.289587	13135.57	1.460384
1600	28.182	0.006	19.868	4	4011.383	25896.09	0.49453	21884.71	2.433094
1600	28.182	0.006	19.868	6	5336.406	30711.69	0.582587	25375.28	2.821168
1600	28.182	0.006	19.868	8	6321.974	33568.78	0.633095	27246.8	3.02924
1600	28.182	0.006	19.868	10	7113.437	35505.69	0.666158	28392.26	3.156589
1600	28.182	0.006	19.868	12	7778.128	36926.69	0.689563	29148.57	3.240674
1600	28.182	0.006	19.868	14	8353.056	38024.45	0.706992	29671.4	3.298801
1600	28.182	0.006	19.868	16	8860.851	38904.25	0.720444	30043.4	3.34016
1600	28.182	0.006	19.868	18	9316.414	39629.04	0.731104	30312.63	3.370092
1600	28.182	0.006	19.868	20	9730.099	40239.78	0.739741	30509.68	3.391999
1600	28.182	0.006	19.868	22	10109.41	40761.48	0.746808	30652.08	3.407831
1600	28.182	0.006	19.868	24	10459.95	41214.79	0.752695	30754.83	3.419255
1600	28.182	0.007	19.868	2	1908.874	15132.02	0.283393	13223.15	1.455557
1600	28.182	0.007	19.868	4	4007.234	26169.62	0.486489	22162.38	2.439555
1600	28.182	0.007	19.868	6	5329.098	31108.26	0.574657	25779.16	2.837677
1600	28.182	0.007	19.868	8	6311.755	34051.68	0.625578	27739.93	3.053511
1600	28.182	0.007	19.868	10	7100.535	36052.91	0.659091	28952.37	3.186973
1600	28.182	0.007	19.868	12	7762.739	37524.34	0.682931	29761.6	3.276049
1600	28.182	0.007	19.868	14	8335.344	38663	0.700767	30327.65	3.338359
1600	28.182	0.007	19.868	16	8840.956	39576.83	0.714593	30735.87	3.383294
1600	28.182	0.007	19.868	18	9294.456	40330.51	0.725599	31036.05	3.416337
1600	28.182	0.007	19.868	20	9706.183	40965.44	0.734538	31259.26	3.440906
1600	28.182	0.007	19.868	22	10083.62	41510.04	0.74193	31426.41	3.459306
1600	28.182	0.007	19.868	24	10432.39	41982.33	0.748088	31549.94	3.472904
1600	28.182	0.008	19.868	2	1907.955	15213.23	0.277421	13305.27	1.450229
1600	28.182	0.008	19.868	4	4003.182	26429.85	0.47861	22426.66	2.44443
1600	28.182	0.008	19.868	6	5321.97	31488.49	0.566819	26166.52	2.852061
1600	28.182	0.008	19.868	8	6301.795	34517.02	0.618103	28215.23	3.075363
1600	28.182	0.008	19.868	10	7087.969	36582.09	0.65203	29494.12	3.214758
1600	28.182	0.008	19.868	12	7747.759	38103.85	0.676277	30356.09	3.30871
1600	28.182	0.008	19.868	14	8318.112	39283.51	0.694496	30965.4	3.375123

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1600	28.182	0.008	19.868	16	8821.609	40231.58	0.708678	31409.97	3.423579
1600	28.182	0.008	19.868	18	9273.112	41014.41	0.720014	31741.29	3.459692
1600	28.182	0.008	19.868	20	9682.943	41674.54	0.72926	31991.6	3.486975
1600	28.182	0.008	19.868	22	10058.58	42240.67	0.736924	32182.09	3.507738
1600	28.182	0.008	19.868	24	10405.62	42733.38	0.743369	32327.77	3.523616
1800	28.182	0.004	19.868	2	1911.75	16767.27	0.29638	14855.52	1.685331
1800	28.182	0.004	19.868	4	4019.985	28641.59	0.502341	24621.6	2.793275
1800	28.182	0.004	19.868	6	5351.587	33845.35	0.589776	28493.76	3.232564
1800	28.182	0.004	19.868	8	6343.236	36912.64	0.639649	30569.4	3.468042
1800	28.182	0.004	19.868	10	7140.309	38981.84	0.672168	31841.53	3.612363
1800	28.182	0.004	19.868	12	7810.211	40495.25	0.695148	32685.04	3.708057
1800	28.182	0.004	19.868	14	8390.012	41661.58	0.712245	33271.57	3.774598
1800	28.182	0.004	19.868	16	8902.391	42594.52	0.725435	33692.13	3.822309
1800	28.182	0.004	19.868	18	9362.289	43361.84	0.73589	33999.55	3.857186
1800	28.182	0.004	19.868	20	9780.093	44006.76	0.744348	34226.67	3.882952
1800	28.182	0.004	19.868	22	10163.33	44559.06	0.751321	34395.73	3.902131
1800	28.182	0.004	19.868	24	10517.64	45036.84	0.757102	34519.2	3.916139
1800	28.182	0.005	19.868	2	1910.77	16887.93	0.289237	14977.16	1.681958
1800	28.182	0.005	19.868	4	4015.632	29013.68	0.493312	24998.05	2.807318
1800	28.182	0.005	19.868	6	5343.899	34378.45	0.580984	29034.55	3.260624
1800	28.182	0.005	19.868	8	6332.464	37555.36	0.631346	31222.89	3.506378
1800	28.182	0.005	19.868	10	7126.69	39708.13	0.664433	32581.44	3.658945
1800	28.182	0.005	19.868	12	7793.946	41285.22	0.687914	33491.27	3.76112
1800	28.182	0.005	19.868	14	8371.27	42502.9	0.70547	34131.63	3.833034
1800	28.182	0.005	19.868	16	8881.321	43478.36	0.719079	34597.04	3.8853
1800	28.182	0.005	19.868	18	9339.015	44281.64	0.729916	34942.63	3.92411
1800	28.182	0.005	19.868	20	9754.723	44957.48	0.738726	35202.75	3.953322
1800	28.182	0.005	19.868	22	10135.96	45535.93	0.746006	35399.97	3.97547
1800	28.182	0.005	19.868	24	10488.36	46038.8	0.752117	35550.44	3.992368
1800	28.182	0.006	19.868	2	1909.812	16999.85	0.282373	15090.04	1.677678
1800	28.182	0.006	19.868	4	4011.383	29365.33	0.484464	25353.95	2.818797
1800	28.182	0.006	19.868	6	5336.406	34887.01	0.57228	29550.61	3.285372
1800	28.182	0.006	19.868	8	6321.974	38173.42	0.623098	31851.44	3.541174
1800	28.182	0.006	19.868	10	7113.437	40408.08	0.656682	33294.64	3.701626
1800	28.182	0.006	19.868	12	7778.128	42048.92	0.680631	34270.79	3.810152
1800	28.182	0.006	19.868	14	8353.056	43318.27	0.698621	34965.21	3.887356
1800	28.182	0.006	19.868	16	8860.851	44336.68	0.712629	35475.83	3.944125
1800	28.182	0.006	19.868	18	9316.414	45176.4	0.723832	35859.99	3.986835
1800	28.182	0.006	19.868	20	9730.099	45883.65	0.732979	36153.55	4.019473
1800	28.182	0.006	19.868	22	10109.41	46489.54	0.74057	36380.14	4.044664
1800	28.182	0.006	19.868	24	10459.95	47015.89	0.746954	36555.93	4.064209

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1800	28.182	0.007	19.868	2	1908.874	17103.86	0.275779	15194.99	1.672609
1800	28.182	0.007	19.868	4	4007.234	29697.78	0.475803	25690.54	2.827922
1800	28.182	0.007	19.868	6	5329.098	35372.06	0.563675	30042.97	3.307021
1800	28.182	0.007	19.868	8	6311.755	38766.25	0.614888	32454.5	3.572474
1800	28.182	0.007	19.868	10	7100.535	41082.23	0.648926	33981.7	3.740583
1800	28.182	0.007	19.868	12	7762.739	42786.73	0.673312	35023.99	3.855315
1800	28.182	0.007	19.868	14	8335.344	44107.91	0.69171	35772.57	3.937715
1800	28.182	0.007	19.868	16	8840.956	45169.59	0.706096	36328.63	3.998925
1800	28.182	0.007	19.868	18	9294.456	46046.13	0.717647	36751.67	4.045492
1800	28.182	0.007	19.868	20	9706.183	46785.21	0.727116	37079.03	4.081526
1800	28.182	0.007	19.868	22	10083.62	47418.98	0.735006	37335.36	4.109742
1800	28.182	0.007	19.868	24	10432.39	47970	0.741668	37537.62	4.132005
1800	28.182	0.008	19.868	2	1907.955	17200.71	0.269443	15292.75	1.666857
1800	28.182	0.008	19.868	4	4003.182	30012.22	0.467334	26009.03	2.834896
1800	28.182	0.008	19.868	6	5321.97	35834.65	0.55518	30512.68	3.325778
1800	28.182	0.008	19.868	8	6301.795	39334.69	0.606728	33032.9	3.600473
1800	28.182	0.008	19.868	10	7087.969	41731.22	0.641179	34643.25	3.775996
1800	28.182	0.008	19.868	12	7747.759	43499.11	0.665968	35751.35	3.896774
1800	28.182	0.008	19.868	14	8318.112	44872.14	0.684749	36554.03	3.984264
1800	28.182	0.008	19.868	16	8821.609	45977.28	0.699492	37155.67	4.049841
1800	28.182	0.008	19.868	18	9273.112	46890.92	0.711374	37617.81	4.100213
1800	28.182	0.008	19.868	20	9682.943	47662.18	0.721151	37979.23	4.139607
1800	28.182	0.008	19.868	22	10058.58	48324.19	0.729326	38265.61	4.170821
1800	28.182	0.008	19.868	24	10405.62	48900.27	0.736255	38494.65	4.195785
2000	28.182	0.004	19.868	2	1911.75	18691.41	0.291029	16779.66	1.903621
2000	28.182	0.004	19.868	4	4019.985	32010.65	0.495	27990.66	3.175489
2000	28.182	0.004	19.868	6	5351.587	37872.64	0.582336	32521.06	3.689453
2000	28.182	0.004	19.868	8	6343.236	41334.23	0.632474	34990.99	3.969663
2000	28.182	0.004	19.868	10	7140.309	43676.35	0.665447	36536.04	4.144946
2000	28.182	0.004	19.868	12	7810.211	45388.8	0.68886	37578.59	4.263221
2000	28.182	0.004	19.868	14	8390.012	46709.82	0.706398	38319.81	4.347311
2000	28.182	0.004	19.868	16	8902.391	47767.26	0.720026	38864.87	4.409148
2000	28.182	0.004	19.868	18	9362.289	48637.5	0.730905	39275.21	4.455699
2000	28.182	0.004	19.868	20	9780.093	49369.26	0.739775	39589.16	4.491317
2000	28.182	0.004	19.868	22	10163.33	49995.27	0.747128	39831.94	4.51886
2000	28.182	0.004	19.868	24	10517.64	50538.43	0.753305	40020.8	4.540285
2000	28.182	0.005	19.868	2	1910.77	18834.81	0.283415	16924.04	1.900595
2000	28.182	0.005	19.868	4	4015.632	32457.22	0.485294	28441.59	3.194034
2000	28.182	0.005	19.868	6	5343.899	38515.5	0.572834	33171.6	3.725221
2000	28.182	0.005	19.868	8	6332.464	42113.2	0.623493	35780.74	4.018231
2000	28.182	0.005	19.868	10	7126.69	44555.06	0.656989	37428.37	4.203263
2000	28.182	0.005	19.868	12	7793.946	46347.97	0.680946	38554.02	4.329675

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
2000	28.182	0.005	19.868	14	8371.27	47732.52	0.698954	39361.25	4.420328
2000	28.182	0.005	19.868	16	8881.321	48842.71	0.71301	39961.39	4.487724
2000	28.182	0.005	19.868	18	9339.015	49757.62	0.724281	40418.6	4.53907
2000	28.182	0.005	19.868	20	9754.723	50527.85	0.73351	40773.13	4.578884
2000	28.182	0.005	19.868	22	10135.96	51187.44	0.741193	41051.48	4.610143
2000	28.182	0.005	19.868	24	10488.36	51760.23	0.747676	41271.87	4.634894
2000	28.182	0.006	19.868	2	1909.812	18966.87	0.276124	17057.06	1.896367
2000	28.182	0.006	19.868	4	4011.383	32876.71	0.475799	28865.33	3.209184
2000	28.182	0.006	19.868	6	5336.406	39125.48	0.563436	33789.07	3.756595
2000	28.182	0.006	19.868	8	6321.974	42857.1	0.614542	36535.13	4.061896
2000	28.182	0.006	19.868	10	7113.437	45399.36	0.648536	38285.92	4.256545
2000	28.182	0.006	19.868	12	7778.128	47271.42	0.672976	39493.29	4.390778
2000	28.182	0.006	19.868	14	8353.056	48719.81	0.691425	40366.76	4.487888
2000	28.182	0.006	19.868	16	8860.851	49883.23	0.705886	41022.38	4.560778
2000	28.182	0.006	19.868	18	9316.414	50843.4	0.71753	41526.99	4.61688
2000	28.182	0.006	19.868	20	9730.099	51652.73	0.727101	41922.63	4.660866
2000	28.182	0.006	19.868	22	10109.41	52346.53	0.735101	42237.12	4.695831
2000	28.182	0.006	19.868	24	10459.95	52949.57	0.741878	42489.62	4.723903
2000	28.182	0.007	19.868	2	1908.874	19088.79	0.269145	17179.91	1.891103
2000	28.182	0.007	19.868	4	4007.234	33270.95	0.466524	29263.72	3.221244
2000	28.182	0.007	19.868	6	5329.098	39704.16	0.554156	34375.06	3.783883
2000	28.182	0.007	19.868	8	6311.755	43567.15	0.605639	37255.4	4.10094
2000	28.182	0.007	19.868	10	7100.535	46208.78	0.640079	39108.25	4.304895
2000	28.182	0.007	19.868	12	7762.739	48159.79	0.664966	40397.05	4.446762
2000	28.182	0.007	19.868	14	8335.344	49672.13	0.683827	41336.78	4.550204
2000	28.182	0.007	19.868	16	8840.956	50889.08	0.69867	42048.12	4.628506
2000	28.182	0.007	19.868	18	9294.456	51894.94	0.710667	42600.49	4.689308
2000	28.182	0.007	19.868	20	9706.183	52743.86	0.720565	43037.68	4.737432
2000	28.182	0.007	19.868	22	10083.62	53472.39	0.728867	43388.77	4.776079
2000	28.182	0.007	19.868	24	10432.39	54106.24	0.735926	43673.86	4.807461
2000	28.182	0.008	19.868	2	1907.955	19201.59	0.262462	17293.63	1.884947
2000	28.182	0.008	19.868	4	4003.182	33641.7	0.457475	29638.52	3.230497
2000	28.182	0.008	19.868	6	5321.97	40253.13	0.545007	34931.16	3.807377
2000	28.182	0.008	19.868	8	6301.795	44244.64	0.596798	37942.85	4.135641
2000	28.182	0.008	19.868	10	7087.969	46984.33	0.631635	39896.36	4.348567
2000	28.182	0.008	19.868	12	7747.759	49011.88	0.656901	41264.12	4.497648
2000	28.182	0.008	19.868	14	8318.112	50590.01	0.676176	42271.9	4.607492
2000	28.182	0.008	19.868	16	8821.609	51860.64	0.691377	43039.03	4.691107
2000	28.182	0.008	19.868	18	9273.112	52912.47	0.703707	43639.36	4.756541
2000	28.182	0.008	19.868	20	9682.943	53801.35	0.713915	44118.4	4.808755
2000	28.182	0.008	19.868	22	10058.58	54565.04	0.722506	44506.46	4.851052
2000	28.182	0.008	19.868	24	10405.62	55230.14	0.729833	44824.52	4.885719

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	28.182	0	19.868	2	1915.892	8986.785	0.357887	7070.893	0.836337
1000	28.182	0	19.868	4	4038.526	14957.02	0.585751	10918.49	1.291426
1000	28.182	0	19.868	6	5384.448	17471.5	0.674058	12087.05	1.429642
1000	28.182	0	19.868	8	6389.404	18923.21	0.720216	12533.81	1.482484
1000	28.182	0	19.868	10	7198.81	19892.16	0.747686	12693.35	1.501354
1000	28.182	0	19.868	12	7880.199	20593.38	0.765015	12713.18	1.5037
1000	28.182	0	19.868	14	8470.777	21130.65	0.776328	12659.87	1.497395
1000	28.182	0	19.868	16	8993.317	21558.27	0.783724	12564.95	1.486167
1000	28.182	0	19.868	18	9462.846	21908.19	0.788417	12445.34	1.47202
1000	28.182	0	19.868	20	9889.819	22201.4	0.791206	12311.58	1.456199
1000	28.182	0	19.868	22	10281.81	22451.38	0.792589	12169.57	1.439402
1000	28.182	0	19.868	24	10644.52	22667.66	0.79291	12023.14	1.422083
1000	29.182	0	20.868	2	1912.505	9045.742	0.348032	7133.237	0.814799
1000	29.182	0	20.868	4	4023.935	15139.97	0.573445	11116.03	1.269736
1000	29.182	0	20.868	6	5359.076	17735.66	0.662489	12376.58	1.413724
1000	29.182	0	20.868	8	6354.239	19245.65	0.70995	12891.41	1.47253
1000	29.182	0	20.868	10	7154.727	20257.95	0.738756	13103.23	1.496725
1000	29.182	0	20.868	12	7827.927	20994.41	0.757453	13166.48	1.50395
1000	29.182	0	20.868	14	8410.903	21560.21	0.770058	13149.3	1.501988
1000	29.182	0	20.868	16	8926.351	22011.76	0.778687	13085.41	1.494689
1000	29.182	0	20.868	18	9389.209	22382.65	0.784588	12993.44	1.484184
1000	29.182	0	20.868	20	9809.882	22693.6	0.788505	12883.72	1.471651
1000	29.182	0	20.868	22	10195.9	22959.45	0.790985	12763.55	1.457925
1000	29.182	0	20.868	24	10552.91	23189.86	0.792367	12636.95	1.443464
1000	30.182	0	21.868	2	1909.346	9101.277	0.338692	7191.931	0.794285
1000	30.182	0	21.868	4	4010.366	15313.7	0.561554	11303.33	1.248352
1000	30.182	0	21.868	6	5335.517	17988.03	0.651144	12652.52	1.397358
1000	30.182	0	21.868	8	6321.634	19554.12	0.69968	13232.49	1.46141
1000	30.182	0	21.868	10	7113.883	20608.98	0.729653	13495.1	1.490414
1000	30.182	0	21.868	12	7779.522	21379.59	0.749527	13600.07	1.502007
1000	30.182	0	21.868	14	8355.492	21973.41	0.763262	13617.92	1.503978
1000	30.182	0	21.868	16	8864.396	22448.58	0.772975	13584.19	1.500253
1000	30.182	0	21.868	18	9321.117	22839.71	0.779911	13518.6	1.493009
1000	30.182	0	21.868	20	9735.988	23168.85	0.784851	13432.86	1.48354
1000	30.182	0	21.868	22	10116.51	23450.16	0.788279	13333.65	1.472583
1000	30.182	0	21.868	24	10468.27	23694.62	0.790588	13226.34	1.460732
1000	31.182	0	22.868	2	1906.399	9153.675	0.329829	7247.276	0.774729
1000	31.182	0	22.868	4	3997.723	15478.88	0.550071	11481.15	1.227327
1000	31.182	0	22.868	6	5313.599	18228.97	0.640022	12915.37	1.380644
1000	31.182	0	22.868	8	6291.311	19849.51	0.689459	13558.2	1.449362
1000	31.182	0	22.868	10	7075.932	20945.87	0.72044	13869.94	1.482686
1000	31.182	0	22.868	12	7734.567	21750.02	0.741347	14015.45	1.498242
1000	31.182	0	22.868	14	8304.058	22371.07	0.756061	14067.01	1.503754

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1000	31.182	0	22.868	16	8806.925	22869.5	0.766729	14062.57	1.503279
1000	31.182	0	22.868	18	9257.968	23280.64	0.774579	14022.67	1.499014
1000	31.182	0	22.868	20	9667.486	23627.21	0.780394	13959.73	1.492285
1000	31.182	0	22.868	22	10042.92	23924.5	0.784693	13881.58	1.48393
1000	31.182	0	22.868	24	10389.86	24182.62	0.787804	13792.76	1.474436
1000	32.182	0	23.868	2	1903.642	9203.193	0.321408	7299.551	0.75607
1000	32.182	0	23.868	4	3985.905	15636.11	0.538982	11650.21	1.2067
1000	32.182	0	23.868	6	5293.148	18459.21	0.629137	13166.06	1.363709
1000	32.182	0	23.868	8	6263.05	20132.69	0.679328	13869.64	1.436583
1000	32.182	0	23.868	10	7040.574	21269.31	0.711171	14228.74	1.473778
1000	32.182	0	23.868	12	7692.721	22105.78	0.732957	14413.06	1.492869
1000	32.182	0	23.868	14	8256.202	22753.96	0.748554	14497.75	1.501642
1000	32.182	0	23.868	16	8753.449	23275.23	0.760065	14521.78	1.504131
1000	32.182	0	23.868	18	9199.247	23706.11	0.768724	14506.86	1.502585
1000	32.182	0	23.868	20	9603.793	24069.95	0.775315	14466.16	1.49837
1000	32.182	0	23.868	22	9974.53	24382.49	0.780357	14407.96	1.492342
1000	32.182	0	23.868	24	10316.99	24654.78	0.784212	14337.79	1.485073
1200	28.182	0	19.868	2	1915.892	10784.15	0.345198	8868.255	1.048927
1200	28.182	0	19.868	4	4038.526	17948.7	0.566071	13910.17	1.645279
1200	28.182	0	19.868	6	5384.448	20965.27	0.652878	15580.82	1.842881
1200	28.182	0	19.868	8	6389.404	22708.47	0.699312	16319.07	1.9302
1200	28.182	0	19.868	10	7198.81	23869.87	0.727679	16671.06	1.971833
1200	28.182	0	19.868	12	7880.199	24712.1	0.746384	16831.9	1.990857
1200	28.182	0	19.868	14	8470.777	25356.74	0.759246	16885.97	1.997252
1200	28.182	0	19.868	16	8993.317	25869.71	0.768317	16876.4	1.99612
1200	28.182	0	19.868	18	9462.846	26289.84	0.774784	16826.99	1.990276
1200	28.182	0	19.868	20	9889.819	26641.73	0.779392	16751.91	1.981396
1200	28.182	0	19.868	22	10281.81	26941.85	0.78263	16660.04	1.970529
1200	28.182	0	19.868	24	10644.52	27201.17	0.784811	16556.65	1.958301
1400	28.182	0	19.868	2	1915.892	12581.53	0.33727	10665.64	1.261519
1400	28.182	0	19.868	4	4038.526	20939.8	0.554027	16901.27	1.999063
1400	28.182	0	19.868	6	5384.448	24459.57	0.640151	19075.12	2.256183
1400	28.182	0	19.868	8	6389.404	26492.5	0.68684	20103.1	2.37777
1400	28.182	0	19.868	10	7198.81	27848.18	0.715924	20649.37	2.442382
1400	28.182	0	19.868	12	7880.199	28830.76	0.735512	20950.56	2.478007
1400	28.182	0	19.868	14	8470.777	29582.87	0.74936	21112.09	2.497113
1400	28.182	0	19.868	16	8993.317	30181.42	0.759472	21188.1	2.506104
1400	28.182	0	19.868	18	9462.846	30671.46	0.767001	21208.62	2.50853
1400	28.182	0	19.868	20	9889.819	31081.95	0.772685	21192.14	2.50658
1400	28.182	0	19.868	22	10281.81	31431.94	0.776998	21150.12	2.501611
1400	28.182	0	19.868	24	10644.52	31734.72	0.780269	21090.2	2.494524

TIT	a	k₁	b	r_p	W_c	W_t	eth	W_n	W_s
1600	28.182	0	19.868	2	1915.892	14378.97	0.331849	12463.08	1.474118
1600	28.182	0	19.868	4	4038.526	23931.2	0.545913	19892.68	2.352882
1600	28.182	0	19.868	6	5384.448	27954.23	0.63166	22569.78	2.669527
1600	28.182	0	19.868	8	6389.404	30277.19	0.678592	23887.78	2.825419
1600	28.182	0	19.868	10	7198.81	31826.49	0.70818	24627.68	2.912933
1600	28.182	0	19.868	12	7880.199	32949.41	0.728388	25069.21	2.965156
1600	28.182	0	19.868	14	8470.777	33809.17	0.742919	25338.4	2.996995
1600	28.182	0	19.868	16	8993.317	34492.95	0.753724	25499.64	3.016066
1600	28.182	0	19.868	18	9462.846	35053.1	0.761969	25590.26	3.026785
1600	28.182	0	19.868	20	9889.819	35522.31	0.768368	25632.49	3.031781
1600	28.182	0	19.868	22	10281.81	35922.74	0.773404	25640.93	3.032778
1600	28.182	0	19.868	24	10644.52	36268.23	0.77736	25623.71	3.030742
1800	28.182	0	19.868	2	1915.892	16176.56	0.32791	14260.66	1.686734
1800	28.182	0	19.868	4	4038.526	26922.61	0.540071	22884.08	2.706702
1800	28.182	0	19.868	6	5384.448	31447.9	0.625563	26063.45	3.082754
1800	28.182	0	19.868	8	6389.404	34062.06	0.672727	27672.66	3.273089
1800	28.182	0	19.868	10	7198.81	35804.84	0.702695	28606.03	3.383487
1800	28.182	0	19.868	12	7880.199	37068.09	0.72336	29187.89	3.452309
1800	28.182	0	19.868	14	8470.777	38035.12	0.738378	29564.34	3.496835
1800	28.182	0	19.868	16	8993.317	38805.13	0.749708	29811.82	3.526106
1800	28.182	0	19.868	18	9462.846	39434.79	0.758448	29971.95	3.545046
1800	28.182	0	19.868	20	9889.819	39962.51	0.76535	30072.69	3.556962
1800	28.182	0	19.868	22	10281.81	40412.49	0.770873	30130.67	3.56382
1800	28.182	0	19.868	24	10644.52	40801.81	0.775341	30157.29	3.566968
1800	29.182	0	20.868	2	1912.505	16282.74	0.318841	14370.23	1.641449
1800	29.182	0	20.868	4	4023.935	27251.9	0.528401	23227.96	2.653229
1800	29.182	0	20.868	6	5359.076	31924.19	0.614133	26565.11	3.034418
1800	29.182	0	20.868	8	6354.239	34642.67	0.661988	28288.43	3.231264
1800	29.182	0	20.868	10	7154.727	36464.14	0.692711	29309.41	3.347887
1800	29.182	0	20.868	12	7827.927	37789.95	0.714115	29962.03	3.422432
1800	29.182	0	20.868	14	8410.903	38808.36	0.72983	30397.46	3.47217
1800	29.182	0	20.868	16	8926.351	39621.07	0.741799	30694.72	3.506124
1800	29.182	0	20.868	18	9389.209	40288.79	0.751172	30899.59	3.529526
1800	29.182	0	20.868	20	9809.882	40848.53	0.758636	31038.65	3.545411
1800	29.182	0	20.868	22	10195.9	41327.01	0.764693	31131.11	3.555971
1800	29.182	0	20.868	24	10552.91	41741.75	0.769664	31188.84	3.562566
2000	28.182	0	19.868	2	1915.892	17974.39	0.324922	16058.5	1.89938

TIT	a	k ₁	b	r _p	W _c	W _t	eth	W _n	W _s
2000	28.182	0	19.868	4	4038.526	29914.02	0.535665	25875.49	3.060522
2000	28.182	0	19.868	6	5384.448	34942.11	0.620998	29557.67	3.496045
2000	28.182	0	19.868	8	6389.404	37847.4	0.668351	31458	3.720814
2000	28.182	0	19.868	10	7198.81	39783.31	0.698607	32584.5	3.854056
2000	28.182	0	19.868	12	7880.199	41186.8	0.719622	33306.6	3.939465
2000	28.182	0	19.868	14	8470.777	42261.24	0.735012	33790.47	3.996696
2000	28.182	0	19.868	16	8993.317	43116.19	0.74671	34122.87	4.036013
2000	28.182	0	19.868	18	9462.846	43816.38	0.755845	34353.53	4.063295
2000	28.182	0	19.868	20	9889.819	44403.06	0.763132	34513.24	4.082185
2000	28.182	0	19.868	22	10281.81	44902.79	0.769022	34620.97	4.094928
2000	28.182	0	19.868	24	10644.52	45335.29	0.773854	34690.77	4.103183

3.2.3 For the one reheat in expansion process

TIT	a	k ₁	b _v	r _p	W _c	W _t	eth	W _n	W _s
1000	28.182	0.004	19.868	2	2009.993	5235.931	0.138325	3225.938	0.365977
1000	28.182	0.004	19.868	4	4451.196	10018.83	0.239272	5567.635	0.631638
1000	28.182	0.004	19.868	6	6112.997	12620.8	0.284317	6507.806	0.738299
1000	28.182	0.004	19.868	8	7409.877	14383.94	0.31062	6974.065	0.791195
1000	28.182	0.004	19.868	10	8488.554	15705.8	0.327872	7217.248	0.818783
1000	28.182	0.004	19.868	12	9419.856	16756.99	0.339913	7337.136	0.832384
1000	28.182	0.004	19.868	14	10243.95	17625.97	0.348616	7382.022	0.837477
1000	28.182	0.004	19.868	16	10988.13	18364.34	0.354959	7376.208	0.836817
1000	28.182	0.004	19.868	18	11665.85	19004.73	0.359676	7338.88	0.832582
1000	28.182	0.004	19.868	20	12290.58	19569.04	0.363133	7278.458	0.825728
1000	28.182	0.004	19.868	22	12871.17	20072.68	0.365606	7201.504	0.816997
1000	28.182	0.004	19.868	24	13414.33	20526.84	0.367292	7112.518	0.806902
1000	28.182	0.005	19.868	2	2007.816	5242.772	0.135887	3234.956	0.36329
1000	28.182	0.005	19.868	4	4440.66	10044.19	0.235715	5603.535	0.629285
1000	28.182	0.005	19.868	6	6093.309	12661.32	0.280561	6568.016	0.737598
1000	28.182	0.005	19.868	8	7381.163	14436.82	0.306913	7055.654	0.792361
1000	28.182	0.005	19.868	10	8451.11	15769.06	0.324319	7317.949	0.821817
1000	28.182	0.005	19.868	12	9374.004	16829.2	0.33657	7455.194	0.83723
1000	28.182	0.005	19.868	14	10190	17706.05	0.345516	7516.043	0.844063
1000	28.182	0.005	19.868	16	10924.28	18451.43	0.352189	7527.15	0.84531
1000	28.182	0.005	19.868	18	11596.09	19098.16	0.357145	7502.069	0.842494
1000	28.182	0.005	19.868	20	12213.39	19668.25	0.360906	7454.858	0.837192
1000	28.182	0.005	19.868	22	12786.76	20177.2	0.363698	7390.438	0.829957
1000	28.182	0.005	19.868	24	13322.88	20636.28	0.365715	7313.398	0.821306
1000	28.182	0.006	19.868	2	2005.691	5249.241	0.13353	3243.55	0.360611
1000	28.182	0.006	19.868	4	4430.426	10068.28	0.232251	5637.853	0.626804
1000	28.182	0.006	19.868	6	6074.241	12699.89	0.276881	6625.648	0.736625

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	28.182	0.006	19.868	8	7353.416	14487.22	0.303259	7133.802	0.793121
1000	28.182	0.006	19.868	10	8414.993	15829.43	0.320794	7414.437	0.824321
1000	28.182	0.006	19.868	12	9329.845	16898.18	0.333227	7568.333	0.841431
1000	28.182	0.006	19.868	14	10138.11	17782.6	0.342389	7644.49	0.849898
1000	28.182	0.006	19.868	16	10864.94	18534.75	0.349299	7669.809	0.852713
1000	28.182	0.006	19.868	18	11529.19	19187.6	0.354521	7658.404	0.851445
1000	28.182	0.006	19.868	20	12139.45	19763.27	0.358554	7623.825	0.8476
1000	28.182	0.006	19.868	22	12705.98	20277.36	0.361628	7571.381	0.84177
1000	28.182	0.006	19.868	24	13235.45	20741.2	0.363937	7505.746	0.834472
1000	28.182	0.007	19.868	2	2003.617	5255.367	0.13125	3251.75	0.357941
1000	28.182	0.007	19.868	4	4420.478	10091.17	0.228875	5670.693	0.624209
1000	28.182	0.007	19.868	6	6055.761	12736.62	0.273276	6680.863	0.735405
1000	28.182	0.007	19.868	8	7326.583	14535.3	0.299661	7208.718	0.79351
1000	28.182	0.007	19.868	10	8380.125	15887.09	0.317302	7506.964	0.82634
1000	28.182	0.007	19.868	12	9287.273	16964.12	0.329893	7676.846	0.845039
1000	28.182	0.007	19.868	14	10088.15	17855.84	0.339245	7767.693	0.85504
1000	28.182	0.007	19.868	16	10807.87	18614.52	0.346366	7806.647	0.859328
1000	28.182	0.007	19.868	18	11463.33	19273.27	0.351871	7809.939	0.85969
1000	28.182	0.007	19.868	20	12068.52	19854.34	0.356098	7785.816	0.857035
1000	28.182	0.007	19.868	22	12628.56	20373.39	0.359423	7744.829	0.852523
1000	28.182	0.007	19.868	24	13151.73	20841.83	0.361993	7690.097	0.846498
1000	28.182	0.008	19.868	2	2001.591	5261.177	0.129045	3259.585	0.355284
1000	28.182	0.008	19.868	4	4410.805	10112.95	0.225587	5702.15	0.621515
1000	28.182	0.008	19.868	6	6037.84	12771.65	0.269746	6733.81	0.733962
1000	28.182	0.008	19.868	8	7300.614	14581.21	0.296119	7280.596	0.79356
1000	28.182	0.008	19.868	10	8346.437	15942.2	0.313846	7595.764	0.827912
1000	28.182	0.008	19.868	12	9246.198	17027.2	0.326575	7781.003	0.848103
1000	28.182	0.008	19.868	14	10040	17925.95	0.336094	7885.96	0.859543
1000	28.182	0.008	19.868	16	10752.93	18690.93	0.343403	7938.002	0.865215
1000	28.182	0.008	19.868	18	11401.85	19355.38	0.349109	7953.534	0.866908
1000	28.182	0.008	19.868	20	11998.66	19941.66	0.353608	7943.003	0.86576
1000	28.182	0.008	19.868	22	12554.28	20465.51	0.357109	7911.237	0.862298
1000	28.182	0.008	19.868	24	13071.46	20938.4	0.359911	7866.94	0.85747
1000	29.182	0.004	20.868	2	2003.364	5242.971	0.134597	3239.607	0.355431
1000	29.182	0.004	20.868	4	4421.283	10045.64	0.233846	5624.355	0.617071
1000	29.182	0.004	20.868	6	6059.402	12664.31	0.278624	6604.91	0.724652
1000	29.182	0.004	20.868	8	7334.036	14441.35	0.305048	7107.312	0.779772
1000	29.182	0.004	20.868	10	8391.957	15775.07	0.322585	7383.113	0.810031
1000	29.182	0.004	20.868	12	9303.828	16836.61	0.334996	7532.785	0.826453
1000	29.182	0.004	20.868	14	10109.64	17714.78	0.344122	7605.146	0.834392
1000	29.182	0.004	20.868	16	10834.44	18461.42	0.350986	7626.987	0.836788

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	29.182	0.004	20.868	18	11497.38	19109.34	0.356143	7611.965	0.83514
1000	29.182	0.004	20.868	20	12106.34	19680.57	0.360112	7574.228	0.830999
1000	29.182	0.004	20.868	22	12671.82	20190.59	0.363117	7518.768	0.824915
1000	29.182	0.004	20.868	24	13200.47	20650.7	0.365353	7450.234	0.817396
1000	29.182	0.005	20.868	2	2001.339	5249.423	0.132286	3248.084	0.352876
1000	29.182	0.005	20.868	4	4411.542	10069.61	0.23044	5658.07	0.6147
1000	29.182	0.005	20.868	6	6041.26	12702.66	0.274996	6661.396	0.723703
1000	29.182	0.005	20.868	8	7307.64	14491.43	0.301433	7183.785	0.780456
1000	29.182	0.005	20.868	10	8357.597	15835.02	0.319084	7477.422	0.812357
1000	29.182	0.005	20.868	12	9261.813	16905.08	0.331661	7643.267	0.830375
1000	29.182	0.005	20.868	14	10060.26	17790.74	0.340985	7730.482	0.83985
1000	29.182	0.005	20.868	16	10777.97	18544.07	0.348067	7766.105	0.84372
1000	29.182	0.005	20.868	18	11431.74	19198.04	0.353526	7766.299	0.843741
1000	29.182	0.005	20.868	20	12035.93	19774.78	0.35769	7738.845	0.840758
1000	29.182	0.005	20.868	22	12594.89	20289.87	0.360956	7694.985	0.835993
1000	29.182	0.005	20.868	24	13117.19	20754.68	0.363462	7637.496	0.829748
1000	29.182	0.006	20.868	2	1999.361	5255.535	0.130051	3256.173	0.35033
1000	29.182	0.006	20.868	4	4402.068	10092.41	0.227121	5690.338	0.61222
1000	29.182	0.006	20.868	6	6023.664	12739.19	0.27144	6715.528	0.722519
1000	29.182	0.006	20.868	8	7282.092	14539.21	0.297874	7257.121	0.780789
1000	29.182	0.006	20.868	10	8324.398	15892.29	0.315618	7567.895	0.814225
1000	29.182	0.006	20.868	12	9221.274	16970.55	0.328339	7749.278	0.83374
1000	29.182	0.006	20.868	14	10012.68	17863.44	0.337836	7850.76	0.844658
1000	29.182	0.006	20.868	16	10723.61	18623.22	0.345114	7899.614	0.849914
1000	29.182	0.006	20.868	18	11370.84	19283.02	0.350781	7912.178	0.851266
1000	29.182	0.006	20.868	20	11968.34	19865.09	0.355177	7896.756	0.849607
1000	29.182	0.006	20.868	22	12521.09	20385.1	0.358676	7864.004	0.846083
1000	29.182	0.006	20.868	24	13037.37	20854.45	0.361422	7817.082	0.841035
1000	29.182	0.007	20.868	2	1996.362	5261.331	0.127923	3264.969	0.347907
1000	29.182	0.007	20.868	4	4392.848	10114.1	0.223886	5721.251	0.609643
1000	29.182	0.007	20.868	6	6006.588	12774.04	0.267958	6767.45	0.721123
1000	29.182	0.007	20.868	8	7257.348	14584.85	0.294371	7327.504	0.780801
1000	29.182	0.007	20.868	10	8292.295	15947.05	0.312189	7654.757	0.815672
1000	29.182	0.007	20.868	12	9182.126	17033.2	0.325034	7851.077	0.836592
1000	29.182	0.007	20.868	14	9966.779	17933.05	0.334686	7966.271	0.848866
1000	29.182	0.007	20.868	16	10671.23	18699.06	0.342136	8027.838	0.855427
1000	29.182	0.007	20.868	18	11312.22	19364.5	0.34799	8052.282	0.858031
1000	29.182	0.007	20.868	20	11901.59	19951.73	0.352642	8050.136	0.857803
1000	29.182	0.007	20.868	22	12450.22	20476.48	0.356299	8026.253	0.855258
1000	29.182	0.007	20.868	24	12960.77	20950.23	0.359259	7989.455	0.851337
1000	29.182	0.008	20.868	2	1994.535	5266.835	0.125826	3272.3	0.345376
1000	29.182	0.008	20.868	4	4383.872	10134.77	0.220733	5750.896	0.60698

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	29.182	0.008	20.868	6	5990.006	12807.3	0.264549	6817.293	0.719534
1000	29.182	0.008	20.868	8	7233.366	14628.47	0.290926	7395.109	0.780519
1000	29.182	0.008	20.868	10	8261.229	15999.44	0.308802	7738.215	0.816733
1000	29.182	0.008	20.868	12	9144.291	17093.2	0.321753	7948.905	0.83897
1000	29.182	0.008	20.868	14	9922.467	17999.75	0.33154	8077.286	0.85252
1000	29.182	0.008	20.868	16	10620.7	18771.78	0.339143	8151.075	0.860308
1000	29.182	0.008	20.868	18	11255.72	19442.66	0.345164	8186.938	0.864093
1000	29.182	0.008	20.868	20	11839.34	20034.87	0.349992	8195.528	0.865
1000	29.182	0.008	20.868	22	12380.22	20564.21	0.353893	8183.984	0.863781
1000	29.182	0.008	20.868	24	12887.18	21042.22	0.356996	8155.039	0.860726
1000	30.182	0.004	21.868	2	1997.18	5249.606	0.131063	3252.426	0.345466
1000	30.182	0.004	21.868	4	4393.478	10070.94	0.228645	5677.46	0.603048
1000	30.182	0.004	21.868	6	6009.68	12705.4	0.273114	6695.721	0.711206
1000	30.182	0.004	21.868	8	7263.772	14495.59	0.299599	7231.819	0.768149
1000	30.182	0.004	21.868	10	8302.555	15840.55	0.317352	7537.994	0.800671
1000	30.182	0.004	21.868	12	9196.528	16911.9	0.330061	7715.374	0.819512
1000	30.182	0.004	21.868	14	9985.513	17798.79	0.339532	7813.277	0.829911
1000	30.182	0.004	21.868	16	10694.41	18553.28	0.346774	7858.866	0.834753
1000	30.182	0.004	21.868	18	11339.93	19208.34	0.3524	7868.407	0.835766
1000	30.182	0.004	21.868	20	11936.37	19786.13	0.356737	7849.755	0.833785
1000	30.182	0.004	21.868	22	12488	20302.22	0.360181	7814.222	0.830011
1000	30.182	0.004	21.868	24	13003.34	20767.98	0.362868	7764.64	0.824745
1000	30.182	0.005	21.868	2	1994.19	5255.703	0.128908	3261.513	0.343151
1000	30.182	0.005	21.868	4	4384.446	10093.63	0.22538	5709.187	0.600676
1000	30.182	0.005	21.868	6	5992.912	12741.74	0.269608	6748.828	0.710059
1000	30.182	0.005	21.868	8	7239.43	14543.09	0.296079	7303.658	0.768434
1000	30.182	0.005	21.868	10	8270.923	15897.44	0.313914	7626.521	0.802403
1000	30.182	0.005	21.868	12	9157.901	16976.91	0.326753	7819.013	0.822656
1000	30.182	0.005	21.868	14	9940.169	17870.95	0.336384	7930.779	0.834415
1000	30.182	0.005	21.868	16	10642.61	18631.82	0.343806	7989.216	0.840563
1000	30.182	0.005	21.868	18	11281.89	19292.65	0.349625	8010.76	0.84283
1000	30.182	0.005	21.868	20	11871.93	19875.71	0.354177	8003.785	0.842096
1000	30.182	0.005	21.868	22	12417.63	20396.65	0.357836	7979.024	0.839491
1000	30.182	0.005	21.868	24	12927.22	20866.91	0.360746	7939.688	0.835352
1000	30.182	0.006	21.868	2	1992.408	5261.486	0.126782	3269.078	0.340721
1000	30.182	0.006	21.868	4	4375.651	10115.24	0.222198	5739.587	0.59821
1000	30.182	0.006	21.868	6	5976.628	12776.41	0.266175	6799.778	0.708709
1000	30.182	0.006	21.868	8	7215.836	14588.46	0.292616	7372.626	0.768414
1000	30.182	0.006	21.868	10	8240.311	15951.86	0.310514	7711.545	0.803738
1000	30.182	0.006	21.868	12	9120.568	17039.14	0.323466	7918.574	0.825316
1000	30.182	0.006	21.868	14	9896.394	17940.07	0.333238	8043.673	0.838354

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	30.182	0.006	21.868	16	10592.64	18707.1	0.340819	8114.463	0.845732
1000	30.182	0.006	21.868	18	11225.97	19373.51	0.34681	8147.545	0.84918
1000	30.182	0.006	21.868	20	11808.14	19961.67	0.351603	8153.53	0.849804
1000	30.182	0.006	21.868	22	12349.99	20487.3	0.355405	8137.311	0.848114
1000	30.182	0.006	21.868	24	12854.1	20961.9	0.358514	8107.798	0.845038
1000	30.182	0.007	21.868	2	1990.662	5266.977	0.124723	3276.316	0.338302
1000	30.182	0.007	21.868	4	4367.083	10135.82	0.219096	5768.742	0.595661
1000	30.182	0.007	21.868	6	5960.804	12809.5	0.262812	6848.699	0.707174
1000	30.182	0.007	21.868	8	7192.952	14631.84	0.28921	7438.889	0.768115
1000	30.182	0.007	21.868	10	8210.665	16003.93	0.307156	7793.264	0.804707
1000	30.182	0.007	21.868	12	9084.46	17098.75	0.320203	8014.287	0.827529
1000	30.182	0.007	21.868	14	9854.099	18006.32	0.330099	8152.218	0.841771
1000	30.182	0.007	21.868	16	10544.41	18779.3	0.337821	8234.892	0.850308
1000	30.182	0.007	21.868	18	11172.03	19451.1	0.343967	8279.071	0.85487
1000	30.182	0.007	21.868	20	11748.69	20044.18	0.348923	8295.487	0.856565
1000	30.182	0.007	21.868	22	12283.02	20574.36	0.352956	8291.337	0.856136
1000	30.182	0.007	21.868	24	12783.79	21053.17	0.356193	8269.373	0.853868
1000	30.182	0.008	21.868	2	1988.951	5272.199	0.122728	3283.249	0.335896
1000	30.182	0.008	21.868	4	4358.732	10155.46	0.216072	5796.729	0.59304
1000	30.182	0.008	21.868	6	5945.42	12841.13	0.259519	6895.711	0.705472
1000	30.182	0.008	21.868	8	7170.743	14673.34	0.285861	7502.602	0.767561
1000	30.182	0.008	21.868	10	8181.936	16053.8	0.303842	7871.864	0.805339
1000	30.182	0.008	21.868	12	9049.509	17155.87	0.31697	8106.365	0.82933
1000	30.182	0.008	21.868	14	9813.203	18069.85	0.326974	8256.652	0.844705
1000	30.182	0.008	21.868	16	10497.82	18848.59	0.334822	8350.768	0.854333
1000	30.182	0.008	21.868	18	11119.96	19525.59	0.341105	8405.629	0.859946
1000	30.182	0.008	21.868	20	11691.36	20123.44	0.346208	8432.08	0.862652
1000	30.182	0.008	21.868	22	12220.59	20658	0.350394	8437.413	0.863198
1000	30.182	0.008	21.868	24	12714.18	21140.89	0.35385	8426.709	0.862103
1000	31.182	0.004	22.868	2	1990.327	5255.872	0.127744	3265.545	0.336148
1000	31.182	0.004	22.868	4	4367.566	10094.85	0.223655	5727.287	0.589555
1000	31.182	0.004	22.868	6	5963.431	12744.27	0.267782	6780.836	0.698005
1000	31.182	0.004	22.868	8	7198.501	14546.93	0.294279	7348.426	0.756431
1000	31.182	0.004	22.868	10	8219.587	15902.54	0.312194	7682.956	0.790867
1000	31.182	0.004	22.868	12	9097.027	16983.21	0.32514	7886.181	0.811786
1000	31.182	0.004	22.868	14	9870.483	17878.37	0.334894	8007.89	0.824315
1000	31.182	0.004	22.868	16	10564.72	18640.32	0.342449	8075.599	0.831285
1000	31.182	0.004	22.868	18	11196.33	19302.17	0.348407	8105.841	0.834398
1000	31.182	0.004	22.868	20	11779.13	19886.19	0.353105	8107.064	0.834524
1000	31.182	0.004	22.868	22	12318	20408.06	0.356913	8090.057	0.832773
1000	31.182	0.004	22.868	24	12821.11	20879.2	0.359975	8058.084	0.829482

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	31.182	0.005	22.868	2	1988.623	5261.641	0.125658	3273.018	0.333825
1000	31.182	0.005	22.868	4	4359.169	10116.37	0.220525	5757.2	0.587194
1000	31.182	0.005	22.868	6	5947.89	12778.76	0.264397	6830.866	0.6967
1000	31.182	0.005	22.868	8	7175.988	14592.04	0.290856	7416.051	0.756385
1000	31.182	0.005	22.868	10	8190.378	15956.61	0.308825	7766.235	0.792101
1000	31.182	0.005	22.868	12	9061.405	17045.02	0.321872	7983.616	0.814273
1000	31.182	0.005	22.868	14	9828.711	17947.01	0.331755	8118.298	0.828009
1000	31.182	0.005	22.868	16	10517.04	18715.05	0.339457	8198.016	0.83614
1000	31.182	0.005	22.868	18	11142.95	19382.42	0.345575	8239.468	0.840368
1000	31.182	0.005	22.868	20	11718.15	19971.48	0.350499	8253.338	0.841782
1000	31.182	0.005	22.868	22	12253.42	20497.99	0.354437	8244.568	0.840888
1000	31.182	0.005	22.868	24	12751.29	20973.43	0.357683	8222.132	0.838599
1000	31.182	0.006	22.868	2	1986.953	5267.121	0.123637	3280.168	0.331511
1000	31.182	0.006	22.868	4	4350.983	10136.88	0.217473	5785.892	0.584753
1000	31.182	0.006	22.868	6	5932.779	12811.69	0.261081	6878.914	0.695219
1000	31.182	0.006	22.868	8	7154.136	14635.18	0.28749	7481.042	0.756073
1000	31.182	0.006	22.868	10	8162.07	16008.37	0.305497	7846.303	0.792988
1000	31.182	0.006	22.868	12	9026.924	17104.24	0.318631	8077.319	0.816336
1000	31.182	0.006	22.868	14	9788.32	18012.81	0.328627	8224.493	0.83121
1000	31.182	0.006	22.868	16	10470.97	18786.75	0.336459	8315.774	0.840436
1000	31.182	0.006	22.868	18	11091.43	19459.45	0.342719	8368.016	0.845715
1000	31.182	0.006	22.868	20	11661.36	20053.39	0.347795	8392.023	0.848142
1000	31.182	0.006	22.868	22	12189.33	20584.38	0.351951	8395.052	0.848448
1000	31.182	0.006	22.868	24	12684.1	21063.98	0.355313	8379.881	0.846915
1000	31.182	0.007	22.868	2	1985.316	5272.332	0.121678	3287.016	0.329209
1000	31.182	0.007	22.868	4	4343.001	10156.44	0.214496	5813.438	0.58224
1000	31.182	0.007	22.868	6	5918.077	12843.17	0.257833	6925.095	0.693578
1000	31.182	0.007	22.868	8	7132.915	14676.46	0.28418	7543.547	0.755518
1000	31.182	0.007	22.868	10	8134.617	16057.95	0.302214	7923.338	0.793556
1000	31.182	0.007	22.868	12	8993.525	17161.02	0.315419	8167.494	0.818009
1000	31.182	0.007	22.868	14	9749.235	18075.94	0.325514	8326.705	0.833955
1000	31.182	0.007	22.868	16	10426.44	18855.56	0.333462	8429.125	0.844213
1000	31.182	0.007	22.868	18	11041.66	19533.42	0.33985	8491.76	0.850486
1000	31.182	0.007	22.868	20	11606.55	20132.08	0.345062	8525.528	0.853868
1000	31.182	0.007	22.868	22	12129.64	20667.42	0.349359	8537.776	0.855094
1000	31.182	0.007	22.868	24	12617.42	21151.05	0.352929	8533.634	0.85468
1000	31.182	0.008	22.868	2	1983.71	5277.293	0.119779	3293.583	0.326919
1000	31.182	0.008	22.868	4	4335.214	10175.12	0.211593	5839.907	0.579666
1000	31.182	0.008	22.868	6	5903.767	12873.28	0.254653	6969.517	0.691791
1000	31.182	0.008	22.868	8	7112.294	14716	0.280928	7603.706	0.75474
1000	31.182	0.008	22.868	10	8107.978	16105.48	0.298976	7997.506	0.793829
1000	31.182	0.008	22.868	12	8961.151	17215.48	0.312241	8254.333	0.819321

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	31.182	0.008	22.868	14	9711.387	18136.53	0.322422	8425.148	0.836276
1000	31.182	0.008	22.868	16	10383.35	18921.66	0.330472	8538.306	0.847508
1000	31.182	0.008	22.868	18	10993.54	19604.5	0.336974	8610.957	0.854719
1000	31.182	0.008	22.868	20	11553.59	20207.72	0.342307	8654.129	0.859005
1000	31.182	0.008	22.868	22	12072.01	20747.27	0.346733	8675.256	0.861102
1000	31.182	0.008	22.868	24	12555.27	21234.8	0.350434	8679.536	0.861527
1000	32.182	0.004	23.868	2	1984.996	5261.797	0.124552	3276.801	0.327202
1000	32.182	0.004	23.868	4	4343.362	10117.49	0.218867	5774.132	0.576571
1000	32.182	0.004	23.868	6	5920.309	12781.09	0.262625	6860.78	0.685078
1000	32.182	0.004	23.868	8	7137.717	14595.58	0.289094	7457.867	0.744699
1000	32.182	0.004	23.868	10	8142.394	15961.32	0.307123	7818.93	0.780753
1000	32.182	0.004	23.868	12	9004.521	17050.84	0.320258	8046.318	0.803459
1000	32.182	0.004	23.868	14	9763.604	17953.87	0.330243	8190.27	0.817833
1000	32.182	0.004	23.868	16	10444.28	18722.91	0.338055	8278.635	0.826657
1000	32.182	0.004	23.868	18	11063.03	19391.22	0.34429	8328.196	0.831605
1000	32.182	0.004	23.868	20	11631.48	19981.19	0.349337	8349.709	0.833754
1000	32.182	0.004	23.868	22	12160.37	20508.55	0.353401	8348.178	0.833601
1000	32.182	0.004	23.868	24	12652.19	20984.81	0.356775	8332.611	0.832046
1000	32.182	0.005	23.868	2	1983.398	5267.265	0.122568	3283.867	0.324987
1000	32.182	0.005	23.868	4	4335.536	10137.92	0.215864	5802.385	0.574232
1000	32.182	0.005	23.868	6	5905.867	12813.87	0.259356	6907.999	0.683649
1000	32.182	0.005	23.868	8	7116.837	14638.49	0.285768	7521.65	0.744379
1000	32.182	0.005	23.868	10	8115.346	16012.77	0.303828	7897.429	0.781568
1000	32.182	0.005	23.868	12	8971.575	17109.69	0.317039	8138.11	0.805387
1000	32.182	0.005	23.868	14	9725.01	18019.24	0.327127	8294.231	0.820837
1000	32.182	0.005	23.868	16	10400.26	18794.11	0.33506	8393.85	0.830696
1000	32.182	0.005	23.868	18	11013.79	19467.7	0.341427	8453.908	0.83664
1000	32.182	0.005	23.868	20	11577.21	20062.49	0.346614	8485.278	0.839744
1000	32.182	0.005	23.868	22	12099.02	20594.29	0.350884	8495.274	0.840733
1000	32.182	0.005	23.868	24	12587.96	21074.67	0.354362	8486.711	0.839886
1000	32.182	0.006	23.868	2	1981.83	5272.465	0.120644	3290.635	0.322782
1000	32.182	0.006	23.868	4	4327.9	10157.41	0.212934	5829.513	0.571824
1000	32.182	0.006	23.868	6	5891.808	12845.2	0.256153	6953.392	0.682066
1000	32.182	0.006	23.868	8	7096.546	14679.55	0.282497	7583.008	0.743826
1000	32.182	0.006	23.868	10	8089.098	16062.07	0.300576	7972.976	0.782078
1000	32.182	0.006	23.868	12	8939.64	17166.12	0.313851	8226.475	0.806944
1000	32.182	0.006	23.868	14	9687.637	18081.96	0.32403	8394.327	0.823409
1000	32.182	0.006	23.868	16	10357.67	18862.47	0.332069	8504.796	0.834245
1000	32.182	0.006	23.868	18	10966.2	19541.17	0.338554	8574.97	0.841129
1000	32.182	0.006	23.868	20	11524.78	20140.62	0.343867	8615.838	0.845137
1000	32.182	0.006	23.868	22	12041.93	20676.73	0.348269	8634.8	0.846997
1000	32.182	0.006	23.868	24	12524.06	21161.09	0.351944	8637.033	0.847216

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	32.182	0.007	23.868	2	1980.292	5277.416	0.118778	3297.124	0.320588
1000	32.182	0.007	23.868	4	4320.446	10176.03	0.210076	5855.582	0.569354
1000	32.182	0.007	23.868	6	5878.115	12875.18	0.253016	6997.063	0.680344
1000	32.182	0.007	23.868	8	7076.817	14718.89	0.279283	7642.076	0.74306
1000	32.182	0.007	23.868	10	8063.609	16109.34	0.29737	8045.732	0.782309
1000	32.182	0.007	23.868	12	8908.664	17220.26	0.310697	8311.597	0.808159
1000	32.182	0.007	23.868	14	9651.421	18142.19	0.320954	8490.765	0.825581
1000	32.182	0.007	23.868	16	10316.44	18928.14	0.329087	8611.698	0.837339
1000	32.182	0.007	23.868	18	10920.14	19611.77	0.335678	8691.629	0.845111
1000	32.182	0.007	23.868	20	11474.09	20215.75	0.341104	8741.653	0.849975
1000	32.182	0.007	23.868	22	11986.76	20756.02	0.345624	8769.257	0.852659
1000	32.182	0.007	23.868	24	12464.56	21244.25	0.349422	8779.685	0.853673
1000	32.182	0.008	23.868	2	1978.783	5282.136	0.116967	3303.353	0.318408
1000	32.182	0.008	23.868	4	4313.168	10193.82	0.207287	5880.655	0.566832
1000	32.182	0.008	23.868	6	5864.773	12903.88	0.249944	7039.109	0.678494
1000	32.182	0.008	23.868	8	7057.624	14756.6	0.276125	7698.979	0.742099
1000	32.182	0.008	23.868	10	8038.846	16154.69	0.294211	8115.846	0.78228
1000	32.182	0.008	23.868	12	8878.601	17272.25	0.307579	8393.646	0.809057
1000	32.182	0.008	23.868	14	9616.304	18200.04	0.317902	8583.737	0.82738
1000	32.182	0.008	23.868	16	10276.49	18991.26	0.326119	8714.768	0.84001
1000	32.182	0.008	23.868	18	10875.56	19679.67	0.332803	8804.112	0.848622
1000	32.182	0.008	23.868	20	11425.04	20288.01	0.338331	8862.969	0.854295
1000	32.182	0.008	23.868	22	11933.41	20832.32	0.342958	8898.908	0.857759
1000	32.182	0.008	23.868	24	12407.06	21324.3	0.346868	8917.238	0.859526
1200	28.182	0.004	19.868	2	2009.993	6289.817	0.139247	4279.825	0.485538
1200	28.182	0.004	19.868	4	4451.196	12047.12	0.243491	7595.92	0.861743
1200	28.182	0.004	19.868	6	6112.997	15184.08	0.291696	9071.086	1.029098
1200	28.182	0.004	19.868	8	7409.877	17311.75	0.320943	9901.874	1.123349
1200	28.182	0.004	19.868	10	8488.554	18907.99	0.340982	10419.43	1.182065
1200	28.182	0.004	19.868	12	9419.856	20178.04	0.355698	10758.18	1.220496
1200	28.182	0.004	19.868	14	10243.95	21228.39	0.366997	10984.44	1.246164
1200	28.182	0.004	19.868	16	10988.13	22121.19	0.375899	11133.06	1.263025
1200	28.182	0.004	19.868	18	11665.85	22895.76	0.383124	11229.91	1.274013
1200	28.182	0.004	19.868	20	12290.58	23578.51	0.389063	11287.92	1.280594
1200	28.182	0.004	19.868	22	12871.17	24187.98	0.394002	11316.81	1.283871
1200	28.182	0.004	19.868	24	13414.33	24737.72	0.398145	11323.39	1.284618
1200	28.182	0.005	19.868	2	2007.816	6299.167	0.136436	4291.351	0.481925
1200	28.182	0.005	19.868	4	4440.66	12081.97	0.23927	7641.31	0.858131
1200	28.182	0.005	19.868	6	6093.309	15239.89	0.287101	9146.579	1.027175
1200	28.182	0.005	19.868	8	7381.163	17384.68	0.316251	10003.51	1.12341

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1200	28.182	0.005	19.868	10	8451.11	18995.33	0.336306	10544.22	1.184131
1200	28.182	0.005	19.868	12	9374.004	20277.82	0.351096	10903.82	1.224515
1200	28.182	0.005	19.868	14	10190	21339.13	0.3625	11149.13	1.252064
1200	28.182	0.005	19.868	16	10924.28	22241.71	0.371571	11317.43	1.270964
1200	28.182	0.005	19.868	18	11596.09	23025.12	0.378903	11429.03	1.283498
1200	28.182	0.005	19.868	20	12213.39	23715.93	0.384993	11502.54	1.291753
1200	28.182	0.005	19.868	22	12786.76	24332.83	0.390091	11546.07	1.296641
1200	28.182	0.005	19.868	24	13322.88	24889.44	0.3944	11566.56	1.298942
1200	28.182	0.006	19.868	2	2005.691	6307.927	0.133732	4302.236	0.478313
1200	28.182	0.006	19.868	4	4430.426	12114.77	0.235179	7684.341	0.854328
1200	28.182	0.006	19.868	6	6074.241	15292.53	0.282625	9218.293	1.02487
1200	28.182	0.006	19.868	8	7353.416	17453.6	0.311661	10100.18	1.122916
1200	28.182	0.006	19.868	10	8414.993	19077.98	0.331715	10662.99	1.185488
1200	28.182	0.006	19.868	12	9329.845	20372.36	0.346559	11042.51	1.227683
1200	28.182	0.006	19.868	14	10138.11	21444.14	0.358051	11306.02	1.256979
1200	28.182	0.006	19.868	16	10864.94	22356.08	0.367229	11491.14	1.27756
1200	28.182	0.006	19.868	18	11529.19	23147.97	0.37469	11618.78	1.29175
1200	28.182	0.006	19.868	20	12139.45	23846.52	0.380912	11707.07	1.301567
1200	28.182	0.006	19.868	22	12705.98	24470.55	0.386149	11764.57	1.307959
1200	28.182	0.006	19.868	24	13235.45	25033.76	0.390601	11798.31	1.31171
1200	28.182	0.007	19.868	2	2003.617	6316.151	0.131129	4312.533	0.474708
1200	28.182	0.007	19.868	4	4420.478	12145.68	0.231212	7725.197	0.850362
1200	28.182	0.007	19.868	6	6055.761	15342.26	0.278266	9286.503	1.022225
1200	28.182	0.007	19.868	8	7326.583	17518.81	0.307174	10192.22	1.121923
1200	28.182	0.007	19.868	10	8380.125	19156.29	0.32721	10776.16	1.186201
1200	28.182	0.007	19.868	12	9287.273	20462.01	0.342093	11174.74	1.230075
1200	28.182	0.007	19.868	14	10088.15	21543.8	0.353655	11455.66	1.260997
1200	28.182	0.007	19.868	16	10807.87	22464.72	0.362924	11656.85	1.283144
1200	28.182	0.007	19.868	18	11463.33	23264.73	0.370526	11801.4	1.299055
1200	28.182	0.007	19.868	20	12068.52	23970.71	0.376832	11902.18	1.31015
1200	28.182	0.007	19.868	22	12628.56	24601.58	0.38219	11973.02	1.317947
1200	28.182	0.007	19.868	24	13151.73	25171.14	0.386769	12019.4	1.323053
1200	28.182	0.008	19.868	2	2001.591	6323.884	0.128623	4322.293	0.471115
1200	28.182	0.008	19.868	4	4410.805	12174.85	0.227366	7764.041	0.846254
1200	28.182	0.008	19.868	6	6037.84	15389.3	0.27402	9351.462	1.019277
1200	28.182	0.008	19.868	8	7300.614	17580.58	0.302788	10279.97	1.120481
1200	28.182	0.008	19.868	10	8346.437	19230.55	0.322793	10884.12	1.186331
1200	28.182	0.008	19.868	12	9246.198	20547.12	0.3377	11300.92	1.231762
1200	28.182	0.008	19.868	14	10040	21638.49	0.349319	11598.5	1.264196
1200	28.182	0.008	19.868	16	10752.93	22568	0.358663	11815.07	1.287802
1200	28.182	0.008	19.868	18	11401.85	23375.79	0.366354	11973.95	1.305119
1200	28.182	0.008	19.868	20	11998.66	24088.9	0.372797	12090.24	1.317795
1200	28.182	0.008	19.868	22	12554.28	24726.35	0.378229	12172.07	1.326714

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1200	28.182	0.008	19.868	24	13071.46	25302	0.382918	12230.54	1.333087
1400	28.182	0.004	19.868	2	2009.993	7345.775	0.139246	5335.782	0.605335
1400	28.182	0.004	19.868	4	4451.196	14082.51	0.245103	9631.316	1.092655
1400	28.182	0.004	19.868	6	6112.997	17758.7	0.294973	11645.7	1.321183
1400	28.182	0.004	19.868	8	7409.877	20254.38	0.325763	12844.5	1.457185
1400	28.182	0.004	19.868	10	8488.554	22127.94	0.347238	13639.38	1.547362
1400	28.182	0.004	19.868	12	9419.856	23619.4	0.363306	14199.55	1.610912
1400	28.182	0.004	19.868	14	10243.95	24853.39	0.37589	14609.44	1.657414
1400	28.182	0.004	19.868	16	10988.13	25902.65	0.386035	14914.52	1.692024
1400	28.182	0.004	19.868	18	11665.85	26813.23	0.394453	15147.39	1.718443
1400	28.182	0.004	19.868	20	12290.58	27616.08	0.401549	15325.5	1.738649
1400	28.182	0.004	19.868	22	12871.17	28332.95	0.407617	15461.77	1.75411
1400	28.182	0.004	19.868	24	13414.33	28979.68	0.412866	15565.36	1.765861
1400	28.182	0.005	19.868	2	2007.816	7357.83	0.136091	5350.014	0.600815
1400	28.182	0.005	19.868	4	4440.66	14127.8	0.240291	9687.145	1.087881
1400	28.182	0.005	19.868	6	6093.309	17831.38	0.289659	11738.07	1.318203
1400	28.182	0.005	19.868	8	7381.163	20349.5	0.320258	12968.34	1.456364
1400	28.182	0.005	19.868	10	8451.11	22241.99	0.341669	13790.88	1.548736
1400	28.182	0.005	19.868	12	9374.004	23749.82	0.357737	14375.81	1.614426
1400	28.182	0.005	19.868	14	10190	24998.22	0.370358	14808.22	1.662985
1400	28.182	0.005	19.868	16	10924.28	26060.37	0.380595	15136.09	1.699805
1400	28.182	0.005	19.868	18	11596.09	26982.61	0.389061	15386.52	1.72793
1400	28.182	0.005	19.868	20	12213.39	27796.11	0.396243	15582.71	1.749962
1400	28.182	0.005	19.868	22	12786.76	28522.77	0.402403	15736.01	1.767178
1400	28.182	0.005	19.868	24	13322.88	29178.58	0.407749	15855.7	1.780619
1400	28.182	0.006	19.868	2	2005.691	7369.033	0.133071	5363.342	0.596285
1400	28.182	0.006	19.868	4	4430.426	14170.06	0.235647	9739.634	1.082831
1400	28.182	0.006	19.868	6	6074.241	17899.38	0.284505	11825.14	1.314693
1400	28.182	0.006	19.868	8	7353.416	20438.66	0.314899	13085.25	1.454789
1400	28.182	0.006	19.868	10	8414.993	22349.05	0.336232	13934.06	1.549158
1400	28.182	0.006	19.868	12	9329.845	23872.38	0.352285	14542.54	1.616808
1400	28.182	0.006	19.868	14	10138.11	25134.47	0.364928	14996.36	1.667262
1400	28.182	0.006	19.868	16	10864.94	26208.87	0.375208	15343.92	1.705904
1400	28.182	0.006	19.868	18	11529.19	27142.21	0.38374	15613.01	1.735821
1400	28.182	0.006	19.868	20	12139.45	27965.85	0.390992	15826.4	1.759545
1400	28.182	0.006	19.868	22	12705.98	28701.86	0.39723	15995.88	1.778388
1400	28.182	0.006	19.868	24	13235.45	29366.34	0.402659	16130.89	1.793397
1400	28.182	0.007	19.868	2	2003.617	7379.469	0.130178	5375.852	0.591754
1400	28.182	0.007	19.868	4	4420.478	14209.56	0.231164	9789.082	1.077547
1400	28.182	0.007	19.868	6	6055.761	17963.1	0.279508	11907.34	1.310717
1400	28.182	0.007	19.868	8	7326.583	20522.37	0.309685	13195.78	1.452544

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1400	28.182	0.007	19.868	10	8380.125	22449.69	0.330926	14069.56	1.548727
1400	28.182	0.007	19.868	12	9287.273	23987.73	0.346952	14700.45	1.618173
1400	28.182	0.007	19.868	14	10088.15	25262.81	0.359603	15174.66	1.670372
1400	28.182	0.007	19.868	16	10807.87	26348.86	0.369914	15540.98	1.710695
1400	28.182	0.007	19.868	18	11463.33	27292.76	0.378521	15829.43	1.742447
1400	28.182	0.007	19.868	20	12068.52	28126.07	0.385806	16057.55	1.767557
1400	28.182	0.007	19.868	22	12628.56	28871	0.392109	16242.44	1.787909
1400	28.182	0.007	19.868	24	13151.73	29543.76	0.397607	16392.03	1.804375
1400	28.182	0.008	19.868	2	2001.591	7389.21	0.127404	5387.619	0.587232
1400	28.182	0.008	19.868	4	4410.805	14246.56	0.226836	9835.751	1.072063
1400	28.182	0.008	19.868	6	6037.84	18022.92	0.274663	11985.08	1.306333
1400	28.182	0.008	19.868	8	7300.614	20601.06	0.304614	13300.45	1.449703
1400	28.182	0.008	19.868	10	8346.437	22544.43	0.325752	14197.99	1.547533
1400	28.182	0.008	19.868	12	9246.198	24096.42	0.341738	14850.22	1.618623
1400	28.182	0.008	19.868	14	10040	25383.85	0.354386	15343.85	1.672427
1400	28.182	0.008	19.868	16	10752.93	26480.98	0.364717	15728.05	1.714304
1400	28.182	0.008	19.868	18	11401.85	27434.95	0.373358	16033.1	1.747553
1400	28.182	0.008	19.868	20	11998.66	28277.48	0.380718	16278.82	1.774335
1400	28.182	0.008	19.868	22	12554.28	29030.91	0.387049	16476.64	1.795897
1400	28.182	0.008	19.868	24	13071.46	29711.57	0.392606	16640.11	1.813715
1600	28.182	0.004	19.868	2	2009.993	8403.867	0.13878	6393.874	0.725373
1600	28.182	0.004	19.868	4	4451.196	16124.72	0.245417	11673.53	1.32434
1600	28.182	0.004	19.868	6	6112.997	20344.09	0.296249	14231.09	1.614491
1600	28.182	0.004	19.868	8	7409.877	23211.07	0.327953	15801.19	1.792616
1600	28.182	0.004	19.868	10	8488.554	25364.75	0.350278	16876.19	1.914573
1600	28.182	0.004	19.868	12	9419.856	27080.06	0.367142	17660.21	2.003517
1600	28.182	0.004	19.868	14	10243.95	28499.83	0.380476	18255.88	2.071096
1600	28.182	0.004	19.868	16	10988.13	29707.47	0.391341	18719.34	2.123675
1600	28.182	0.004	19.868	18	11665.85	30755.82	0.400442	19089.98	2.165722
1600	28.182	0.004	19.868	20	12290.58	31680.38	0.408195	19389.8	2.199737
1600	28.182	0.004	19.868	22	12871.17	32506.11	0.414898	19634.94	2.227547
1600	28.182	0.004	19.868	24	13414.33	33251.22	0.420762	19836.89	2.250459
1600	28.182	0.005	19.868	2	2007.816	8418.733	0.135302	6410.918	0.719956
1600	28.182	0.005	19.868	4	4440.66	16181.21	0.240059	11740.55	1.318482
1600	28.182	0.005	19.868	6	6093.309	20434.98	0.290281	14341.67	1.610591
1600	28.182	0.005	19.868	8	7381.163	23330.2	0.32172	15949.04	1.791101
1600	28.182	0.005	19.868	10	8451.11	25507.73	0.343925	17056.62	1.915485
1600	28.182	0.005	19.868	12	9374.004	27243.7	0.36074	17869.7	2.006794
1600	28.182	0.005	19.868	14	10190	28681.68	0.374067	18491.68	2.076643
1600	28.182	0.005	19.868	16	10924.28	29905.62	0.384975	18981.34	2.131633
1600	28.182	0.005	19.868	18	11596.09	30968.73	0.394091	19372.64	2.175577
1600	28.182	0.005	19.868	20	12213.39	31906.77	0.401892	19693.37	2.211596

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1600	28.182	0.005	19.868	22	12786.76	32744.92	0.40865	19958.16	2.241331
1600	28.182	0.005	19.868	24	13322.88	33501.53	0.414575	20178.65	2.266093
1600	28.182	0.006	19.868	2	2005.691	8432.453	0.131989	6426.761	0.714513
1600	28.182	0.006	19.868	4	4430.426	16233.49	0.234909	11803.06	1.312239
1600	28.182	0.006	19.868	6	6074.241	20519.33	0.284517	14445.09	1.605974
1600	28.182	0.006	19.868	8	7353.416	23440.98	0.315679	16087.56	1.78858
1600	28.182	0.006	19.868	10	8414.993	25640.91	0.337749	17225.91	1.91514
1600	28.182	0.006	19.868	12	9329.845	27396.3	0.354501	18066.46	2.008589
1600	28.182	0.006	19.868	14	10138.11	28851.45	0.367807	18713.33	2.080508
1600	28.182	0.006	19.868	16	10864.94	30090.77	0.37872	19225.83	2.137486
1600	28.182	0.006	19.868	18	11529.19	31167.82	0.387863	19638.63	2.18338
1600	28.182	0.006	19.868	20	12139.45	32118.63	0.395698	19979.18	2.221241
1600	28.182	0.006	19.868	22	12705.98	32968.54	0.402498	20262.57	2.252748
1600	28.182	0.006	19.868	24	13235.45	33736.08	0.408472	20500.63	2.279215
1600	28.182	0.007	19.868	2	2003.617	8445.147	0.128829	6441.53	0.70906
1600	28.182	0.007	19.868	4	4420.478	16281.99	0.229958	11861.51	1.305672
1600	28.182	0.007	19.868	6	6055.761	20597.78	0.27895	14542.02	1.600733
1600	28.182	0.007	19.868	8	7326.583	23544.2	0.309826	16217.62	1.785177
1600	28.182	0.007	19.868	10	8380.125	25765.17	0.331749	17385.04	1.913683
1600	28.182	0.007	19.868	12	9287.273	27538.85	0.348426	18251.58	2.009068
1600	28.182	0.007	19.868	14	10088.15	29010.19	0.361699	18922.04	2.08287
1600	28.182	0.007	19.868	16	10807.87	30264.05	0.372605	19456.17	2.141665
1600	28.182	0.007	19.868	18	11463.33	31354.29	0.381781	19890.96	2.189525
1600	28.182	0.007	19.868	20	12068.52	32317.17	0.389621	20248.65	2.228898
1600	28.182	0.007	19.868	22	12628.56	33178.24	0.396453	20549.68	2.262034
1600	28.182	0.007	19.868	24	13151.73	33956.13	0.402464	20804.4	2.290073
1600	28.182	0.008	19.868	2	2001.591	8456.923	0.125813	6455.332	0.703609
1600	28.182	0.008	19.868	4	4410.805	16327.09	0.225196	11916.28	1.298834
1600	28.182	0.008	19.868	6	6037.84	20670.9	0.273573	14633.06	1.594953
1600	28.182	0.008	19.868	8	7300.614	23640.56	0.304155	16339.95	1.780998
1600	28.182	0.008	19.868	10	8346.437	25881.32	0.325922	17534.89	1.911243
1600	28.182	0.008	19.868	12	9246.198	27672.25	0.342515	18426.05	2.008376
1600	28.182	0.008	19.868	14	10040	29158.86	0.355745	19118.87	2.083891
1600	28.182	0.008	19.868	16	10752.93	30426.46	0.366634	19673.53	2.144347
1600	28.182	0.008	19.868	18	11401.85	31529.18	0.37581	20127.33	2.19381
1600	28.182	0.008	19.868	20	11998.66	32503.51	0.383686	20504.85	2.234958
1600	28.182	0.008	19.868	22	12554.28	33375.14	0.390521	20820.87	2.269403
1600	28.182	0.008	19.868	24	13071.46	34162.86	0.39656	21091.4	2.29889
1800	28.182	0.004	19.868	2	2009.993	9464.196	0.138054	7454.203	0.845666
1800	28.182	0.004	19.868	4	4451.196	18173.52	0.245002	13722.32	1.556772
1800	28.182	0.004	19.868	6	6112.997	22939.79	0.296412	16826.79	1.908968

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1800	28.182	0.004	19.868	8	7409.877	26181.17	0.328691	18771.29	2.129568
1800	28.182	0.004	19.868	10	8488.554	28617.61	0.351562	20129.06	2.283604
1800	28.182	0.004	19.868	12	9419.856	30559.08	0.368938	21139.22	2.398206
1800	28.182	0.004	19.868	14	10243.95	32166.67	0.382755	21922.72	2.487092
1800	28.182	0.004	19.868	16	10988.13	33534.54	0.39408	22546.41	2.557848
1800	28.182	0.004	19.868	18	11665.85	34722.32	0.403618	23056.48	2.615714
1800	28.182	0.004	19.868	20	12290.58	35770.12	0.411789	23479.53	2.66371
1800	28.182	0.004	19.868	22	12871.17	36706.13	0.418893	23834.95	2.704031
1800	28.182	0.004	19.868	24	13414.33	37550.92	0.425144	24136.59	2.738251
1800	28.182	0.005	19.868	2	2007.816	9481.878	0.13427	7474.062	0.839348
1800	28.182	0.005	19.868	4	4440.66	18241.79	0.23913	13801.13	1.549887
1800	28.182	0.005	19.868	6	6093.309	23049.96	0.289833	16956.65	1.904257
1800	28.182	0.005	19.868	8	7381.163	26325.8	0.321786	18944.64	2.127511
1800	28.182	0.005	19.868	10	8451.11	28791.39	0.344489	20340.28	2.284245
1800	28.182	0.005	19.868	12	9374.004	30758.13	0.361778	21384.12	2.401469
1800	28.182	0.005	19.868	14	10190	32388.02	0.375554	22198.02	2.492871
1800	28.182	0.005	19.868	16	10924.28	33775.86	0.386889	22851.58	2.566267
1800	28.182	0.005	19.868	18	11596.09	34981.75	0.396418	23385.66	2.626245
1800	28.182	0.005	19.868	20	12213.39	36046.09	0.404611	23832.7	2.676448
1800	28.182	0.005	19.868	22	12786.76	36997.35	0.411745	24210.59	2.718886
1800	28.182	0.005	19.868	24	13322.88	37856.28	0.418034	24533.4	2.755138
1800	28.182	0.006	19.868	2	2005.691	9498.106	0.130682	7492.415	0.83299
1800	28.182	0.006	19.868	4	4430.426	18304.48	0.233509	13874.06	1.542487
1800	28.182	0.006	19.868	6	6074.241	23151.42	0.283503	17077.18	1.898603
1800	28.182	0.006	19.868	8	7353.416	26459.27	0.315118	19105.85	2.124147
1800	28.182	0.006	19.868	10	8414.993	28952.03	0.33764	20537.04	2.283263
1800	28.182	0.006	19.868	12	9329.845	30942.36	0.354828	21612.51	2.402832
1800	28.182	0.006	19.868	14	10138.11	32593.13	0.368551	22455.02	2.4965
1800	28.182	0.006	19.868	16	10864.94	33999.7	0.379862	23134.76	2.572072
1800	28.182	0.006	19.868	18	11529.19	35222.57	0.38939	23693.38	2.634178
1800	28.182	0.006	19.868	20	12139.45	36302.47	0.397592	24163.03	2.686392
1800	28.182	0.006	19.868	22	12705.98	37268.09	0.404745	24562.11	2.730762
1800	28.182	0.006	19.868	24	13235.45	38140.35	0.41106	24904.9	2.768873
1800	28.182	0.007	19.868	2	2003.617	9513.043	0.127276	7509.426	0.826611
1800	28.182	0.007	19.868	4	4420.478	18362.23	0.228126	13941.76	1.534658
1800	28.182	0.007	19.868	6	6055.761	23245.1	0.277413	17189.34	1.892141
1800	28.182	0.007	19.868	8	7326.583	26582.74	0.308682	19256.16	2.119648
1800	28.182	0.007	19.868	10	8380.125	29100.85	0.331011	20720.73	2.280863
1800	28.182	0.007	19.868	12	9287.273	31113.25	0.348088	21825.98	2.402525
1800	28.182	0.007	19.868	14	10088.15	32783.58	0.361746	22695.43	2.498231
1800	28.182	0.007	19.868	16	10807.87	34207.72	0.373022	23399.85	2.575771
1800	28.182	0.007	19.868	18	11463.33	35446.56	0.382553	23983.23	2.639987
1800	28.182	0.007	19.868	20	12068.52	36541.09	0.390738	24472.57	2.693852

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1800	28.182	0.007	19.868	22	12628.56	37520.22	0.397901	24891.66	2.739984
1800	28.182	0.007	19.868	24	13151.73	38405.05	0.404231	25253.31	2.779794
1800	28.182	0.008	19.868	2	2001.591	9526.829	0.124039	7525.238	0.820225
1800	28.182	0.008	19.868	4	4410.805	18415.58	0.222969	14004.78	1.526473
1800	28.182	0.008	19.868	6	6037.84	23331.83	0.271554	17294	1.884986
1800	28.182	0.008	19.868	8	7300.614	26697.24	0.30247	19396.63	2.114166
1800	28.182	0.008	19.868	10	8346.437	29239.04	0.324599	20892.6	2.277222
1800	28.182	0.008	19.868	12	9246.198	31272.1	0.341555	22025.91	2.400748
1800	28.182	0.008	19.868	14	10040	32960.77	0.355138	22920.78	2.498286
1800	28.182	0.008	19.868	16	10752.93	34401.41	0.366369	23648.48	2.577604
1800	28.182	0.008	19.868	18	11401.85	35655.26	0.375876	24253.41	2.643539
1800	28.182	0.008	19.868	20	11998.66	36763.57	0.38407	24764.91	2.69929
1800	28.182	0.008	19.868	22	12554.28	37755.43	0.391217	25201.15	2.746839
1800	28.182	0.008	19.868	24	13071.46	38652.1	0.397555	25580.63	2.788201
2000	28.182	0.004	19.868	2	2009.993	10526.88	0.137176	8516.883	0.966225
2000	28.182	0.004	19.868	4	4451.196	20228.72	0.244144	15777.53	1.789931
2000	28.182	0.004	19.868	6	6112.997	25545.39	0.295897	19432.39	2.204569
2000	28.182	0.004	19.868	8	7409.877	29164.1	0.328553	21754.22	2.467976
2000	28.182	0.004	19.868	10	8488.554	31885.81	0.35179	23397.26	2.654375
2000	28.182	0.004	19.868	12	9419.856	34055.62	0.369513	24635.76	2.794881
2000	28.182	0.004	19.868	14	10243.95	35852.98	0.383659	25609.03	2.905297
2000	28.182	0.004	19.868	16	10988.13	37382.82	0.3953	26394.69	2.994428
2000	28.182	0.004	19.868	18	11665.85	38711.63	0.405136	27045.78	3.068293
2000	28.182	0.004	19.868	20	12290.58	39884.12	0.413593	27593.53	3.130435
2000	28.182	0.004	19.868	22	12871.17	40931.75	0.42097	28060.58	3.18342
2000	28.182	0.004	19.868	24	13414.33	41877.48	0.427484	28463.15	3.229092
2000	28.182	0.005	19.868	2	2007.816	10547.27	0.1331	8539.457	0.958994
2000	28.182	0.005	19.868	4	4440.66	20309.17	0.237784	15868.51	1.782058
2000	28.182	0.005	19.868	6	6093.309	25675.68	0.288741	19582.37	2.199129
2000	28.182	0.005	19.868	8	7381.163	29335.43	0.321014	21954.27	2.465497
2000	28.182	0.005	19.868	10	8451.11	32091.91	0.344041	23640.8	2.654898
2000	28.182	0.005	19.868	12	9374.004	34291.88	0.361645	24917.88	2.798315
2000	28.182	0.005	19.868	14	10190	36115.9	0.375724	25925.89	2.911517
2000	28.182	0.005	19.868	16	10924.28	37669.62	0.387348	26745.34	3.003542
2000	28.182	0.005	19.868	18	11596.09	39020.09	0.397156	27424	3.079757
2000	28.182	0.005	19.868	20	12213.39	40212.4	0.405614	27999.01	3.14433
2000	28.182	0.005	19.868	22	12786.76	41278.31	0.413004	28491.55	3.199644
2000	28.182	0.005	19.868	24	13322.88	42240.99	0.419538	28918.11	3.247547
2000	28.182	0.006	19.868	2	2005.691	10565.93	0.129254	8560.235	0.951708
2000	28.182	0.006	19.868	4	4430.426	20382.53	0.231719	15952.11	1.77352
2000	28.182	0.006	19.868	6	6074.241	25794.78	0.281881	19720.54	2.192486

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
2000	28.182	0.006	19.868	8	7353.416	29492.38	0.31376	22138.97	2.461362
2000	28.182	0.006	19.868	10	8414.993	32281.04	0.336566	23866.04	2.653375
2000	28.182	0.006	19.868	12	9329.845	34508.99	0.354037	25179.14	2.799362
2000	28.182	0.006	19.868	14	10138.11	36357.78	0.368035	26219.67	2.915045
2000	28.182	0.006	19.868	16	10864.94	37933.75	0.379611	27068.8	3.009451
2000	28.182	0.006	19.868	18	11529.19	39304.41	0.389397	27775.22	3.087989
2000	28.182	0.006	19.868	20	12139.45	40515.23	0.397845	28375.78	3.154758
2000	28.182	0.006	19.868	22	12705.98	41598.23	0.405236	28892.25	3.212177
2000	28.182	0.006	19.868	24	13235.45	42576.79	0.411779	29341.34	3.262106
2000	28.182	0.007	19.868	2	2003.617	10583.03	0.125619	8579.414	0.944391
2000	28.182	0.007	19.868	4	4420.478	20449.66	0.225935	16029.19	1.764435
2000	28.182	0.007	19.868	6	6055.761	25904.02	0.275305	19848.26	2.184825
2000	28.182	0.007	19.868	8	7326.583	29636.6	0.306784	22310.02	2.455807
2000	28.182	0.007	19.868	10	8380.125	32455.07	0.329358	24074.95	2.650083
2000	28.182	0.007	19.868	12	9287.273	34709.02	0.346685	25421.74	2.798334
2000	28.182	0.007	19.868	14	10088.15	36580.86	0.360591	26492.71	2.916222
2000	28.182	0.007	19.868	16	10807.87	38177.57	0.372109	27369.7	3.012758
2000	28.182	0.007	19.868	18	11463.33	39567.09	0.381874	28103.76	3.093561
2000	28.182	0.007	19.868	20	12068.52	40795.21	0.390289	28726.68	3.162129
2000	28.182	0.007	19.868	22	12628.56	41894.19	0.397671	29265.63	3.221455
2000	28.182	0.007	19.868	24	13151.73	42887.61	0.404214	29735.88	3.273218
2000	28.182	0.008	19.868	2	2001.591	10598.76	0.122179	8597.167	0.937062
2000	28.182	0.008	19.868	4	4410.805	20511.3	0.220414	16100.5	1.754899
2000	28.182	0.008	19.868	6	6037.84	26004.52	0.269002	19966.68	2.1763
2000	28.182	0.008	19.868	8	7300.614	29769.5	0.300076	22468.89	2.449032
2000	28.182	0.008	19.868	10	8346.437	32615.66	0.322409	24269.22	2.645262
2000	28.182	0.008	19.868	12	9246.198	34893.78	0.339584	25647.58	2.795499
2000	28.182	0.008	19.868	14	10040	36787.11	0.35339	26747.12	2.915344
2000	28.182	0.008	19.868	16	10752.93	38403.18	0.364839	27650.25	3.013782
2000	28.182	0.008	19.868	18	11401.85	39810.31	0.37456	28408.47	3.096426
2000	28.182	0.008	19.868	20	11998.66	41054.61	0.382962	29055.95	3.166999
2000	28.182	0.008	19.868	22	12554.28	42168.56	0.390314	29614.28	3.227855
2000	28.182	0.008	19.868	24	13071.46	43175.92	0.396848	30104.45	3.281282
1000	28.182	0	19.868	2	2019.263	5204.152	0.148972	3184.889	0.376705
1000	28.182	0	19.868	4	4496.658	9902.444	0.25446	5405.785	0.63939
1000	28.182	0	19.868	6	6198.685	12436.15	0.300079	6237.466	0.73776
1000	28.182	0	19.868	8	7535.651	14144.13	0.325899	6608.48	0.781643
1000	28.182	0	19.868	10	8653.402	15419.92	0.342217	6766.516	0.800335
1000	28.182	0	19.868	12	9624.636	16431.59	0.353008	6806.951	0.805118
1000	28.182	0	19.868	14	10486.49	17265.97	0.36033	6779.48	0.801869
1000	28.182	0	19.868	16	11265.42	17973.57	0.365226	6708.155	0.793433
1000	28.182	0	19.868	18	11978.41	18586.25	0.368349	6607.844	0.781568

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	28.182	0	19.868	20	12637.54	19125.36	0.37012	6487.825	0.767372
1000	28.182	0	19.868	22	13251.7	19605.89	0.370822	6354.184	0.751565
1000	28.182	0	19.868	24	13827.67	20038.71	0.370655	6211.041	0.734635
1000	29.182	0	20.868	2	2011.967	5213.126	0.144663	3201.158	0.365654
1000	29.182	0	20.868	4	4463.175	9936.038	0.248383	5472.863	0.625141
1000	29.182	0	20.868	6	6138.042	12490.15	0.293872	6352.11	0.725574
1000	29.182	0	20.868	8	7449.14	14214.91	0.320003	6765.774	0.772825
1000	29.182	0	20.868	10	8542.5	15504.9	0.336822	6962.404	0.795285
1000	29.182	0	20.868	12	9488.641	16528.89	0.348288	7040.249	0.804177
1000	29.182	0	20.868	14	10330.12	17374.14	0.356245	7044.025	0.804608
1000	29.182	0	20.868	16	11088.02	18091.48	0.361885	7003.468	0.799976
1000	29.182	0	20.868	18	11780.89	18713	0.3658	6932.111	0.791825
1000	29.182	0	20.868	20	12420.7	19260.19	0.368407	6839.497	0.781246
1000	29.182	0	20.868	22	13016.25	19748.17	0.369988	6731.916	0.768958
1000	29.182	0	20.868	24	13574.25	20187.9	0.37074	6613.649	0.755448
1000	30.182	0	21.868	2	2005.183	5221.527	0.140594	3216.344	0.355217
1000	30.182	0	21.868	4	4432.198	9967.54	0.242566	5535.342	0.611329
1000	30.182	0	21.868	6	6082.096	12540.86	0.287854	6458.761	0.713313
1000	30.182	0	21.868	8	7369.484	14281.44	0.3142	6911.957	0.763364
1000	30.182	0	21.868	10	8440.536	15584.84	0.331412	7144.304	0.789025
1000	30.182	0	21.868	12	9365.64	16620.45	0.343368	7254.813	0.80123
1000	30.182	0	21.868	14	10186.74	17475.99	0.351894	7289.255	0.805033
1000	30.182	0	21.868	16	10925.52	18202.55	0.358137	7277.031	0.803683
1000	30.182	0	21.868	18	11600.12	18832.43	0.362694	7232.306	0.798744
1000	30.182	0	21.868	20	12222.4	19387.28	0.365975	7164.881	0.791297
1000	30.182	0	21.868	22	12801.08	19882.31	0.368259	7081.224	0.782058
1000	30.182	0	21.868	24	13342.82	20328.6	0.369744	6985.778	0.771517
1000	31.182	0	22.868	2	1998.862	5229.404	0.136746	3230.543	0.345343
1000	31.182	0	22.868	4	4403.462	9997.151	0.236994	5593.689	0.597961
1000	31.182	0	22.868	6	6030.324	12588.57	0.282026	6558.243	0.701071
1000	31.182	0	22.868	8	7295.908	14344.09	0.308511	7048.179	0.753445
1000	31.182	0	22.868	10	8346.483	15660.16	0.326029	7313.679	0.781827
1000	31.182	0	22.868	12	9252.318	16706.78	0.338378	7454.462	0.796877
1000	31.182	0	22.868	14	10053.12	17572.05	0.347416	7518.933	0.803769
1000	31.182	0	22.868	16	10776.15	18307.35	0.354104	7531.2	0.80508
1000	31.182	0	22.868	18	11434.08	18945.15	0.359184	7511.071	0.802928
1000	31.182	0	22.868	20	12040.39	19507.26	0.363014	7466.872	0.798203

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	31.182	0	22.868	22	12603.72	20008.99	0.365869	7405.264	0.791617
1000	31.182	0	22.868	24	13130.66	20461.5	0.367946	7330.844	0.783662
1000	32.182	0	23.868	2	1992.953	5236.809	0.133101	3243.856	0.335991
1000	32.182	0	23.868	4	4376.725	10025.02	0.231656	5648.3	0.585037
1000	32.182	0	23.868	6	5982.28	12633.54	0.276386	6651.261	0.688921
1000	32.182	0	23.868	8	7227.743	14403.18	0.302946	7175.44	0.743215
1000	32.182	0	23.868	10	8259.465	15731.25	0.320698	7471.781	0.773909
1000	32.182	0	23.868	12	9147.579	16788.3	0.333365	7640.726	0.791408
1000	32.182	0	23.868	14	9931.649	17662.81	0.342771	7731.158	0.800775
1000	32.182	0	23.868	16	10636.4	18406.39	0.34993	7769.985	0.804796
1000	32.182	0	23.868	18	11281.06	19051.72	0.355385	7770.654	0.804865
1000	32.182	0	23.868	20	11872.76	19620.72	0.359666	7747.959	0.802515
1000	32.182	0	23.868	22	12422.07	20128.82	0.36299	7706.747	0.798246
1000	32.182	0	23.868	24	12935.5	20587.24	0.36555	7651.742	0.792549
1200	28.182	0	19.868	2	2019.263	6245.21	0.151684	4225.947	0.49984
1200	28.182	0	19.868	4	4496.658	11883.02	0.261746	7386.364	0.87365
1200	28.182	0	19.868	6	6198.685	14923.43	0.311284	8724.745	1.031952
1200	28.182	0	19.868	8	7535.651	16972.98	0.340703	9437.333	1.116236
1200	28.182	0	19.868	10	8653.402	18503.92	0.360445	9850.521	1.165108
1200	28.182	0	19.868	12	9624.636	19717.92	0.374583	10093.29	1.193822
1200	28.182	0	19.868	14	10486.49	20719.18	0.385192	10232.68	1.210309
1200	28.182	0	19.868	16	11265.42	21568.29	0.393358	10302.88	1.218612
1200	28.182	0	19.868	18	11978.41	22303.51	0.399755	10325.1	1.22124
1200	28.182	0	19.868	20	12637.54	22950.45	0.404821	10312.91	1.219798
1200	28.182	0	19.868	22	13251.7	23527.07	0.408852	10275.37	1.215358
1200	28.182	0	19.868	24	13827.67	24046.46	0.412059	10218.79	1.208666
1400	28.182	0	19.868	2	2019.263	7286.855	0.153389	5267.592	0.623044
1400	28.182	0	19.868	4	4496.658	13863.86	0.26615	9367.203	1.107942
1400	28.182	0	19.868	6	6198.685	17410.86	0.317891	11212.18	1.326163
1400	28.182	0	19.868	8	7535.651	19801.95	0.349252	12266.3	1.450843
1400	28.182	0	19.868	10	8653.402	21588	0.370778	12934.6	1.529889
1400	28.182	0	19.868	12	9624.636	23004.32	0.386605	13379.68	1.582533
1400	28.182	0	19.868	14	10486.49	24172.43	0.398824	13685.94	1.618756
1400	28.182	0	19.868	16	11265.42	25163.05	0.408548	13897.64	1.643796
1400	28.182	0	19.868	18	11978.41	26020.8	0.416465	14042.39	1.660917
1400	28.182	0	19.868	20	12637.54	26775.55	0.423021	14138.01	1.672227
1400	28.182	0	19.868	22	13251.7	27448.28	0.428523	14196.58	1.679154
1400	28.182	0	19.868	24	13827.67	28054.23	0.433185	14226.56	1.6827

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1600	28.182	0	19.868	2	2019.263	8329.7	0.154579	6310.438	0.746391
1600	28.182	0	19.868	4	4496.658	15845.31	0.269109	11348.65	1.342305
1600	28.182	0	19.868	6	6198.685	19898.7	0.322255	13700.01	1.620421
1600	28.182	0	19.868	8	7535.651	22631.2	0.354824	15095.55	1.785483
1600	28.182	0	19.868	10	8653.402	24672.31	0.377436	16018.91	1.894698
1600	28.182	0	19.868	12	9624.636	26290.89	0.394272	16666.25	1.971265
1600	28.182	0	19.868	14	10486.49	27625.83	0.407436	17139.34	2.027221
1600	28.182	0	19.868	16	11265.42	28757.95	0.418059	17492.53	2.068996
1600	28.182	0	19.868	18	11978.41	29738.2	0.426839	17759.79	2.100607
1600	28.182	0	19.868	20	12637.54	30600.76	0.434232	17963.22	2.124668
1600	28.182	0	19.868	22	13251.7	31369.57	0.440546	18117.87	2.14296
1600	28.182	0	19.868	24	13827.67	32062.07	0.446001	18234.4	2.156743
1800	28.182	0	19.868	2	2019.263	9374.589	0.155483	7355.326	0.869979
1800	28.182	0	19.868	4	4496.658	17827.88	0.271248	13331.22	1.576801
1800	28.182	0	19.868	6	6198.685	22387.3	0.325362	16188.62	1.91477
1800	28.182	0	19.868	8	7535.651	25461.03	0.35875	17925.38	2.120193
1800	28.182	0	19.868	10	8653.402	27757.08	0.382089	19103.68	2.259561
1800	28.182	0	19.868	12	9624.636	29577.84	0.399592	19953.21	2.360041
1800	28.182	0	19.868	14	10486.49	31079.56	0.413373	20593.07	2.435723
1800	28.182	0	19.868	16	11265.42	32353.11	0.424577	21087.7	2.494227
1800	28.182	0	19.868	18	11978.41	33455.84	0.43391	21477.43	2.540325
1800	28.182	0	19.868	20	12637.54	34426.17	0.441832	21788.63	2.577134
1800	28.182	0	19.868	22	13251.7	35291.05	0.448657	22039.35	2.606788
1800	28.182	0	19.868	24	13827.67	36070.09	0.454607	22242.41	2.630806
2000	28.182	0	19.868	2	2019.263	10408.22	0.155977	8388.955	0.992236
2000	28.182	0	19.868	4	4496.658	19812.21	0.272882	15315.55	1.811505
2000	28.182	0	19.868	6	6198.685	24877.15	0.327697	18678.47	2.209267
2000	28.182	0	19.868	8	7535.651	28291.83	0.361674	20756.18	2.455016
2000	28.182	0	19.868	10	8653.402	30842.64	0.385531	22189.24	2.624517
2000	28.182	0	19.868	12	9624.636	32865.47	0.403505	23240.83	2.748898
2000	28.182	0	19.868	14	10486.49	34533.86	0.417719	24047.37	2.844294
2000	28.182	0	19.868	16	11265.42	35948.78	0.429328	24683.37	2.919519
2000	28.182	0	19.868	18	11978.41	37173.94	0.439043	25195.53	2.980097
2000	28.182	0	19.868	20	12637.54	38252	0.447329	25614.46	3.029647
2000	28.182	0	19.868	22	13251.7	39212.91	0.454502	25961.2	3.07066
2000	28.182	0	19.868	24	13827.67	40078.44	0.460787	26250.77	3.104909

3.2.4 For one inter cooler used in compression process and one reheat in expansion

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	28.182	0.004	19.868	2	1911.75	5235.931	0.136064	3324.181	0.377122
1000	28.182	0.004	19.868	4	4019.985	10018.83	0.232165	5998.845	0.680558
1000	28.182	0.004	19.868	6	5351.587	12620.8	0.274234	7269.217	0.824679
1000	28.182	0.004	19.868	8	6343.236	14383.94	0.298762	8040.706	0.912203
1000	28.182	0.004	19.868	10	7140.309	15705.8	0.315028	8565.492	0.971739
1000	28.182	0.004	19.868	12	7810.211	16756.99	0.32664	8946.78	1.014996
1000	28.182	0.004	19.868	14	8390.012	17625.97	0.335335	9235.961	1.047803
1000	28.182	0.004	19.868	16	8902.391	18364.34	0.342063	9461.949	1.073441
1000	28.182	0.004	19.868	18	9362.289	19004.73	0.347395	9642.438	1.093917
1000	28.182	0.004	19.868	20	9780.093	19569.04	0.351696	9788.949	1.110538
1000	28.182	0.004	19.868	22	10163.33	20072.68	0.355213	9909.348	1.124197
1000	28.182	0.004	19.868	24	10517.64	20526.84	0.358118	10009.21	1.135526
1000	28.182	0.005	19.868	2	1910.77	5242.772	0.13374	3332.002	0.374189
1000	28.182	0.005	19.868	4	4015.632	10044.19	0.228933	6028.563	0.677017
1000	28.182	0.005	19.868	6	5343.899	12661.32	0.270898	7317.426	0.821758
1000	28.182	0.005	19.868	8	6332.464	14436.82	0.2955	8104.353	0.910131
1000	28.182	0.005	19.868	10	7126.69	15769.06	0.311897	8642.369	0.970551
1000	28.182	0.005	19.868	12	7793.946	16829.2	0.323661	9035.253	1.014673
1000	28.182	0.005	19.868	14	8371.27	17706.05	0.332512	9334.775	1.048309
1000	28.182	0.005	19.868	16	8881.321	18451.43	0.339398	9570.11	1.074738
1000	28.182	0.005	19.868	18	9339.015	19098.16	0.344885	9759.141	1.095966
1000	28.182	0.005	19.868	20	9754.723	19668.25	0.349338	9913.527	1.113304
1000	28.182	0.005	19.868	22	10135.96	20177.2	0.353002	10041.24	1.127646
1000	28.182	0.005	19.868	24	10488.36	20636.28	0.35605	10147.92	1.139627
1000	28.182	0.006	19.868	2	1909.812	5249.241	0.131489	3339.429	0.37127
1000	28.182	0.006	19.868	4	4011.383	10068.28	0.225774	6056.896	0.673392
1000	28.182	0.006	19.868	6	5336.406	12699.89	0.267618	7363.483	0.818656
1000	28.182	0.006	19.868	8	6321.974	14487.22	0.292275	8165.243	0.907794
1000	28.182	0.006	19.868	10	7113.437	15829.43	0.308785	8715.993	0.969025
1000	28.182	0.006	19.868	12	7778.128	16898.18	0.320684	9120.05	1.013947
1000	28.182	0.006	19.868	14	8353.056	17782.6	0.329678	9429.545	1.048356
1000	28.182	0.006	19.868	16	8860.851	18534.75	0.336707	9673.903	1.075523
1000	28.182	0.006	19.868	18	9316.414	19187.6	0.342337	9871.183	1.097457
1000	28.182	0.006	19.868	20	9730.099	19763.27	0.346929	10033.18	1.115467
1000	28.182	0.006	19.868	22	10109.41	20277.36	0.350729	10167.95	1.130451
1000	28.182	0.006	19.868	24	10459.95	20741.2	0.353909	10281.24	1.143046
1000	28.182	0.007	19.868	2	1908.874	5255.367	0.12931	3346.493	0.36837
1000	28.182	0.007	19.868	4	4007.234	10091.17	0.222689	6083.937	0.669698
1000	28.182	0.007	19.868	6	5329.098	12736.62	0.264394	7407.525	0.815394

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	28.182	0.007	19.868	8	6311.755	14535.3	0.289088	8223.546	0.905218
1000	28.182	0.007	19.868	10	7100.535	15887.09	0.305696	8786.555	0.967192
1000	28.182	0.007	19.868	12	7762.739	16964.12	0.317715	9201.381	1.012855
1000	28.182	0.007	19.868	14	8335.344	17855.84	0.326838	9520.497	1.047982
1000	28.182	0.007	19.868	16	8840.956	18614.52	0.333999	9773.565	1.075839
1000	28.182	0.007	19.868	18	9294.456	19273.27	0.339758	9978.813	1.098432
1000	28.182	0.007	19.868	20	9706.183	19854.34	0.344479	10148.16	1.117073
1000	28.182	0.007	19.868	22	10083.62	20373.39	0.348404	10289.77	1.13266
1000	28.182	0.007	19.868	24	10432.39	20841.83	0.351706	10409.44	1.145834
1000	28.182	0.008	19.868	2	1907.955	5261.177	0.127198	3353.221	0.36549
1000	28.182	0.008	19.868	4	4003.182	10112.95	0.219674	6109.773	0.665944
1000	28.182	0.008	19.868	6	5321.97	12771.65	0.261226	7449.68	0.81199
1000	28.182	0.008	19.868	8	6301.795	14581.21	0.285942	8279.416	0.902428
1000	28.182	0.008	19.868	10	7087.969	15942.2	0.302632	8854.233	0.965081
1000	28.182	0.008	19.868	12	7747.759	17027.2	0.314758	9279.442	1.011427
1000	28.182	0.008	19.868	14	8318.112	17925.95	0.323998	9607.843	1.047222
1000	28.182	0.008	19.868	16	8821.609	18690.93	0.331278	9869.321	1.075722
1000	28.182	0.008	19.868	18	9273.112	19355.38	0.337158	10082.27	1.098933
1000	28.182	0.008	19.868	20	9682.943	19941.66	0.341996	10258.72	1.118165
1000	28.182	0.008	19.868	22	10058.58	20465.51	0.346037	10406.93	1.13432
1000	28.182	0.008	19.868	24	10405.62	20938.4	0.349452	10532.79	1.148038
1000	29.182	0.004	20.868	2	1908.646	5242.971	0.132455	3334.324	0.365822
1000	29.182	0.004	20.868	4	4006.727	10045.64	0.227055	6038.911	0.662554
1000	29.182	0.004	20.868	6	5328.643	12664.31	0.268911	7335.668	0.804826
1000	29.182	0.004	20.868	8	6311.55	14441.35	0.293525	8129.798	0.891953
1000	29.182	0.004	20.868	10	7100.698	15775.07	0.309979	8674.373	0.951701
1000	29.182	0.004	20.868	12	7763.342	16836.61	0.321819	9073.271	0.995466
1000	29.182	0.004	20.868	14	8336.434	17714.78	0.330756	9378.35	1.028937
1000	29.182	0.004	20.868	16	8842.566	18461.42	0.33773	9618.858	1.055324
1000	29.182	0.004	20.868	18	9296.607	19109.34	0.343308	9812.733	1.076595
1000	29.182	0.004	20.868	20	9708.888	19680.57	0.34785	9971.678	1.094034
1000	29.182	0.004	20.868	22	10086.89	20190.59	0.351604	10103.7	1.108518
1000	29.182	0.004	20.868	24	10436.23	20650.7	0.354739	10214.48	1.120672
1000	29.182	0.005	20.868	2	1907.732	5249.423	0.13025	3341.691	0.363046
1000	29.182	0.005	20.868	4	4002.678	10069.61	0.223952	6066.934	0.65912
1000	29.182	0.005	20.868	6	5321.506	12702.66	0.26568	7381.15	0.801898
1000	29.182	0.005	20.868	8	6301.561	14491.43	0.290341	8189.864	0.889758
1000	29.182	0.005	20.868	10	7088.08	15835.02	0.3069	8746.94	0.950279
1000	29.182	0.005	20.868	12	7748.284	16905.08	0.318867	9156.795	0.994806
1000	29.182	0.005	20.868	14	8319.097	17790.74	0.327939	9471.648	1.029012
1000	29.182	0.005	20.868	16	8823.085	18544.07	0.33505	9720.99	1.056101
1000	29.182	0.005	20.868	18	9275.098	19198.04	0.340762	9922.938	1.078041

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	29.182	0.005	20.868	20	9685.454	19774.78	0.345437	10089.32	1.096117
1000	29.182	0.005	20.868	22	10061.62	20289.87	0.349319	10228.25	1.111211
1000	29.182	0.005	20.868	24	10409.2	20754.68	0.35258	10345.48	1.123947
1000	29.182	0.006	20.868	2	1906.837	5255.535	0.128113	3348.698	0.360284
1000	29.182	0.006	20.868	4	3998.723	10092.41	0.220918	6093.683	0.655615
1000	29.182	0.006	20.868	6	5314.541	12739.19	0.262504	7424.651	0.798813
1000	29.182	0.006	20.868	8	6291.823	14539.21	0.287196	8247.389	0.887331
1000	29.182	0.006	20.868	10	7075.788	15892.29	0.303845	8816.506	0.948562
1000	29.182	0.006	20.868	12	7733.624	16970.55	0.315925	9236.927	0.993795
1000	29.182	0.006	20.868	14	8302.226	17863.44	0.325118	9561.212	1.028685
1000	29.182	0.006	20.868	16	8804.136	18623.22	0.332353	9819.088	1.056429
1000	29.182	0.006	20.868	18	9254.186	19283.02	0.338189	10028.84	1.078996
1000	29.182	0.006	20.868	20	9662.678	19865.09	0.342986	10202.42	1.097671
1000	29.182	0.006	20.868	22	10037.07	20385.1	0.346987	10348.03	1.113338
1000	29.182	0.006	20.868	24	10382.95	20854.45	0.350364	10471.5	1.126622
1000	29.182	0.007	20.868	2	1905.96	5261.331	0.126042	3355.371	0.35754
1000	29.182	0.007	20.868	4	3992.725	10114.1	0.218021	6121.375	0.652279
1000	29.182	0.007	20.868	6	5307.743	12774.04	0.259383	7466.294	0.79559
1000	29.182	0.007	20.868	8	6282.327	14584.85	0.284091	8302.525	0.884697
1000	29.182	0.007	20.868	10	7063.808	15947.05	0.300815	8883.244	0.946577
1000	29.182	0.007	20.868	12	7719.345	17033.2	0.312995	9313.858	0.992462
1000	29.182	0.007	20.868	14	8285.801	17933.05	0.322298	9647.249	1.027987
1000	29.182	0.007	20.868	16	8785.696	18699.06	0.329647	9913.368	1.056344
1000	29.182	0.007	20.868	18	9233.844	19364.5	0.335596	10130.66	1.079498
1000	29.182	0.007	20.868	20	9640.53	19951.73	0.340505	10311.2	1.098736
1000	29.182	0.007	20.868	22	10013.2	20476.48	0.344616	10463.27	1.11494
1000	29.182	0.007	20.868	24	10357.44	20950.23	0.3481	10592.79	1.128742
1000	29.182	0.008	20.868	2	1905.101	5266.835	0.124033	3361.734	0.354815
1000	29.182	0.008	20.868	4	3989.07	10134.77	0.21512	6145.698	0.64865
1000	29.182	0.008	20.868	6	5301.106	12807.3	0.256318	7506.192	0.792244
1000	29.182	0.008	20.868	8	6273.062	14628.47	0.281027	8355.413	0.881875
1000	29.182	0.008	20.868	10	7052.129	15999.44	0.297815	8947.315	0.944348
1000	29.182	0.008	20.868	12	7705.431	17093.2	0.310083	9387.765	0.990835
1000	29.182	0.008	20.868	14	8269.804	17999.75	0.319485	9729.949	1.026951
1000	29.182	0.008	20.868	16	8767.744	18771.78	0.326936	10004.03	1.055879
1000	29.182	0.008	20.868	18	9214.046	19442.66	0.332989	10228.61	1.079583
1000	29.182	0.008	20.868	20	9618.983	20034.87	0.338001	10415.88	1.099348
1000	29.182	0.008	20.868	22	9989.992	20564.21	0.342213	10574.21	1.116059
1000	29.182	0.008	20.868	24	10332.64	21042.22	0.345797	10709.58	1.130347
1000	30.182	0.004	21.868	2	1905.745	5249.606	0.129031	3343.861	0.355178
1000	30.182	0.004	21.868	4	3994.36	10070.94	0.222151	6076.578	0.645442

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	30.182	0.004	21.868	6	5307.263	12705.4	0.263758	7398.138	0.785815
1000	30.182	0.004	21.868	8	6282.045	14495.59	0.288416	8213.546	0.872426
1000	30.182	0.004	21.868	10	7063.832	15840.55	0.305017	8776.717	0.932245
1000	30.182	0.004	21.868	12	7719.742	16911.9	0.317046	9192.16	0.976373
1000	30.182	0.004	21.868	14	8286.614	17798.79	0.326189	9512.177	1.010364
1000	30.182	0.004	21.868	16	8786.955	18553.28	0.333375	9766.324	1.037359
1000	30.182	0.004	21.868	18	9235.568	19208.34	0.339164	9972.771	1.059288
1000	30.182	0.004	21.868	20	9642.735	19786.13	0.343916	10143.39	1.077411
1000	30.182	0.004	21.868	22	10015.9	20302.22	0.347875	10286.32	1.092593
1000	30.182	0.004	21.868	24	10360.63	20767.98	0.351212	10407.36	1.105449
1000	30.182	0.005	21.868	2	1904.89	5255.703	0.126936	3350.813	0.352546
1000	30.182	0.005	21.868	4	3988.38	10093.63	0.21924	6105.252	0.642347
1000	30.182	0.005	21.868	6	5300.619	12741.74	0.26063	7441.122	0.782897
1000	30.182	0.005	21.868	8	6272.757	14543.09	0.285313	8270.331	0.87014
1000	30.182	0.005	21.868	10	7052.11	15897.44	0.301996	8845.334	0.930637
1000	30.182	0.005	21.868	12	7705.764	16976.91	0.314131	9271.15	0.975438
1000	30.182	0.005	21.868	14	8270.53	17870.95	0.323388	9600.419	1.010081
1000	30.182	0.005	21.868	16	8768.891	18631.82	0.330692	9862.931	1.037701
1000	30.182	0.005	21.868	18	9215.634	19292.65	0.336599	10077.02	1.060226
1000	30.182	0.005	21.868	20	9621.025	19875.71	0.341466	10254.69	1.078918
1000	30.182	0.005	21.868	22	9992.497	20396.65	0.345539	10404.16	1.094644
1000	30.182	0.005	21.868	24	10335.61	20866.91	0.348986	10531.3	1.108021
1000	30.182	0.006	21.868	2	1904.052	5261.486	0.124904	3357.434	0.34993
1000	30.182	0.006	21.868	4	3984.816	10115.24	0.21632	6130.422	0.638945
1000	30.182	0.006	21.868	6	5294.129	12776.41	0.257556	7482.277	0.779842
1000	30.182	0.006	21.868	8	6263.694	14588.46	0.282248	8324.768	0.867651
1000	30.182	0.006	21.868	10	7040.679	15951.86	0.299001	8911.176	0.92877
1000	30.182	0.006	21.868	12	7692.14	17039.14	0.311229	9347.002	0.974194
1000	30.182	0.006	21.868	14	8254.861	17940.07	0.32059	9685.207	1.009444
1000	30.182	0.006	21.868	16	8751.301	18707.1	0.328001	9955.803	1.037646
1000	30.182	0.006	21.868	18	9196.23	19373.51	0.334015	10177.28	1.06073
1000	30.182	0.006	21.868	20	9599.901	19961.67	0.33899	10361.76	1.079958
1000	30.182	0.006	21.868	22	9969.733	20487.3	0.343166	10517.57	1.096197
1000	30.182	0.006	21.868	24	10311.28	20961.9	0.346715	10650.62	1.110064
1000	30.182	0.007	21.868	2	1903.23	5266.977	0.122933	3363.747	0.34733
1000	30.182	0.007	21.868	4	3981.323	10135.82	0.213467	6154.501	0.635494
1000	30.182	0.007	21.868	6	5287.79	12809.5	0.254535	7521.714	0.776667
1000	30.182	0.007	21.868	8	6254.846	14631.84	0.279224	8376.994	0.864981
1000	30.182	0.007	21.868	10	7029.528	16003.93	0.296035	8974.401	0.926667
1000	30.182	0.007	21.868	12	7678.857	17098.75	0.308345	9419.89	0.972667
1000	30.182	0.007	21.868	14	8239.59	18006.32	0.317799	9766.727	1.00848
1000	30.182	0.007	21.868	16	8734.165	18779.3	0.325307	10045.14	1.037228
1000	30.182	0.007	21.868	18	9177.334	19451.1	0.33142	10273.77	1.060836

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	30.182	0.007	21.868	20	9579.335	20044.18	0.336492	10464.85	1.080566
1000	30.182	0.007	21.868	22	9947.578	20574.36	0.340765	10626.78	1.097286
1000	30.182	0.007	21.868	24	10287.61	21053.17	0.344409	10765.56	1.111616
1000	30.182	0.008	21.868	2	1902.425	5272.199	0.121021	3369.775	0.344748
1000	30.182	0.008	21.868	4	3977.902	10155.46	0.210678	6177.56	0.632001
1000	30.182	0.008	21.868	6	5281.594	12841.13	0.251568	7559.537	0.773386
1000	30.182	0.008	21.868	8	6246.206	14673.34	0.276243	8427.138	0.862147
1000	30.182	0.008	21.868	10	7018.645	16053.8	0.293099	9035.154	0.92435
1000	30.182	0.008	21.868	12	7665.901	17155.87	0.305481	9489.974	0.970881
1000	30.182	0.008	21.868	14	8224.701	18069.85	0.315019	9845.154	1.007218
1000	30.182	0.008	21.868	16	8717.464	18848.59	0.322615	10131.12	1.036474
1000	30.182	0.008	21.868	18	9158.924	19525.59	0.328818	10366.67	1.060572
1000	30.182	0.008	21.868	20	9559.305	20123.44	0.33398	10564.13	1.080774
1000	30.182	0.008	21.868	22	9926.007	20658	0.338342	10732	1.097947
1000	30.182	0.008	21.868	24	10264.56	21140.89	0.342073	10876.33	1.112713
1000	31.182	0.004	22.868	2	1903.027	5255.872	0.125779	3352.845	0.345135
1000	31.182	0.004	22.868	4	3980.653	10094.85	0.21751	6114.199	0.629383
1000	31.182	0.004	22.868	6	5287.292	12744.27	0.258773	7456.976	0.767605
1000	31.182	0.004	22.868	8	6254.503	14546.93	0.283439	8292.424	0.853604
1000	31.182	0.004	22.868	10	7029.439	15902.54	0.300152	8873.104	0.913378
1000	31.182	0.004	22.868	12	7679.083	16983.21	0.312335	9304.125	0.957747
1000	31.182	0.004	22.868	14	8240.172	17878.37	0.321651	9638.201	0.992136
1000	31.182	0.004	22.868	16	8735.131	18640.32	0.329019	9905.187	1.019619
1000	31.182	0.004	22.868	18	9178.703	19302.17	0.334991	10123.47	1.042088
1000	31.182	0.004	22.868	20	9581.119	19886.19	0.339925	10305.07	1.060782
1000	31.182	0.004	22.868	22	9949.786	20408.06	0.344063	10458.27	1.076552
1000	31.182	0.004	22.868	24	10290.24	20879.2	0.347576	10588.95	1.090004
1000	31.182	0.005	22.868	2	1902.225	5261.641	0.123785	3359.416	0.342637
1000	31.182	0.005	22.868	4	3977.245	10116.37	0.214639	6139.124	0.626147
1000	31.182	0.005	22.868	6	5281.091	12778.76	0.255744	7497.665	0.764709
1000	31.182	0.005	22.868	8	6245.846	14592.04	0.280415	8346.193	0.851253
1000	31.182	0.005	22.868	10	7018.522	15956.61	0.297191	8938.091	0.911622
1000	31.182	0.005	22.868	12	7666.074	17045.02	0.309462	9378.947	0.956586
1000	31.182	0.005	22.868	14	8225.211	17947.01	0.318876	9721.797	0.991555
1000	31.182	0.005	22.868	16	8718.337	18715.05	0.326345	9996.716	1.019594
1000	31.182	0.005	22.868	18	9160.178	19382.42	0.332419	10222.24	1.042597
1000	31.182	0.005	22.868	20	9560.953	19971.48	0.337455	10410.53	1.061801
1000	31.182	0.005	22.868	22	9928.057	20497.99	0.341692	10569.93	1.078059
1000	31.182	0.005	22.868	24	10267.02	20973.43	0.345302	10706.41	1.091978
1000	31.182	0.006	22.868	2	1901.439	5267.121	0.121851	3365.682	0.340153

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	31.182	0.006	22.868	4	3973.905	10136.88	0.211833	6162.971	0.622862
1000	31.182	0.006	22.868	6	5275.031	12811.69	0.252768	7536.662	0.761694
1000	31.182	0.006	22.868	8	6237.39	14635.18	0.277431	8397.788	0.848724
1000	31.182	0.006	22.868	10	7007.865	16008.37	0.294259	9000.507	0.909638
1000	31.182	0.006	22.868	12	7653.382	17104.24	0.306607	9450.861	0.955153
1000	31.182	0.006	22.868	14	8210.621	18012.81	0.316109	9802.191	0.990661
1000	31.182	0.006	22.868	16	8701.967	18786.75	0.323669	10084.78	1.019221
1000	31.182	0.006	22.868	18	9142.127	19459.45	0.329837	10317.32	1.042722
1000	31.182	0.006	22.868	20	9541.309	20053.39	0.334966	10512.08	1.062406
1000	31.182	0.006	22.868	22	9906.896	20584.38	0.339295	10677.49	1.079123
1000	31.182	0.006	22.868	24	10244.41	21063.98	0.342995	10819.57	1.093483
1000	31.182	0.007	22.868	2	1900.667	5272.332	0.119974	3371.664	0.337686
1000	31.182	0.007	22.868	4	3970.631	10156.44	0.209089	6185.809	0.619535
1000	31.182	0.007	22.868	6	5269.105	12843.17	0.249844	7574.068	0.758575
1000	31.182	0.007	22.868	8	6229.128	14676.46	0.274489	8447.334	0.846036
1000	31.182	0.007	22.868	10	6997.46	16057.95	0.291357	9060.495	0.907447
1000	31.182	0.007	22.868	12	7640.995	17161.02	0.303772	9520.024	0.953471
1000	31.182	0.007	22.868	14	8196.388	18075.94	0.313352	9879.551	0.989479
1000	31.182	0.007	22.868	16	8686.003	18855.56	0.320996	10169.56	1.018525
1000	31.182	0.007	22.868	18	9124.53	19533.42	0.327249	10408.89	1.042495
1000	31.182	0.007	22.868	20	9522.165	20132.08	0.332464	10609.91	1.062628
1000	31.182	0.007	22.868	22	9886.278	20667.42	0.336878	10781.14	1.079777
1000	31.182	0.007	22.868	24	10222.38	21151.05	0.340661	10928.66	1.094552
1000	31.182	0.008	22.868	2	1899.911	5277.293	0.118151	3377.382	0.335237
1000	31.182	0.008	22.868	4	3967.421	10175.12	0.206407	6207.7	0.616173
1000	31.182	0.008	22.868	6	5263.308	12873.28	0.246973	7609.976	0.755363
1000	31.182	0.008	22.868	8	6221.053	14716	0.271588	8494.947	0.843204
1000	31.182	0.008	22.868	10	6987.296	16105.48	0.288488	9118.188	0.905067
1000	31.182	0.008	22.868	12	7628.901	17215.48	0.30096	9586.582	0.95156
1000	31.182	0.008	22.868	14	8182.498	18136.53	0.31061	9954.037	0.988033
1000	31.182	0.008	22.868	16	8670.429	18921.66	0.31833	10251.23	1.017532
1000	31.182	0.008	22.868	18	9107.369	19604.5	0.324661	10497.13	1.04194
1000	31.182	0.008	22.868	20	9503.499	20207.72	0.329954	10704.22	1.062495
1000	31.182	0.008	22.868	22	9866.182	20747.27	0.334446	10881.08	1.080051
1000	31.182	0.008	22.868	24	10200.92	21234.8	0.338306	11033.88	1.095218
1000	32.182	0.004	23.868	2	1900.475	5261.797	0.122685	3361.322	0.335642
1000	32.182	0.004	23.868	4	3969.993	10117.49	0.212979	6147.501	0.613854
1000	32.182	0.004	23.868	6	5268.595	12781.09	0.253948	7512.494	0.750154
1000	32.182	0.004	23.868	8	6228.736	14595.58	0.278594	8366.848	0.835465
1000	32.182	0.004	23.868	10	6997.278	15961.32	0.295387	8964.046	0.895098
1000	32.182	0.004	23.868	12	7641.08	17050.84	0.307696	9409.759	0.939604
1000	32.182	0.004	23.868	14	8196.778	17953.87	0.317158	9757.096	0.974287

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	32.182	0.004	23.868	16	8686.723	18722.91	0.32468	10036.19	1.002156
1000	32.182	0.004	23.868	18	9125.599	19391.22	0.33081	10265.62	1.025066
1000	32.182	0.004	23.868	20	9523.594	19981.19	0.335902	10457.59	1.044235
1000	32.182	0.004	23.868	22	9888.077	20508.55	0.340197	10620.47	1.060499
1000	32.182	0.004	23.868	24	10224.56	20984.81	0.343864	10760.25	1.074456
1000	32.182	0.005	23.868	2	1899.722	5267.265	0.120786	3367.543	0.333268
1000	32.182	0.005	23.868	4	3966.795	10137.92	0.210219	6171.126	0.610724
1000	32.182	0.005	23.868	6	5262.796	12813.87	0.251016	7551.07	0.74729
1000	32.182	0.005	23.868	8	6220.648	14638.49	0.275649	8417.839	0.83307
1000	32.182	0.005	23.868	10	6987.086	16012.77	0.29249	9025.688	0.893226
1000	32.182	0.005	23.868	12	7628.943	17109.69	0.30487	9480.742	0.93826
1000	32.182	0.005	23.868	14	8182.828	18019.24	0.314415	9836.412	0.973459
1000	32.182	0.005	23.868	16	8671.072	18794.11	0.322024	10123.04	1.001825
1000	32.182	0.005	23.868	18	9108.342	19467.7	0.328242	10359.36	1.025212
1000	32.182	0.005	23.868	20	9504.815	20062.49	0.333423	10557.67	1.044838
1000	32.182	0.005	23.868	22	9867.848	20594.29	0.337806	10726.45	1.061541
1000	32.182	0.005	23.868	24	10202.95	21074.67	0.341559	10871.72	1.075918
1000	32.182	0.006	23.868	2	1898.983	5272.465	0.118943	3373.482	0.330909
1000	32.182	0.006	23.868	4	3963.66	10157.41	0.20752	6193.753	0.607552
1000	32.182	0.006	23.868	6	5257.123	12845.2	0.248135	7588.077	0.744323
1000	32.182	0.006	23.868	8	6212.74	14679.55	0.272745	8466.814	0.830519
1000	32.182	0.006	23.868	10	6977.129	16062.07	0.289622	9084.944	0.891153
1000	32.182	0.006	23.868	12	7617.091	17166.12	0.302064	9549.024	0.936675
1000	32.182	0.006	23.868	14	8169.211	18081.96	0.311683	9912.753	0.972353
1000	32.182	0.006	23.868	16	8655.8	18862.47	0.319371	10206.67	1.001184
1000	32.182	0.006	23.868	18	9091.509	19541.17	0.325671	10449.66	1.025019
1000	32.182	0.006	23.868	20	9486.502	20140.62	0.330933	10654.12	1.045075
1000	32.182	0.006	23.868	22	9848.128	20676.73	0.335396	10828.6	1.06219
1000	32.182	0.006	23.868	24	10181.88	21161.09	0.339228	10979.21	1.076963
1000	32.182	0.007	23.868	2	1898.257	5277.416	0.117152	3379.159	0.328565
1000	32.182	0.007	23.868	4	3960.584	10176.03	0.20488	6215.444	0.604345
1000	32.182	0.007	23.868	6	5251.572	12875.18	0.245305	7623.606	0.741264
1000	32.182	0.007	23.868	8	6205.008	14718.89	0.269882	8513.885	0.827828
1000	32.182	0.007	23.868	10	6967.398	16109.34	0.286786	9141.943	0.888896
1000	32.182	0.007	23.868	12	7605.514	17220.26	0.299282	9614.747	0.934868
1000	32.182	0.007	23.868	14	8155.915	18142.19	0.308966	9986.271	0.970993
1000	32.182	0.007	23.868	16	8640.892	18928.14	0.316725	10287.25	1.000257
1000	32.182	0.007	23.868	18	9075.084	19611.77	0.323099	10536.69	1.024511
1000	32.182	0.007	23.868	20	9468.638	20215.75	0.328436	10747.11	1.044971
1000	32.182	0.007	23.868	22	9828.895	20756.02	0.332973	10927.12	1.062474
1000	32.182	0.007	23.868	24	10161.34	21244.25	0.336879	11082.91	1.077621
1000	32.182	0.008	23.868	2	1897.545	5282.136	0.115413	3384.59	0.326238

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	32.182	0.008	23.868	4	3957.566	10193.82	0.202299	6236.257	0.601108
1000	32.182	0.008	23.868	6	5246.138	12903.88	0.242525	7657.744	0.738124
1000	32.182	0.008	23.868	8	6197.445	14756.6	0.267061	8559.158	0.825011
1000	32.182	0.008	23.868	10	6957.885	16154.69	0.283983	9196.807	0.886473
1000	32.182	0.008	23.868	12	7594.2	17272.25	0.296524	9678.047	0.93286
1000	32.182	0.008	23.868	14	8142.927	18200.04	0.306266	10057.11	0.969398
1000	32.182	0.008	23.868	16	8626.336	18991.26	0.31409	10364.92	0.999067
1000	32.182	0.008	23.868	18	9059.049	19679.67	0.320531	10620.62	1.023714
1000	32.182	0.008	23.868	20	9451.205	20288.01	0.325937	10836.81	1.044552
1000	32.182	0.008	23.868	22	9810.131	20832.32	0.330542	11022.19	1.062421
1000	32.182	0.008	23.868	24	10141.31	21324.3	0.334515	11182.99	1.07792
1200	28.182	0.004	19.868	2	1911.75	6289.817	0.13748	4378.068	0.496684
1200	28.182	0.004	19.868	4	4019.985	12047.12	0.237731	8027.131	0.910663
1200	28.182	0.004	19.868	6	5351.587	15184.08	0.283228	9832.497	1.115479
1200	28.182	0.004	19.868	8	6343.236	17311.75	0.310602	10968.52	1.244358
1200	28.182	0.004	19.868	10	7140.309	18907.99	0.32931	11767.68	1.335021
1200	28.182	0.004	19.868	12	7810.211	20178.04	0.343072	12367.82	1.403107
1200	28.182	0.004	19.868	14	8390.012	21228.39	0.353695	12838.38	1.45649
1200	28.182	0.004	19.868	16	8902.391	22121.19	0.362178	13218.8	1.499648
1200	28.182	0.004	19.868	18	9362.289	22895.76	0.369124	13533.47	1.535347
1200	28.182	0.004	19.868	20	9780.093	23578.51	0.374925	13798.41	1.565404
1200	28.182	0.004	19.868	22	10163.33	24187.98	0.379843	14024.65	1.591071
1200	28.182	0.004	19.868	24	10517.64	24737.72	0.384066	14220.08	1.613242
1200	28.182	0.005	19.868	2	1910.77	6299.167	0.134774	4388.396	0.492824
1200	28.182	0.005	19.868	4	4015.632	12081.97	0.233829	8066.339	0.905862
1200	28.182	0.005	19.868	6	5343.899	15239.89	0.279076	9895.989	1.111334
1200	28.182	0.005	19.868	8	6332.464	17384.68	0.306424	11052.21	1.24118
1200	28.182	0.005	19.868	10	7126.69	18995.33	0.325186	11868.64	1.332866
1200	28.182	0.005	19.868	12	7793.946	20277.82	0.339035	12483.88	1.401958
1200	28.182	0.005	19.868	14	8371.27	21339.13	0.349759	12967.86	1.45631
1200	28.182	0.005	19.868	16	8881.321	22241.71	0.358349	13360.39	1.500392
1200	28.182	0.005	19.868	18	9339.015	23025.12	0.365405	13686.11	1.53697
1200	28.182	0.005	19.868	20	9754.723	23715.93	0.371315	13961.21	1.567865
1200	28.182	0.005	19.868	22	10135.96	24332.83	0.376341	14196.87	1.59433
1200	28.182	0.005	19.868	24	10488.36	24889.44	0.38067	14401.08	1.617263
1200	28.182	0.006	19.868	2	1909.812	6307.927	0.132168	4398.115	0.488973
1200	28.182	0.006	19.868	4	4011.383	12114.77	0.230034	8103.384	0.900917
1200	28.182	0.006	19.868	6	5336.406	15292.53	0.275016	9956.128	1.106901
1200	28.182	0.006	19.868	8	6321.974	17453.6	0.30232	11131.62	1.237589
1200	28.182	0.006	19.868	10	7113.437	19077.98	0.321118	11964.55	1.330192
1200	28.182	0.006	19.868	12	7778.128	20372.36	0.335038	12594.23	1.400199
1200	28.182	0.006	19.868	14	8353.056	21444.14	0.34585	13091.08	1.455438

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1200	28.182	0.006	19.868	16	8860.851	22356.08	0.354535	13495.23	1.500371
1200	28.182	0.006	19.868	18	9316.414	23147.97	0.361688	13831.55	1.537762
1200	28.182	0.006	19.868	20	9730.099	23846.52	0.367696	14116.42	1.569433
1200	28.182	0.006	19.868	22	10109.41	24470.55	0.372819	14361.14	1.596664
1200	28.182	0.006	19.868	24	10459.95	25033.76	0.377244	14573.8	1.620284
1200	28.182	0.007	19.868	2	1908.874	6316.151	0.129656	4407.277	0.485137
1200	28.182	0.007	19.868	4	4007.234	12145.68	0.226346	8138.441	0.89585
1200	28.182	0.007	19.868	6	5329.098	15342.26	0.271047	10013.17	1.102213
1200	28.182	0.007	19.868	8	6311.755	17518.81	0.298291	11207.05	1.233632
1200	28.182	0.007	19.868	10	7100.535	19156.29	0.31711	12055.75	1.327054
1200	28.182	0.007	19.868	12	7762.739	20462.01	0.331087	12699.27	1.39789
1200	28.182	0.007	19.868	14	8335.344	21543.8	0.341973	13208.46	1.45394
1200	28.182	0.007	19.868	16	8840.956	22464.72	0.350741	13623.76	1.499655
1200	28.182	0.007	19.868	18	9294.456	23264.73	0.357981	13970.27	1.537797
1200	28.182	0.007	19.868	20	9706.183	23970.71	0.364076	14264.53	1.570188
1200	28.182	0.007	19.868	22	10083.62	24601.58	0.369287	14517.95	1.598084
1200	28.182	0.007	19.868	24	10432.39	25171.14	0.373799	14738.75	1.622388
1200	28.182	0.008	19.868	2	1907.955	6323.884	0.127234	4415.929	0.481321
1200	28.182	0.008	19.868	4	4003.182	12174.85	0.222759	8171.664	0.890683
1200	28.182	0.008	19.868	6	5321.97	15389.3	0.267169	10067.33	1.097305
1200	28.182	0.008	19.868	8	6301.795	17580.58	0.294338	11278.79	1.229349
1200	28.182	0.008	19.868	10	7087.969	19230.55	0.313165	12142.59	1.3235
1200	28.182	0.008	19.868	12	7747.759	20547.12	0.327187	12799.36	1.395086
1200	28.182	0.008	19.868	14	8318.112	21638.49	0.338135	13320.38	1.451876
1200	28.182	0.008	19.868	16	8821.609	22568	0.346974	13746.39	1.498309
1200	28.182	0.008	19.868	18	9273.112	23375.79	0.354291	14102.68	1.537144
1200	28.182	0.008	19.868	20	9682.943	24088.9	0.360464	14405.96	1.5702
1200	28.182	0.008	19.868	22	10058.58	24726.35	0.365754	14667.77	1.598736
1200	28.182	0.008	19.868	24	10405.62	25302	0.370344	14896.39	1.623655
1400	28.182	0.004	19.868	2	1911.75	7345.775	0.137819	5434.025	0.61648
1400	28.182	0.004	19.868	4	4019.985	14082.51	0.240358	10062.53	1.141575
1400	28.182	0.004	19.868	6	5351.587	17758.7	0.287877	12407.11	1.407563
1400	28.182	0.004	19.868	8	6343.236	20254.38	0.316953	13911.14	1.578193
1400	28.182	0.004	19.868	10	7140.309	22127.94	0.337127	14987.63	1.700318
1400	28.182	0.004	19.868	12	7810.211	23619.4	0.352182	15809.19	1.793523
1400	28.182	0.004	19.868	14	8390.012	24853.39	0.363964	16463.38	1.86774
1400	28.182	0.004	19.868	16	8902.391	25902.65	0.3735	17000.26	1.928648
1400	28.182	0.004	19.868	18	9362.289	26813.23	0.381414	17450.94	1.979777
1400	28.182	0.004	19.868	20	9780.093	27616.08	0.38811	17835.99	2.02346
1400	28.182	0.004	19.868	22	10163.33	28332.95	0.393865	18169.62	2.06131
1400	28.182	0.004	19.868	24	10517.64	28979.68	0.398873	18462.05	2.094485
1400	28.182	0.005	19.868	2	1910.77	7357.83	0.134762	5447.06	0.611713

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1400	28.182	0.005	19.868	4	4015.632	14127.8	0.235852	10112.17	1.135612
1400	28.182	0.005	19.868	6	5343.899	17831.38	0.283001	12487.48	1.402363
1400	28.182	0.005	19.868	8	6332.464	20349.5	0.311973	14017.04	1.574134
1400	28.182	0.005	19.868	10	7126.69	22241.99	0.332144	15115.3	1.697471
1400	28.182	0.005	19.868	12	7793.946	23749.82	0.347239	15955.87	1.791869
1400	28.182	0.005	19.868	14	8371.27	24998.22	0.359083	16626.95	1.867231
1400	28.182	0.005	19.868	16	8881.321	26060.37	0.368693	17179.05	1.929233
1400	28.182	0.005	19.868	18	9339.015	26982.61	0.376686	17643.59	1.981402
1400	28.182	0.005	19.868	20	9754.723	27796.11	0.383465	18041.38	2.026074
1400	28.182	0.005	19.868	22	10135.96	28522.77	0.389303	18386.81	2.064866
1400	28.182	0.005	19.868	24	10488.36	29178.58	0.394393	18690.23	2.098941
1400	28.182	0.006	19.868	2	1909.812	7369.033	0.131832	5459.221	0.606944
1400	28.182	0.006	19.868	4	4011.383	14170.06	0.231491	10158.68	1.12942
1400	28.182	0.006	19.868	6	5336.406	17899.38	0.278255	12562.98	1.396724
1400	28.182	0.006	19.868	8	6321.974	20438.66	0.307106	14116.69	1.569463
1400	28.182	0.006	19.868	10	7113.437	22349.05	0.327255	15235.61	1.693862
1400	28.182	0.006	19.868	12	7778.128	23872.38	0.342375	16094.26	1.789324
1400	28.182	0.006	19.868	14	8353.056	25134.47	0.354267	16781.41	1.865721
1400	28.182	0.006	19.868	16	8860.851	26208.87	0.363937	17348.02	1.928714
1400	28.182	0.006	19.868	18	9316.414	27142.21	0.371998	17825.79	1.981833
1400	28.182	0.006	19.868	20	9730.099	27965.85	0.378847	18235.75	2.027411
1400	28.182	0.006	19.868	22	10109.41	28701.86	0.384757	18592.45	2.067069
1400	28.182	0.006	19.868	24	10459.95	29366.34	0.389921	18906.39	2.101971
1400	28.182	0.007	19.868	2	1908.874	7379.469	0.129022	5470.595	0.602183
1400	28.182	0.007	19.868	4	4007.234	14209.56	0.227269	10202.33	1.123035
1400	28.182	0.007	19.868	6	5329.098	17963.1	0.273637	12634.01	1.390706
1400	28.182	0.007	19.868	8	6311.755	20522.37	0.30235	14210.61	1.564253
1400	28.182	0.007	19.868	10	7100.535	22449.69	0.322463	15349.15	1.68958
1400	28.182	0.007	19.868	12	7762.739	23987.73	0.337593	16224.99	1.785988
1400	28.182	0.007	19.868	14	8335.344	25262.81	0.349521	16927.46	1.863314
1400	28.182	0.007	19.868	16	8840.956	26348.86	0.35924	17507.9	1.927206
1400	28.182	0.007	19.868	18	9294.456	27292.76	0.367357	17998.31	1.981189
1400	28.182	0.007	19.868	20	9706.183	28126.07	0.374267	18419.89	2.027595
1400	28.182	0.007	19.868	22	10083.62	28871	0.380239	18787.38	2.068047
1400	28.182	0.007	19.868	24	10432.39	29543.76	0.385466	19111.37	2.103711
1400	28.182	0.008	19.868	2	1907.955	7389.21	0.126324	5481.254	0.597438
1400	28.182	0.008	19.868	4	4003.182	14246.56	0.223183	10243.37	1.116493
1400	28.182	0.008	19.868	6	5321.97	18022.92	0.269144	12700.95	1.38436
1400	28.182	0.008	19.868	8	6301.795	20601.06	0.297707	14299.27	1.558571
1400	28.182	0.008	19.868	10	7087.969	22544.43	0.31777	15456.46	1.684701
1400	28.182	0.008	19.868	12	7747.759	24096.42	0.332899	16348.66	1.781948
1400	28.182	0.008	19.868	14	8318.112	25383.85	0.34485	17065.73	1.860107
1400	28.182	0.008	19.868	16	8821.609	26480.98	0.354607	17659.37	1.924811

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1400	28.182	0.008	19.868	18	9273.112	27434.95	0.36277	18161.84	1.979578
1400	28.182	0.008	19.868	20	9682.943	28277.48	0.369731	18594.53	2.02674
1400	28.182	0.008	19.868	22	10058.58	29030.91	0.375757	18972.33	2.067919
1400	28.182	0.008	19.868	24	10405.62	29711.57	0.38104	19305.95	2.104283
1600	28.182	0.004	19.868	2	1911.75	8403.867	0.137598	6492.117	0.736519
1600	28.182	0.004	19.868	4	4019.985	16124.72	0.241439	12104.74	1.37326
1600	28.182	0.004	19.868	6	5351.587	20344.09	0.290239	14992.5	1.700871
1600	28.182	0.004	19.868	8	6343.236	23211.07	0.320421	16867.83	1.913624
1600	28.182	0.004	19.868	10	7140.309	25364.75	0.341559	18224.44	2.067528
1600	28.182	0.004	19.868	12	7810.211	27080.06	0.357466	19269.85	2.186129
1600	28.182	0.004	19.868	14	8390.012	28499.83	0.370013	20109.82	2.281422
1600	28.182	0.004	19.868	16	8902.391	29707.47	0.380245	20805.08	2.360298
1600	28.182	0.004	19.868	18	9362.289	30755.82	0.388799	21393.53	2.427057
1600	28.182	0.004	19.868	20	9780.093	31680.38	0.396089	21900.29	2.484547
1600	28.182	0.004	19.868	22	10163.33	32506.11	0.402397	22342.78	2.534747
1600	28.182	0.004	19.868	24	10517.64	33251.22	0.407924	22733.58	2.579083
1600	28.182	0.005	19.868	2	1910.77	8418.733	0.134212	6507.963	0.730854
1600	28.182	0.005	19.868	4	4015.632	16181.21	0.236373	12165.58	1.366213
1600	28.182	0.005	19.868	6	5343.899	20434.98	0.284697	15091.08	1.694751
1600	28.182	0.005	19.868	8	6332.464	23330.2	0.314709	16997.74	1.908871
1600	28.182	0.005	19.868	10	7126.69	25507.73	0.335794	18381.05	2.064219
1600	28.182	0.005	19.868	12	7793.946	27243.7	0.351704	19449.75	2.184237
1600	28.182	0.005	19.868	14	8371.27	28681.68	0.364283	20310.41	2.28089
1600	28.182	0.005	19.868	16	8881.321	29905.62	0.374563	21024.3	2.361061
1600	28.182	0.005	19.868	18	9339.015	30968.73	0.383173	21629.71	2.429049
1600	28.182	0.005	19.868	20	9754.723	31906.77	0.390525	22152.04	2.487708
1600	28.182	0.005	19.868	22	10135.96	32744.92	0.396897	22608.95	2.53902
1600	28.182	0.005	19.868	24	10488.36	33501.53	0.40249	23013.18	2.584415
1600	28.182	0.006	19.868	2	1909.812	8432.453	0.130982	6522.641	0.725173
1600	28.182	0.006	19.868	4	4011.383	16233.49	0.23149	12222.11	1.358827
1600	28.182	0.006	19.868	6	5336.406	20519.33	0.279325	15182.93	1.688005
1600	28.182	0.006	19.868	8	6321.974	23440.98	0.309148	17119	1.903254
1600	28.182	0.006	19.868	10	7113.437	25640.91	0.330163	18527.47	2.059844
1600	28.182	0.006	19.868	12	7778.128	27396.3	0.346059	19618.17	2.181106
1600	28.182	0.006	19.868	14	8353.056	28851.45	0.358655	20498.39	2.278966
1600	28.182	0.006	19.868	16	8860.851	30090.77	0.368969	21229.92	2.360296
1600	28.182	0.006	19.868	18	9316.414	31167.82	0.377624	21851.41	2.429392
1600	28.182	0.006	19.868	20	9730.099	32118.63	0.385025	22388.53	2.489108
1600	28.182	0.006	19.868	22	10109.41	32968.54	0.391451	22859.14	2.541429
1600	28.182	0.006	19.868	24	10459.95	33736.08	0.397099	23276.12	2.587789
1600	28.182	0.007	19.868	2	1908.874	8445.147	0.127899	6536.273	0.719489

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1600	28.182	0.007	19.868	4	4007.234	16281.99	0.226784	12274.75	1.351161
1600	28.182	0.007	19.868	6	5329.098	20597.78	0.274119	15268.68	1.680721
1600	28.182	0.007	19.868	8	6311.755	23544.2	0.303738	17232.44	1.896885
1600	28.182	0.007	19.868	10	7100.535	25765.17	0.324668	18664.63	2.054536
1600	28.182	0.007	19.868	12	7762.739	27538.85	0.340537	19776.11	2.176883
1600	28.182	0.007	19.868	14	8335.344	29010.19	0.353136	20674.85	2.275812
1600	28.182	0.007	19.868	16	8840.956	30264.05	0.363472	21423.09	2.358177
1600	28.182	0.007	19.868	18	9294.456	31354.29	0.372159	22059.83	2.428267
1600	28.182	0.007	19.868	20	9706.183	32317.17	0.3796	22610.99	2.488936
1600	28.182	0.007	19.868	22	10083.62	33178.24	0.386069	23094.61	2.542172
1600	28.182	0.007	19.868	24	10432.39	33956.13	0.391764	23523.74	2.589409
1600	28.182	0.008	19.868	2	1907.955	8456.923	0.124952	6548.967	0.713815
1600	28.182	0.008	19.868	4	4003.182	16327.09	0.222248	12323.9	1.343263
1600	28.182	0.008	19.868	6	5321.97	20670.9	0.269075	15348.93	1.67298
1600	28.182	0.008	19.868	8	6301.795	23640.56	0.298478	17338.77	1.889866
1600	28.182	0.008	19.868	10	7087.969	25881.32	0.31931	18793.36	2.048411
1600	28.182	0.008	19.868	12	7747.759	27672.25	0.335139	19924.49	2.171701
1600	28.182	0.008	19.868	14	8318.112	29158.86	0.34773	20840.75	2.271571
1600	28.182	0.008	19.868	16	8821.609	30426.46	0.358077	21604.85	2.354854
1600	28.182	0.008	19.868	18	9273.112	31529.18	0.366786	22256.07	2.425835
1600	28.182	0.008	19.868	20	9682.943	32503.51	0.374257	22820.56	2.487363
1600	28.182	0.008	19.868	22	10058.58	33375.14	0.380761	23316.56	2.541426
1600	28.182	0.008	19.868	24	10405.62	34162.86	0.386494	23757.24	2.589458
1800	28.182	0.004	19.868	2	1911.75	9464.196	0.137057	7552.446	0.856811
1800	28.182	0.004	19.868	4	4019.985	18173.52	0.241616	14153.53	1.605692
1800	28.182	0.004	19.868	6	5351.587	22939.79	0.291261	17588.2	1.995349
1800	28.182	0.004	19.868	8	6343.236	26181.17	0.322199	19837.93	2.250577
1800	28.182	0.004	19.868	10	7140.309	28617.61	0.344004	21477.3	2.43656
1800	28.182	0.004	19.868	12	7810.211	30559.08	0.360506	22748.87	2.580817
1800	28.182	0.004	19.868	14	8390.012	32166.67	0.373591	23776.66	2.697418
1800	28.182	0.004	19.868	16	8902.391	33534.54	0.384314	24632.15	2.794472
1800	28.182	0.004	19.868	18	9362.289	34722.32	0.39332	25360.03	2.877049
1800	28.182	0.004	19.868	20	9780.093	35770.12	0.401028	25990.02	2.94852
1800	28.182	0.004	19.868	22	10163.33	36706.13	0.407727	26542.8	3.011231
1800	28.182	0.004	19.868	24	10517.64	37550.92	0.413622	27033.28	3.066875
1800	28.182	0.005	19.868	2	1910.77	9481.878	0.13336	7571.107	0.850247
1800	28.182	0.005	19.868	4	4015.632	18241.79	0.236022	14226.16	1.597619
1800	28.182	0.005	19.868	6	5343.899	23049.96	0.285093	17706.06	1.988417
1800	28.182	0.005	19.868	8	6332.464	26325.8	0.3158	19993.33	2.245282
1800	28.182	0.005	19.868	10	7126.69	28791.39	0.33751	21664.7	2.432979
1800	28.182	0.005	19.868	12	7793.946	30758.13	0.353982	22964.18	2.578912
1800	28.182	0.005	19.868	14	8371.27	32388.02	0.367073	24016.75	2.697117

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1800	28.182	0.005	19.868	16	8881.321	33775.86	0.377821	24894.54	2.795695
1800	28.182	0.005	19.868	18	9339.015	34981.75	0.386864	25642.73	2.879717
1800	28.182	0.005	19.868	20	9754.723	36046.09	0.394618	26291.37	2.95256
1800	28.182	0.005	19.868	22	10135.96	36997.35	0.401366	26861.39	3.016574
1800	28.182	0.005	19.868	24	10488.36	37856.28	0.407312	27367.93	3.07346
1800	28.182	0.006	19.868	2	1909.812	9498.106	0.12985	7588.294	0.84365
1800	28.182	0.006	19.868	4	4011.383	18304.48	0.230653	14293.1	1.589076
1800	28.182	0.006	19.868	6	5336.406	23151.42	0.279138	17815.01	1.980634
1800	28.182	0.006	19.868	8	6321.974	26459.27	0.309596	20137.29	2.23882
1800	28.182	0.006	19.868	10	7113.437	28952.03	0.331193	21838.59	2.427967
1800	28.182	0.006	19.868	12	7778.128	30942.36	0.347618	23164.23	2.575349
1800	28.182	0.006	19.868	14	8353.056	32593.13	0.360698	24240.08	2.694959
1800	28.182	0.006	19.868	16	8860.851	33999.7	0.371458	25138.85	2.794882
1800	28.182	0.006	19.868	18	9316.414	35222.57	0.380525	25906.16	2.88019
1800	28.182	0.006	19.868	20	9730.099	36302.47	0.388311	26572.38	2.954259
1800	28.182	0.006	19.868	22	10109.41	37268.09	0.395097	27158.68	3.019443
1800	28.182	0.006	19.868	24	10459.95	38140.35	0.401084	27680.4	3.077446
1800	28.182	0.007	19.868	2	1908.874	9513.043	0.126514	7604.169	0.83704
1800	28.182	0.007	19.868	4	4007.234	18362.23	0.2255	14355	1.580147
1800	28.182	0.007	19.868	6	5329.098	23245.1	0.273391	17916	1.972129
1800	28.182	0.007	19.868	8	6311.755	26582.74	0.303585	20270.99	2.231357
1800	28.182	0.007	19.868	10	7100.535	29100.85	0.325053	22000.32	2.421716
1800	28.182	0.007	19.868	12	7762.739	31113.25	0.341417	23350.51	2.57034
1800	28.182	0.007	19.868	14	8335.344	32783.58	0.354473	24448.24	2.691174
1800	28.182	0.007	19.868	16	8840.956	34207.72	0.365231	25366.76	2.792282
1800	28.182	0.007	19.868	18	9294.456	35446.56	0.37431	26152.1	2.878729
1800	28.182	0.007	19.868	20	9706.183	36541.09	0.382118	26834.91	2.95389
1800	28.182	0.007	19.868	22	10083.62	37520.22	0.388932	27436.6	3.020122
1800	28.182	0.007	19.868	24	10432.39	38405.05	0.394951	27972.66	3.079129
1800	28.182	0.008	19.868	2	1907.955	9526.829	0.123341	7618.874	0.830431
1800	28.182	0.008	19.868	4	4003.182	18415.58	0.220553	14412.4	1.570902
1800	28.182	0.008	19.868	6	5321.97	23331.83	0.267845	18009.86	1.963014
1800	28.182	0.008	19.868	8	6301.795	26697.24	0.297763	20395.45	2.223034
1800	28.182	0.008	19.868	10	7087.969	29239.04	0.31909	22151.07	2.414391
1800	28.182	0.008	19.868	12	7747.759	31272.1	0.33538	23524.34	2.564073
1800	28.182	0.008	19.868	14	8318.112	32960.77	0.3484	24642.66	2.685965
1800	28.182	0.008	19.868	16	8821.609	34401.41	0.359145	25579.8	2.788111
1800	28.182	0.008	19.868	18	9273.112	35655.26	0.368227	26382.14	2.875563
1800	28.182	0.008	19.868	20	9682.943	36763.57	0.376047	27080.62	2.951695
1800	28.182	0.008	19.868	22	10058.58	37755.43	0.382879	27696.85	3.018862
1800	28.182	0.008	19.868	24	10405.62	38652.1	0.388922	28246.48	3.07877

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
2000	28.182	0.004	19.868	2	1911.75	10526.88	0.136322	8615.126	0.97737
2000	28.182	0.004	19.868	4	4019.985	20228.72	0.241225	16208.74	1.838851
2000	28.182	0.004	19.868	6	5351.587	25545.39	0.291435	20193.81	2.29095
2000	28.182	0.004	19.868	8	6343.236	29164.1	0.322906	22820.86	2.588985
2000	28.182	0.004	19.868	10	7140.309	31885.81	0.345191	24745.5	2.807331
2000	28.182	0.004	19.868	12	7810.211	34055.62	0.362126	26245.41	2.977493
2000	28.182	0.004	19.868	14	8390.012	35852.98	0.375604	27462.97	3.115623
2000	28.182	0.004	19.868	16	8902.391	37382.82	0.386688	28480.43	3.231051
2000	28.182	0.004	19.868	18	9362.289	38711.63	0.396026	29349.34	3.329628
2000	28.182	0.004	19.868	20	9780.093	39884.12	0.404044	30104.02	3.415245
2000	28.182	0.004	19.868	22	10163.33	40931.75	0.411032	30768.42	3.49062
2000	28.182	0.004	19.868	24	10517.64	41877.48	0.417198	31359.84	3.557716
2000	28.182	0.005	19.868	2	1910.77	10547.27	0.132328	8636.503	0.969892
2000	28.182	0.005	19.868	4	4015.632	20309.17	0.23513	16293.54	1.829789
2000	28.182	0.005	19.868	6	5343.899	25675.68	0.284674	20331.78	2.283289
2000	28.182	0.005	19.868	8	6332.464	29335.43	0.315857	23002.96	2.583268
2000	28.182	0.005	19.868	10	7126.69	32091.91	0.338007	24965.22	2.803632
2000	28.182	0.005	19.868	12	7793.946	34291.88	0.354883	26497.94	2.975758
2000	28.182	0.005	19.868	14	8371.27	36115.9	0.368343	27744.63	3.115763
2000	28.182	0.005	19.868	16	8881.321	37669.62	0.379432	28788.3	3.23297
2000	28.182	0.005	19.868	18	9339.015	39020.09	0.388791	29681.07	3.333229
2000	28.182	0.005	19.868	20	9754.723	40212.4	0.396839	30457.67	3.420443
2000	28.182	0.005	19.868	22	10135.96	41278.31	0.403863	31142.34	3.497332
2000	28.182	0.005	19.868	24	10488.36	42240.99	0.410069	31752.64	3.565869
2000	28.182	0.006	19.868	2	1909.812	10565.93	0.128555	8656.114	0.962368
2000	28.182	0.006	19.868	4	4011.383	20382.53	0.229305	16371.15	1.820109
2000	28.182	0.006	19.868	6	5336.406	25794.78	0.278172	20458.37	2.274517
2000	28.182	0.006	19.868	8	6321.974	29492.38	0.309049	23170.41	2.576036
2000	28.182	0.006	19.868	10	7113.437	32281.04	0.331046	25167.6	2.798079
2000	28.182	0.006	19.868	12	7778.128	34508.99	0.347844	26730.86	2.971879
2000	28.182	0.006	19.868	14	8353.056	36357.78	0.361269	28004.72	3.113504
2000	28.182	0.006	19.868	16	8860.851	37933.75	0.372348	29072.9	3.232261
2000	28.182	0.006	19.868	18	9316.414	39304.41	0.381714	29988	3.334
2000	28.182	0.006	19.868	20	9730.099	40515.23	0.389779	30785.13	3.422624
2000	28.182	0.006	19.868	22	10109.41	41598.23	0.396828	31488.82	3.500858
2000	28.182	0.006	19.868	24	10459.95	42576.79	0.403063	32116.83	3.570679
2000	28.182	0.007	19.868	2	1908.874	10583.03	0.124985	8674.157	0.95482
2000	28.182	0.007	19.868	4	4007.234	20449.66	0.223737	16442.43	1.809923
2000	28.182	0.007	19.868	6	5329.098	25904.02	0.271921	20574.92	2.264813
2000	28.182	0.007	19.868	8	6311.755	29636.6	0.302478	23324.85	2.567515
2000	28.182	0.007	19.868	10	7100.535	32455.07	0.324307	25354.54	2.790936
2000	28.182	0.007	19.868	12	7762.739	34709.02	0.341012	26946.28	2.966149
2000	28.182	0.007	19.868	14	8335.344	36580.86	0.354388	28245.52	3.109165

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
2000	28.182	0.007	19.868	16	8840.956	38177.57	0.365444	29336.62	3.229269
2000	28.182	0.007	19.868	18	9294.456	39567.09	0.374804	30272.64	3.332303
2000	28.182	0.007	19.868	20	9706.183	40795.21	0.382875	31089.02	3.422168
2000	28.182	0.007	19.868	22	10083.62	41894.19	0.389938	31810.56	3.501592
2000	28.182	0.007	19.868	24	10432.39	42887.61	0.396192	32455.23	3.572554
2000	28.182	0.008	19.868	2	1907.955	10598.76	0.121604	8690.803	0.947268
2000	28.182	0.008	19.868	4	4003.182	20511.3	0.218412	16508.12	1.799329
2000	28.182	0.008	19.868	6	5321.97	26004.52	0.265912	20682.55	2.254327
2000	28.182	0.008	19.868	8	6301.795	29769.5	0.296139	23467.71	2.5579
2000	28.182	0.008	19.868	10	7087.969	32615.66	0.317786	25527.69	2.782431
2000	28.182	0.008	19.868	12	7747.759	34893.78	0.334387	27146.02	2.958823
2000	28.182	0.008	19.868	14	8318.112	36787.11	0.347701	28469	3.103024
2000	28.182	0.008	19.868	16	8821.609	38403.18	0.358724	29581.57	3.22429
2000	28.182	0.008	19.868	18	9273.112	39810.31	0.368067	30537.2	3.328451
2000	28.182	0.008	19.868	20	9682.943	41054.61	0.376134	31371.67	3.419404
2000	28.182	0.008	19.868	22	10058.58	42168.56	0.383201	32109.98	3.499878
2000	28.182	0.008	19.868	24	10405.62	43175.92	0.389466	32770.3	3.57185
1000	28.182	0	19.868	2	1915.892	5204.152	0.146169	3288.26	0.388931
1000	28.182	0	19.868	4	4038.526	9902.444	0.245846	5863.918	0.693577
1000	28.182	0	19.868	6	5384.448	12436.15	0.288094	7051.702	0.834067
1000	28.182	0	19.868	8	6389.404	14144.13	0.312098	7754.728	0.91722
1000	28.182	0	19.868	10	7198.81	15419.92	0.327631	8221.109	0.972383
1000	28.182	0	19.868	12	7880.199	16431.59	0.338449	8551.388	1.011448
1000	28.182	0	19.868	14	8470.777	17265.97	0.346339	8795.197	1.040285
1000	28.182	0	19.868	16	8993.317	17973.57	0.352275	8980.253	1.062174
1000	28.182	0	19.868	18	9462.846	18586.25	0.356836	9123.408	1.079106
1000	28.182	0	19.868	20	9889.819	19125.36	0.36039	9235.546	1.092369
1000	28.182	0	19.868	22	10281.81	19605.89	0.363185	9324.074	1.10284
1000	28.182	0	19.868	24	10644.52	20038.71	0.365391	9394.195	1.111134
1000	29.182	0	20.868	2	1912.505	5213.126	0.142025	3300.621	0.377016
1000	29.182	0	20.868	4	4023.935	9936.038	0.240191	5912.103	0.675314
1000	29.182	0	20.868	6	5359.076	12490.15	0.282355	7131.076	0.814552
1000	29.182	0	20.868	8	6354.239	14214.91	0.306582	7860.675	0.897891
1000	29.182	0	20.868	10	7154.727	15504.9	0.322434	8350.178	0.953805
1000	29.182	0	20.868	12	7827.927	16528.89	0.333601	8700.963	0.993873
1000	29.182	0	20.868	14	8410.903	17374.14	0.341847	8963.241	1.023832
1000	29.182	0	20.868	16	8926.351	18091.48	0.348136	9165.133	1.046893
1000	29.182	0	20.868	18	9389.209	18713	0.353043	9323.793	1.065016
1000	29.182	0	20.868	20	9809.882	19260.19	0.356934	9450.313	1.079468
1000	29.182	0	20.868	22	10195.9	19748.17	0.360055	9552.267	1.091114
1000	29.182	0	20.868	24	10552.91	20187.9	0.362578	9634.995	1.100564
1000	30.182	0	21.868	2	1909.346	5221.527	0.138108	3312.181	0.365801

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1000	30.182	0	21.868	4	4010.366	9967.54	0.234768	5957.174	0.657917
1000	30.182	0	21.868	6	5335.517	12540.86	0.276791	7205.34	0.795766
1000	30.182	0	21.868	8	6321.634	14281.44	0.30118	7959.807	0.87909
1000	30.182	0	21.868	10	7113.883	15584.84	0.317291	8470.958	0.935542
1000	30.182	0	21.868	12	7779.522	16620.45	0.328751	8840.932	0.976402
1000	30.182	0	21.868	14	8355.492	17475.99	0.337301	9120.502	1.007278
1000	30.182	0	21.868	16	8864.396	18202.55	0.343894	9338.159	1.031317
1000	30.182	0	21.868	18	9321.117	18832.43	0.349099	9511.311	1.05044
1000	30.182	0	21.868	20	9735.988	19387.28	0.353281	9651.291	1.065899
1000	30.182	0	21.868	22	10116.51	19882.31	0.356686	9765.8	1.078546
1000	30.182	0	21.868	24	10468.27	20328.6	0.359485	9860.322	1.088985
1000	31.182	0	22.868	2	1906.399	5229.404	0.134398	3323.005	0.355227
1000	31.182	0	22.868	4	3997.723	9997.151	0.229566	5999.428	0.641335
1000	31.182	0	22.868	6	5313.599	12588.57	0.271402	7274.969	0.777689
1000	31.182	0	22.868	8	6291.311	14344.09	0.2959	8052.777	0.860836
1000	31.182	0	22.868	10	7075.932	15660.16	0.312219	8584.231	0.917648
1000	31.182	0	22.868	12	7734.567	16706.78	0.323925	8972.212	0.959123
1000	31.182	0	22.868	14	8304.058	17572.05	0.332734	9267.997	0.990742
1000	31.182	0	22.868	16	8806.925	18307.35	0.339587	9500.426	1.015589
1000	31.182	0	22.868	18	9257.968	18945.15	0.34505	9687.185	1.035553
1000	31.182	0	22.868	20	9667.486	19507.26	0.349485	9839.775	1.051865
1000	31.182	0	22.868	22	10042.92	20008.99	0.353137	9966.065	1.065365
1000	31.182	0	22.868	24	10389.86	20461.5	0.356177	10071.64	1.076652
1000	32.182	0	23.868	2	1903.642	5236.809	0.13088	3333.167	0.345241
1000	32.182	0	23.868	4	3985.905	10025.02	0.224573	6039.119	0.625517
1000	32.182	0	23.868	6	5293.148	12633.54	0.266184	7340.394	0.7603
1000	32.182	0	23.868	8	6263.05	14403.18	0.290747	8140.133	0.843135
1000	32.182	0	23.868	10	7040.574	15731.25	0.307231	8690.672	0.900159
1000	32.182	0	23.868	12	7692.721	16788.3	0.319141	9095.583	0.942098
1000	32.182	0	23.868	14	8256.202	17662.81	0.328169	9406.605	0.974313
1000	32.182	0	23.868	16	8753.449	18406.39	0.335247	9652.936	0.999828
1000	32.182	0	23.868	18	9199.247	19051.72	0.340933	9852.471	1.020495
1000	32.182	0	23.868	20	9603.793	19620.72	0.345589	10016.93	1.037529
1000	32.182	0	23.868	22	9974.53	20128.82	0.349456	10154.29	1.051756
1000	32.182	0	23.868	24	10316.99	20587.24	0.352706	10270.25	1.063767
1200	28.182	0	19.868	2	1915.892	6245.21	0.149404	4329.318	0.512067
1200	28.182	0	19.868	4	4038.526	11883.02	0.254465	7844.497	0.927838
1200	28.182	0	19.868	6	5384.448	14923.43	0.300732	9538.981	1.128259
1200	28.182	0	19.868	8	6389.404	16972.98	0.327979	10583.58	1.251813
1200	28.182	0	19.868	10	7198.81	18503.92	0.346264	11305.11	1.337155
1200	28.182	0	19.868	12	7880.199	19717.92	0.359491	11837.73	1.400152
1200	28.182	0	19.868	14	8470.777	20719.18	0.369537	12248.4	1.448726

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1200	28.182	0	19.868	16	8993.317	21568.29	0.377433	12574.98	1.487353
1200	28.182	0	19.868	18	9462.846	22303.51	0.383796	12840.66	1.518778
1200	28.182	0	19.868	20	9889.819	22950.45	0.389025	13060.63	1.544795
1200	28.182	0	19.868	22	10281.81	23527.07	0.393385	13245.26	1.566633
1200	28.182	0	19.868	24	10644.52	24046.46	0.397066	13401.94	1.585166
1400	28.182	0	19.868	2	1915.892	7286.855	0.151471	5370.963	0.635271
1400	28.182	0	19.868	4	4038.526	13863.86	0.259909	9825.336	1.162129
1400	28.182	0	19.868	6	5384.448	17410.86	0.308674	12026.42	1.42247
1400	28.182	0	19.868	8	6389.404	19801.95	0.337924	13412.54	1.58642
1400	28.182	0	19.868	10	7198.81	21588	0.357895	14389.19	1.701937
1400	28.182	0	19.868	12	7880.199	23004.32	0.37259	15124.12	1.788863
1400	28.182	0	19.868	14	8470.777	24172.43	0.383943	15701.66	1.857173
1400	28.182	0	19.868	16	8993.317	25163.05	0.393021	16169.74	1.912537
1400	28.182	0	19.868	18	9462.846	26020.8	0.400468	16557.95	1.958455
1400	28.182	0	19.868	20	9889.819	26775.55	0.406699	16885.73	1.997225
1400	28.182	0	19.868	22	10281.81	27448.28	0.411994	17166.47	2.030429
1400	28.182	0	19.868	24	10644.52	28054.23	0.416552	17409.71	2.0592
1600	28.182	0	19.868	2	1915.892	8329.7	0.152926	6413.808	0.758618
1600	28.182	0	19.868	4	4038.526	15845.31	0.263668	11806.78	1.396492
1600	28.182	0	19.868	6	5384.448	19898.7	0.314135	14514.25	1.716728
1600	28.182	0	19.868	8	6389.404	22631.2	0.34474	16241.8	1.92106
1600	28.182	0	19.868	10	7198.81	24672.31	0.36585	17473.5	2.066745
1600	28.182	0	19.868	12	7880.199	26290.89	0.381532	18410.69	2.177595
1600	28.182	0	19.868	14	8470.777	27625.83	0.393761	19155.06	2.265637
1600	28.182	0	19.868	16	8993.317	28757.95	0.403629	19764.63	2.337737
1600	28.182	0	19.868	18	9462.846	29738.2	0.411799	20275.35	2.398145
1600	28.182	0	19.868	20	9889.819	30600.76	0.418696	20710.94	2.449665
1600	28.182	0	19.868	22	10281.81	31369.57	0.424611	21087.76	2.494235
1600	28.182	0	19.868	24	10644.52	32062.07	0.42975	21417.55	2.533242
1800	28.182	0	19.868	2	1915.892	9374.589	0.15403	7458.697	0.882206
1800	28.182	0	19.868	4	4038.526	17827.88	0.266433	13789.35	1.630988
1800	28.182	0	19.868	6	5384.448	22387.3	0.318127	17002.85	2.011077
1800	28.182	0	19.868	8	6389.404	25461.03	0.34971	19071.63	2.25577
1800	28.182	0	19.868	10	7198.81	27757.08	0.371638	20558.27	2.431608
1800	28.182	0	19.868	12	7880.199	29577.84	0.388028	21697.64	2.566371
1800	28.182	0	19.868	14	8470.777	31079.56	0.400884	22608.78	2.67414
1800	28.182	0	19.868	16	8993.317	32353.11	0.411318	23359.79	2.762969
1800	28.182	0	19.868	18	9462.846	33455.84	0.420003	23992.99	2.837863
1800	28.182	0	19.868	20	9889.819	34426.17	0.427375	24536.35	2.902131
1800	28.182	0	19.868	22	10281.81	35291.05	0.433731	25009.24	2.958063

TIT	a	k1	bv	rp	Wc	Wt	eth	Wn	Ws
1800	28.182	0	19.868	24	10644.52	36070.09	0.439282	25425.57	3.007306
2000	28.182	0	19.868	2	1915.892	10408.22	0.154686	8492.326	1.004462
2000	28.182	0	19.868	4	4038.526	19812.21	0.268566	15773.69	1.865693
2000	28.182	0	19.868	6	5384.448	24877.15	0.321183	19492.7	2.305574
2000	28.182	0	19.868	8	6389.404	28291.83	0.353501	21902.43	2.590593
2000	28.182	0	19.868	10	7198.81	30842.64	0.376045	23643.83	2.796564
2000	28.182	0	19.868	12	7880.199	32865.47	0.392967	24985.27	2.955228
2000	28.182	0	19.868	14	8470.777	34533.86	0.406294	26063.09	3.082711
2000	28.182	0	19.868	16	8993.317	35948.78	0.417151	26955.47	3.18826
2000	28.182	0	19.868	18	9462.846	37173.94	0.426221	27711.09	3.277635
2000	28.182	0	19.868	20	9889.819	38252	0.433948	28362.18	3.354644
2000	28.182	0	19.868	22	10281.81	39212.91	0.440634	28931.09	3.421935
2000	28.182	0	19.868	24	10644.52	40078.44	0.446493	29433.92	3.481409

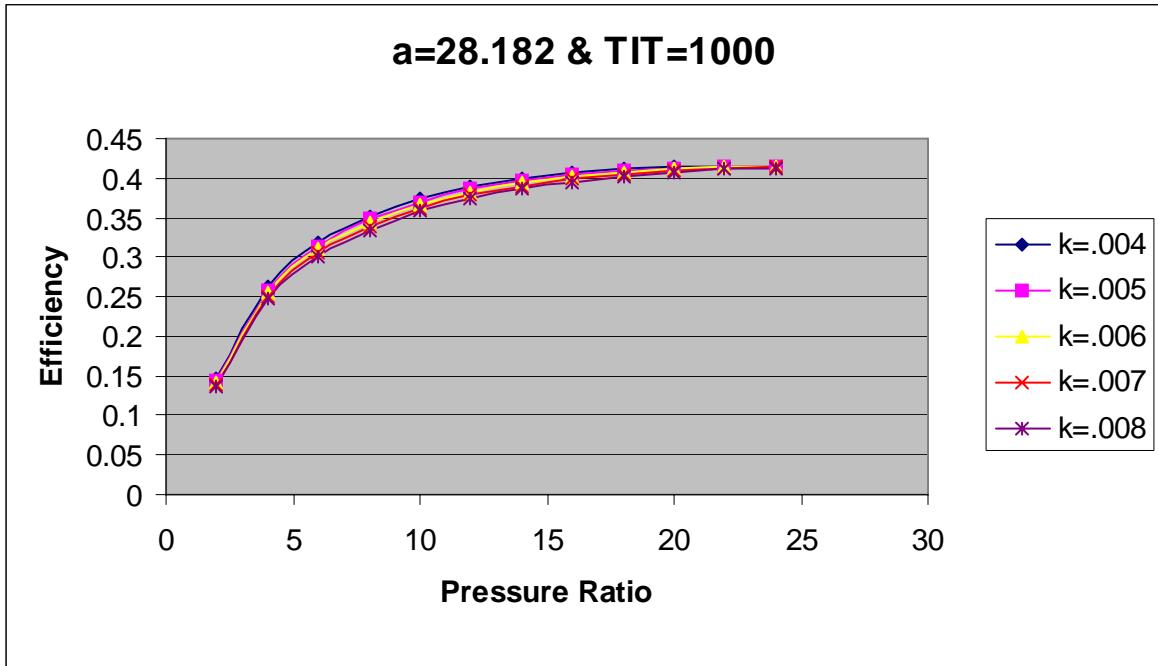


Fig 3.1.1 Variation of Efficiency of gas turbine Vs Pressure ratio

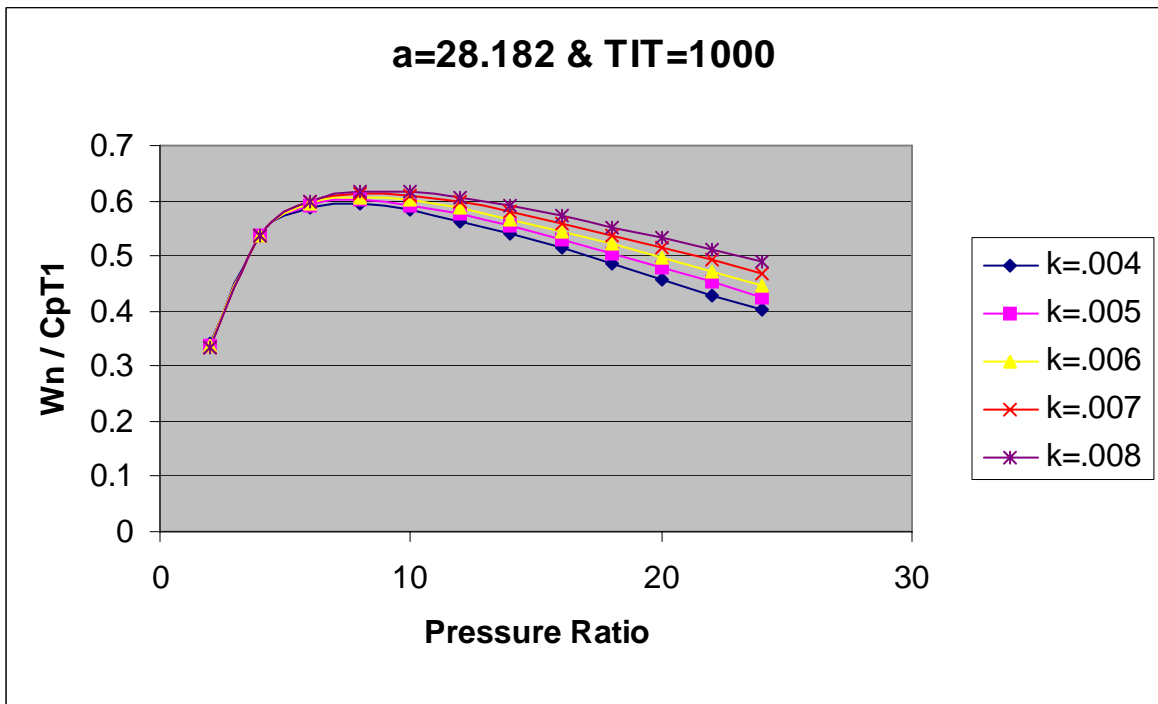


Fig 3.1.2 Variation of $W_n / C_p T_1$ Vs Pressure ratio

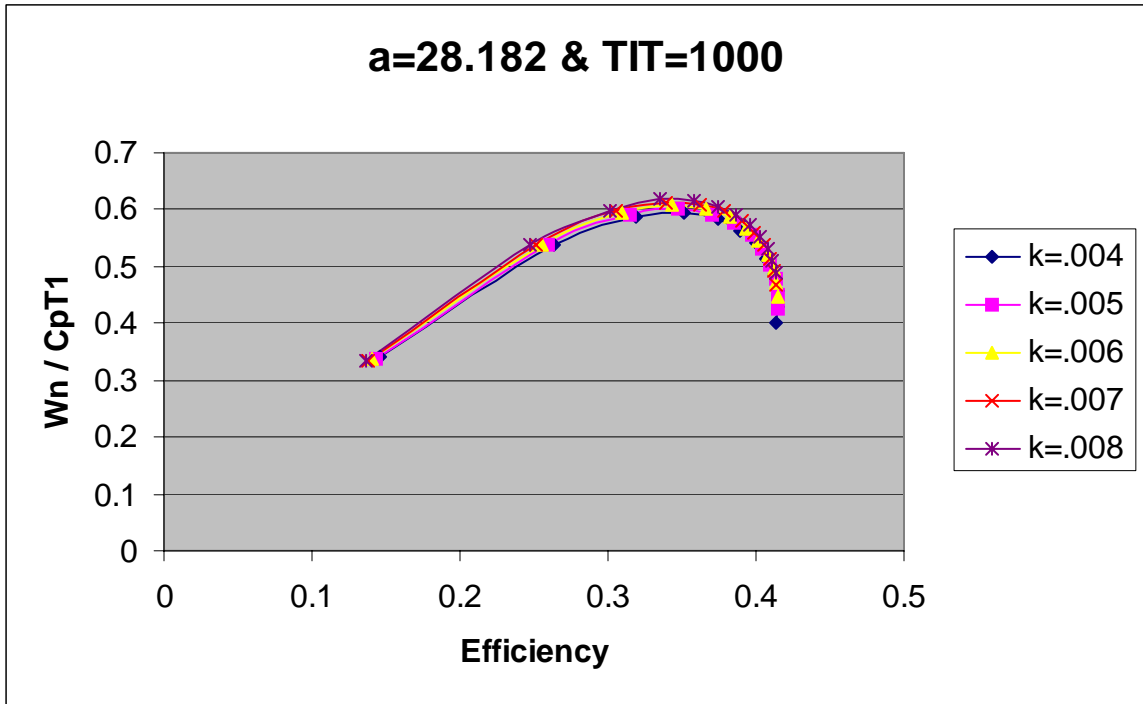


Fig 3.1.3 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine

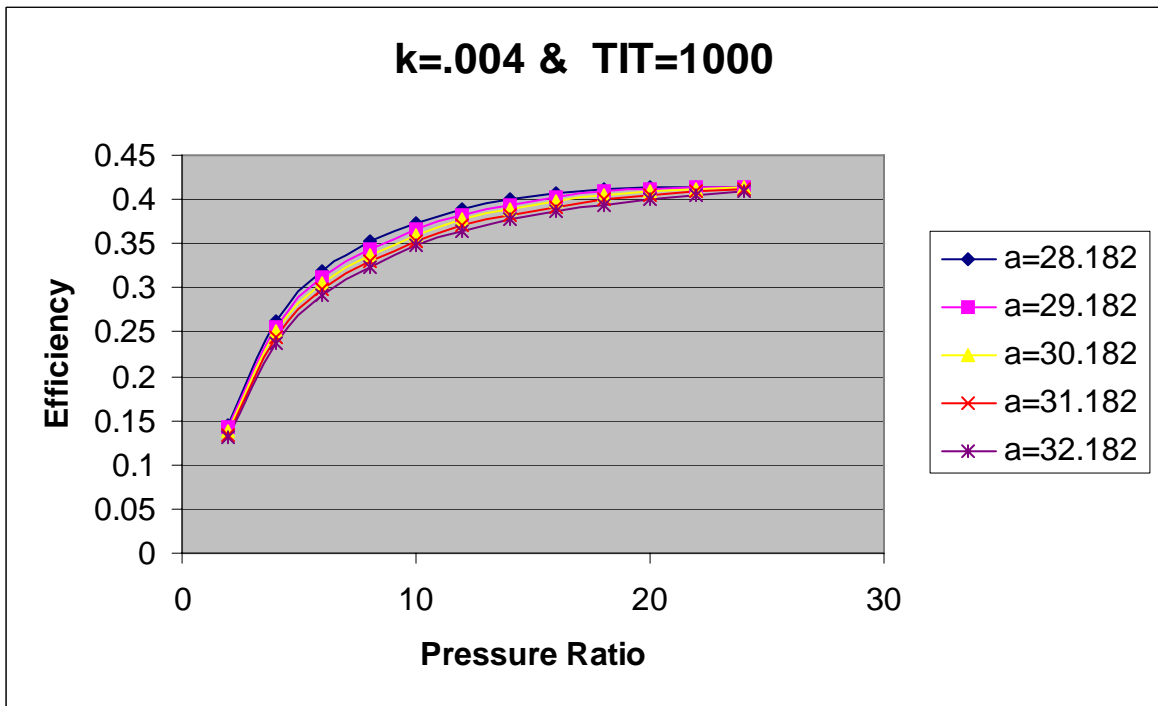


Fig 3.1.4 Variation of Efficiency of gas turbine Vs Pressure ratio

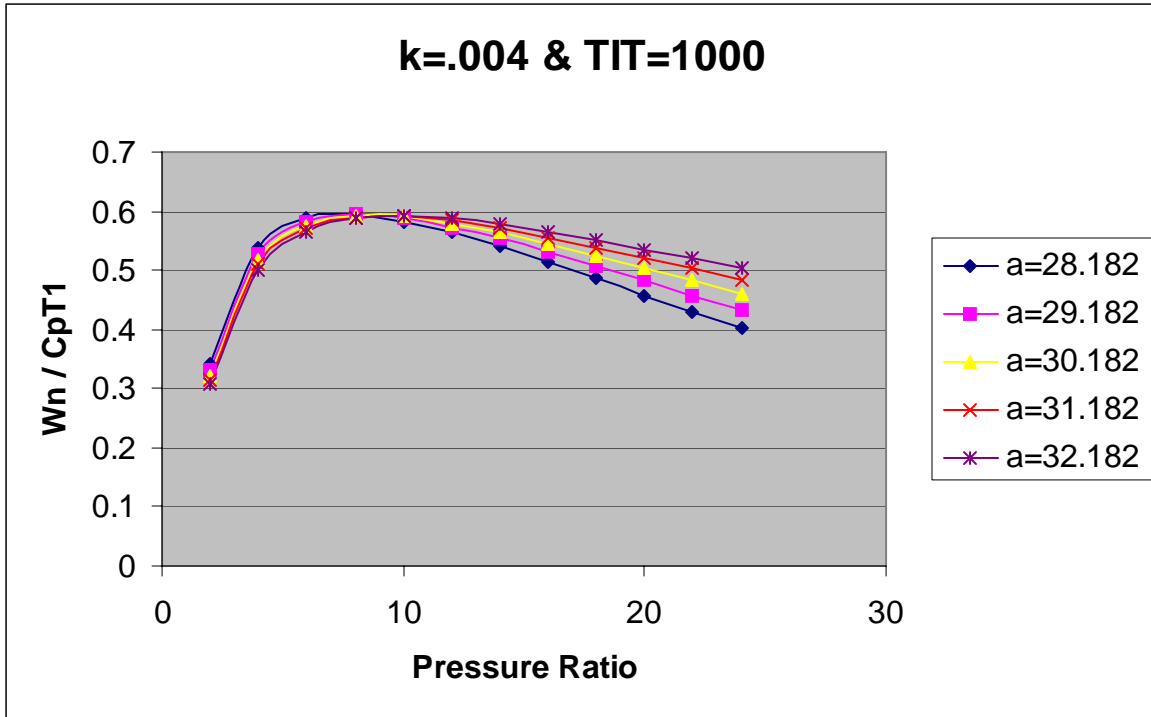


Fig 3.1.5 Variation of W_n/C_pT_1 Vs Pressure ratio

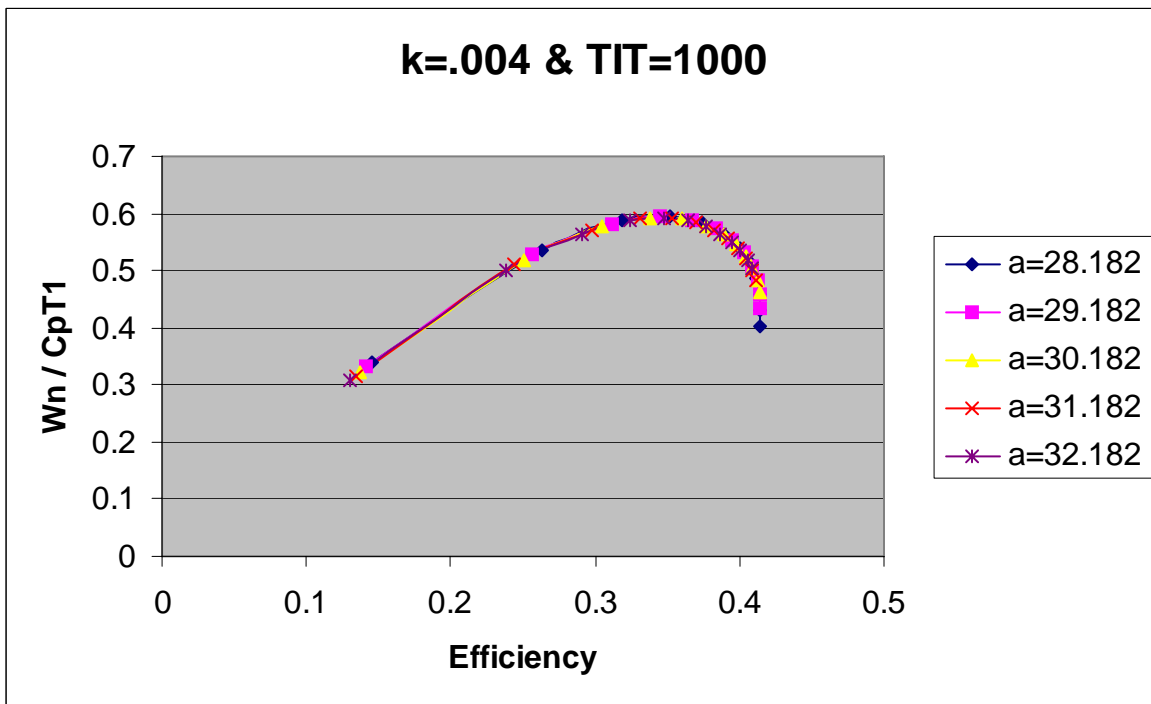


Fig 3.1.6 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine

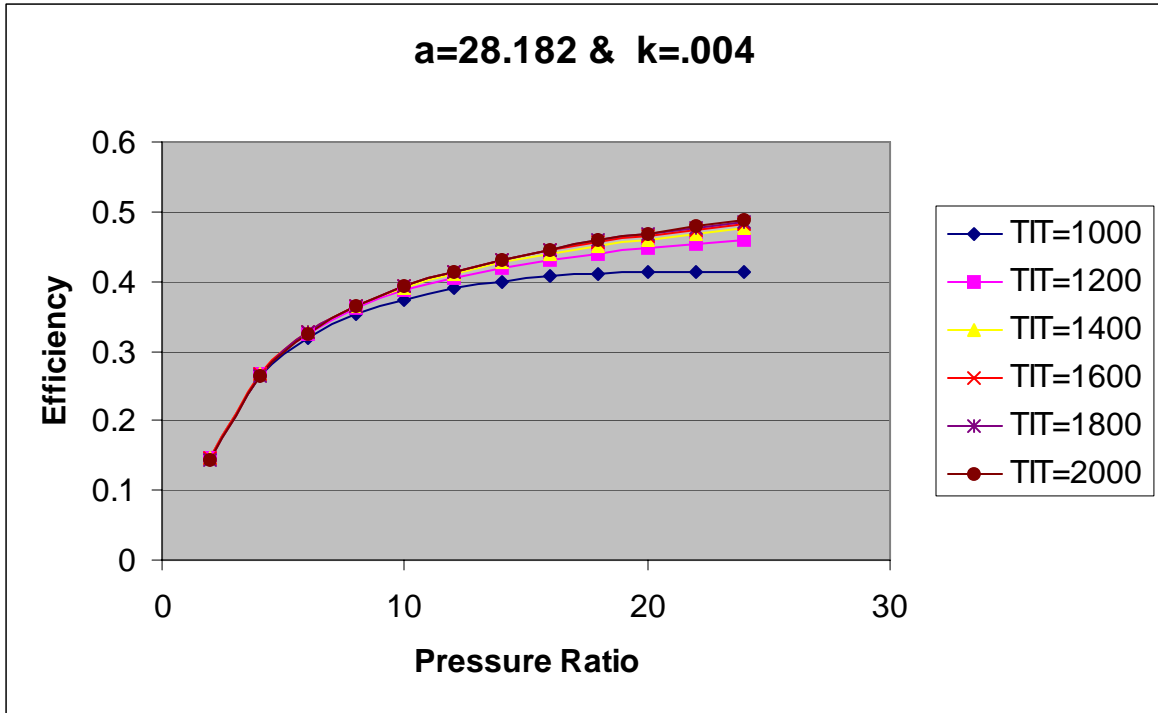


Fig 3.1.7 Variation of Efficiency of gas turbine Vs Pressure ratio

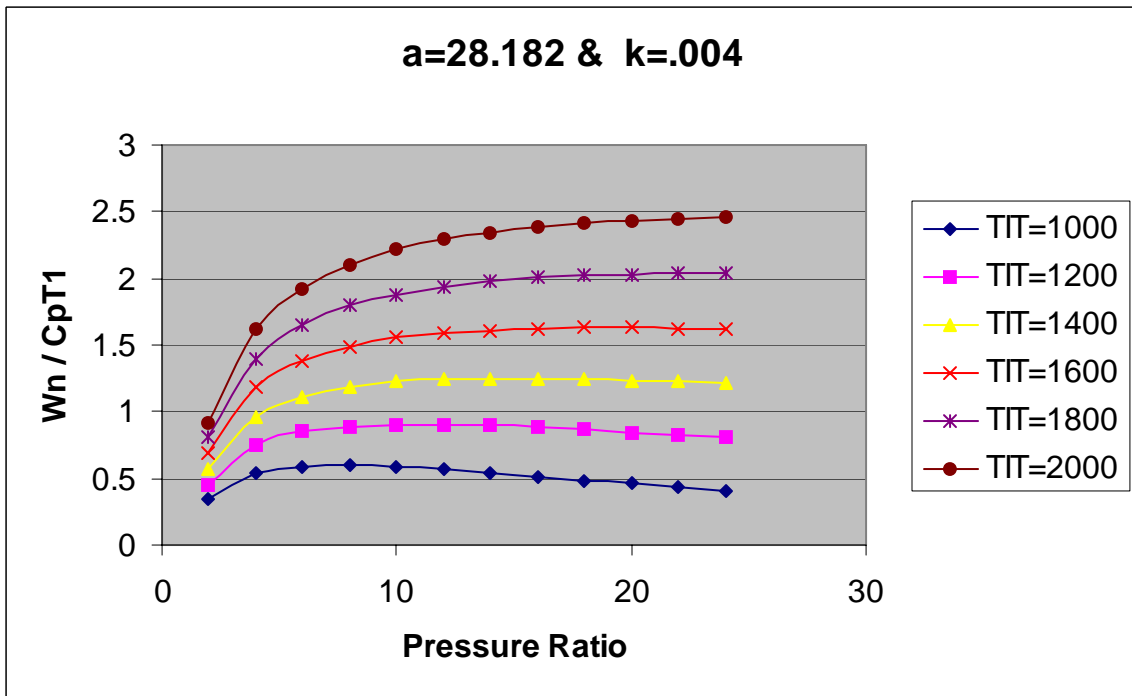


Fig 3.1.8 Variation of W_n/C_pT_1 Vs Pressure ratio

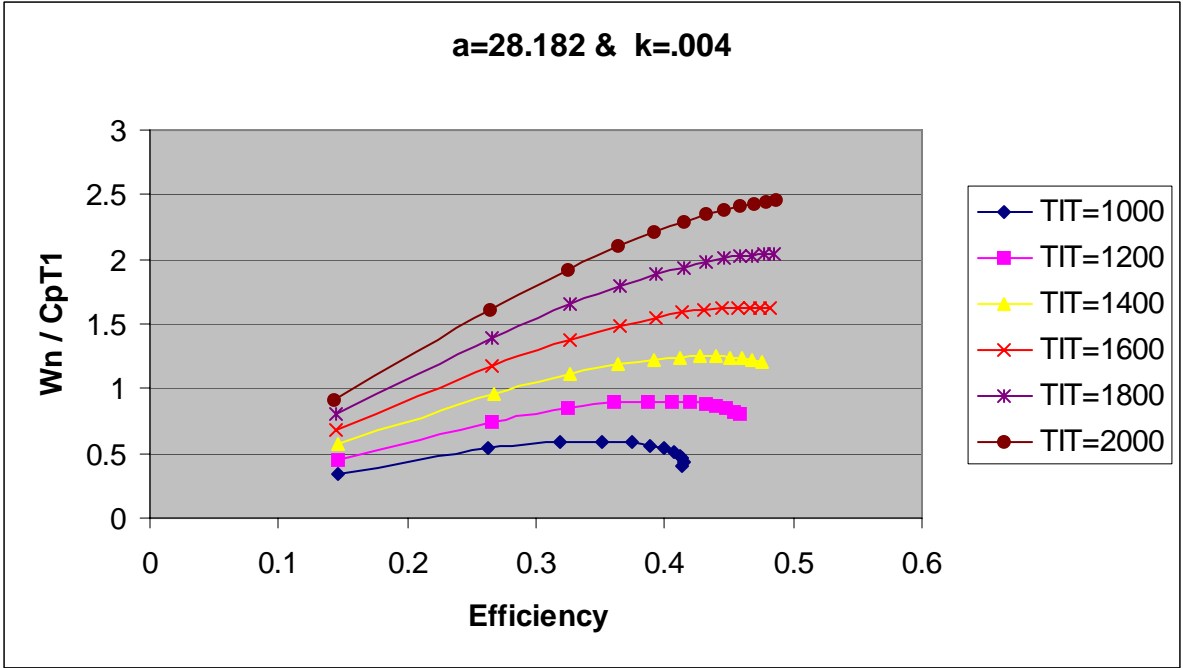


Fig 3.1.9 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine

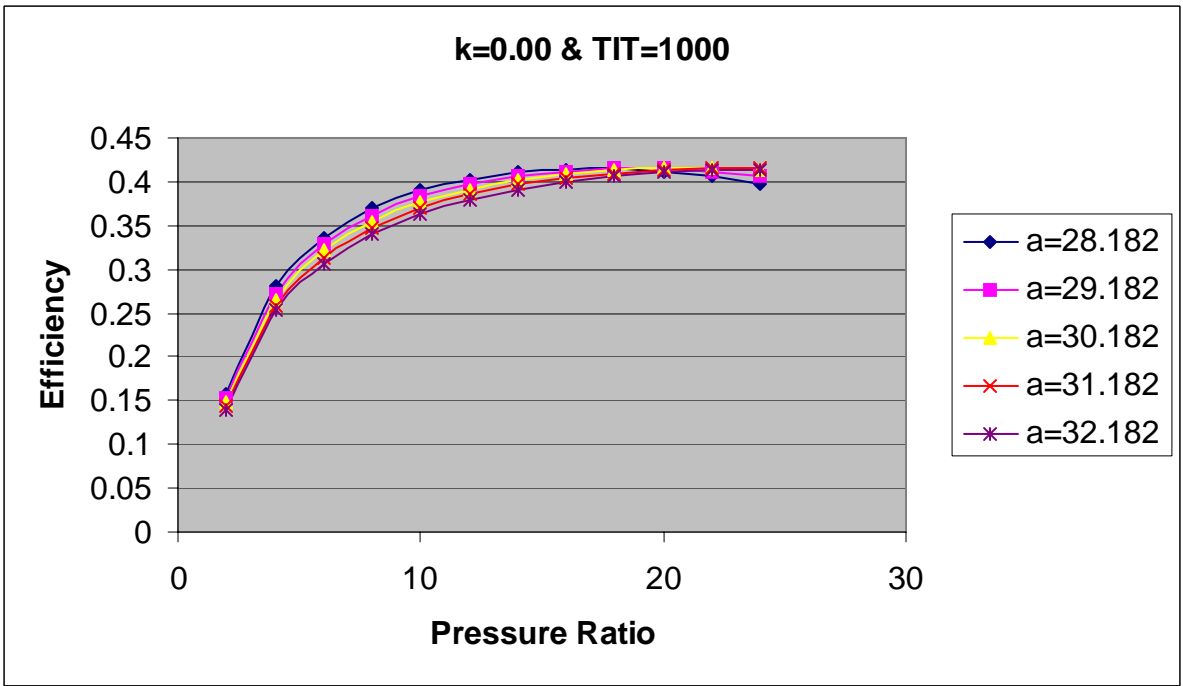


Fig 3.1.10 Variation of Efficiency of gas turbine Vs Pressure ratio

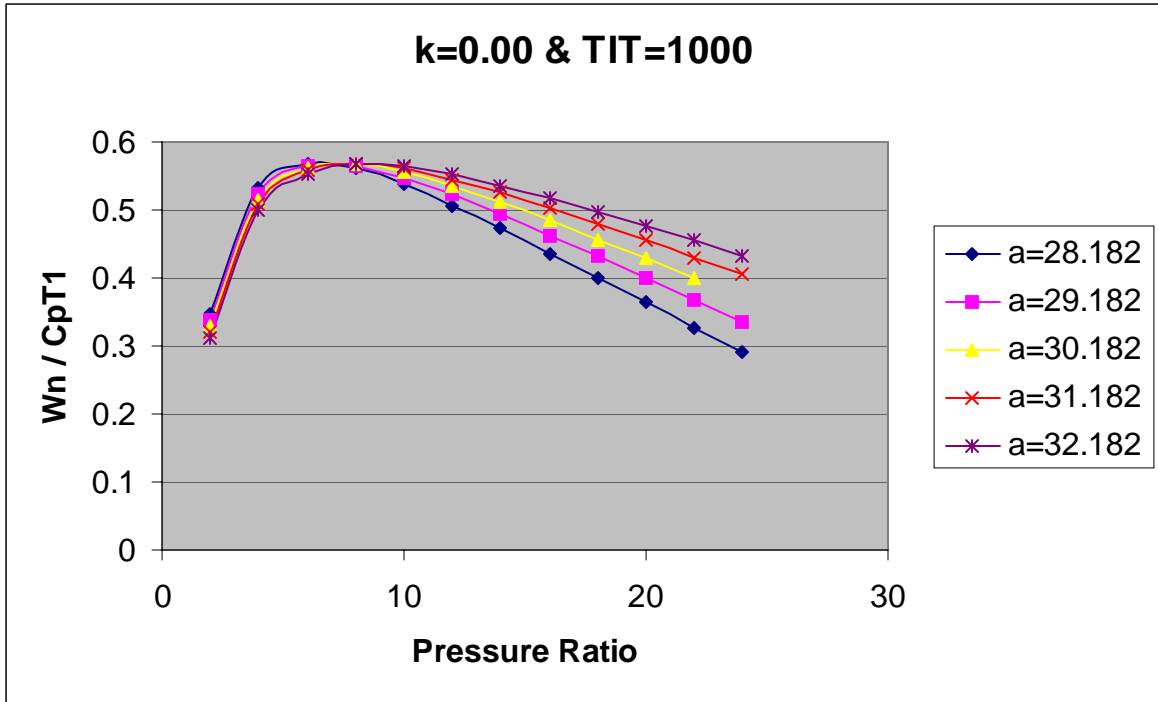


Fig 3.1.11 Variation of W_n/C_pT_1 Vs Pressure ratio

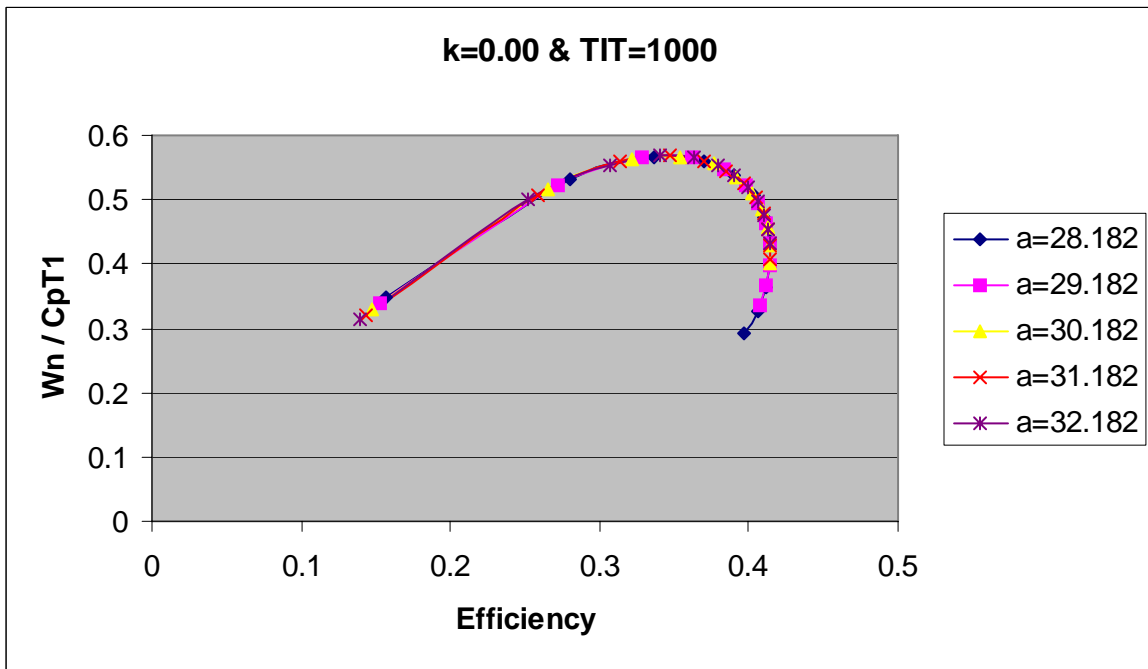


Fig 3.1.12 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine

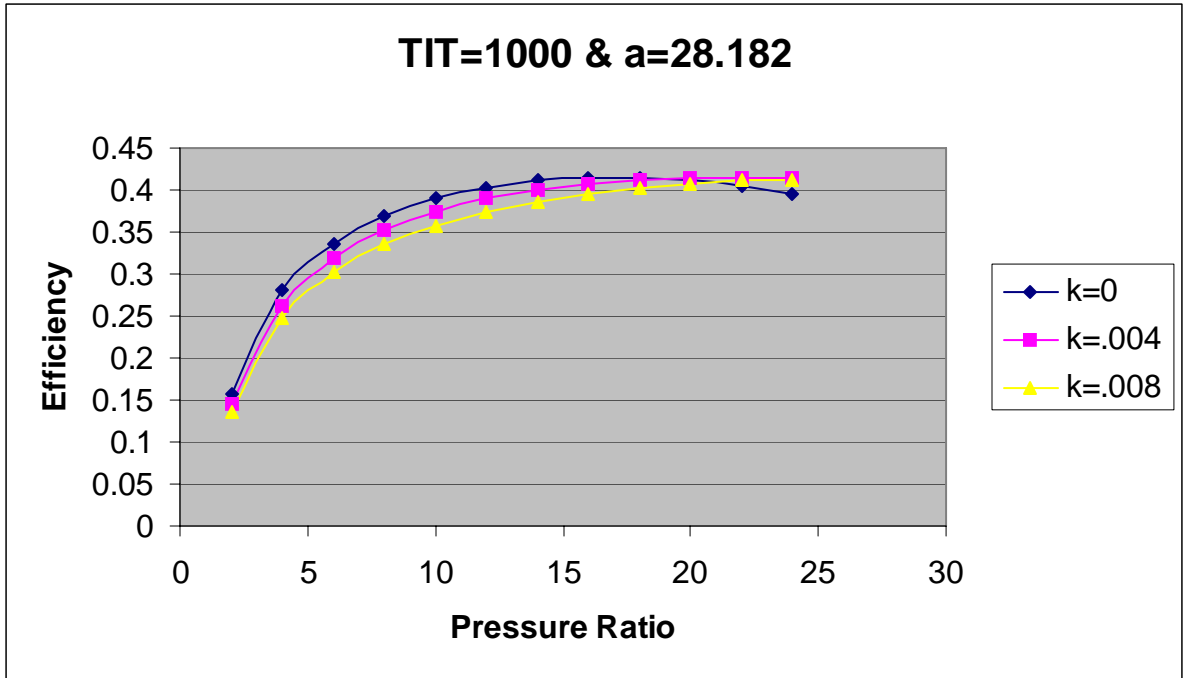


Fig 3.1.13 Variation of Efficiency of gas turbine Vs Pressure ratio

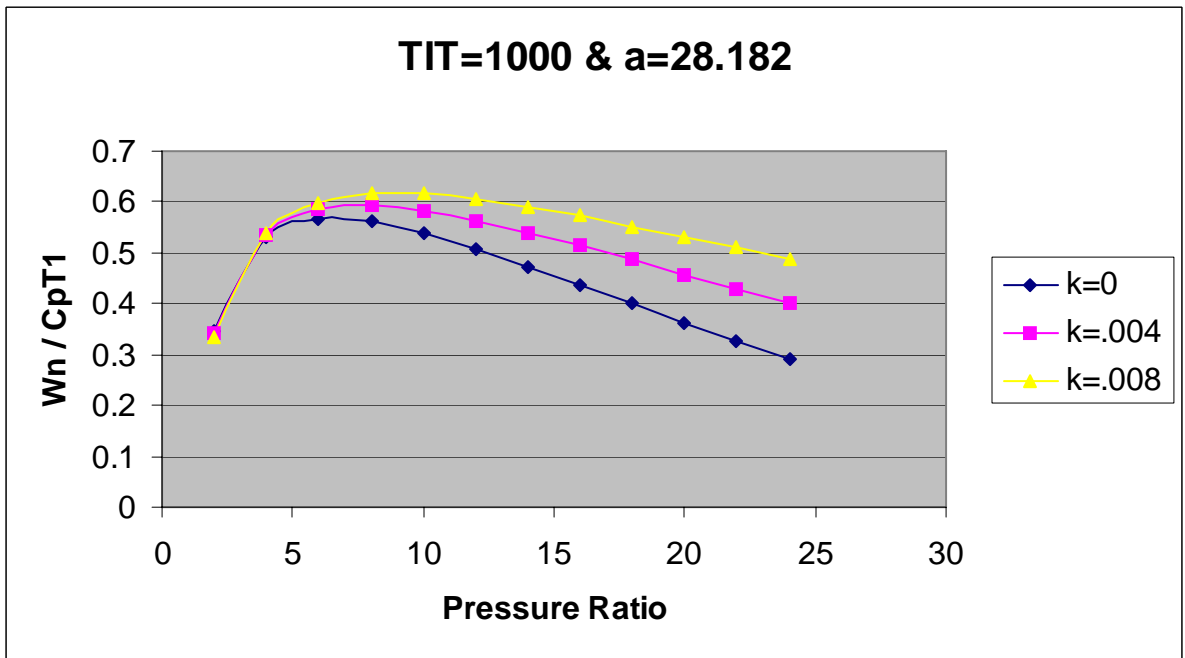


Fig 3.1.14 Variation of W_n/C_pT_1 Vs Pressure ratio

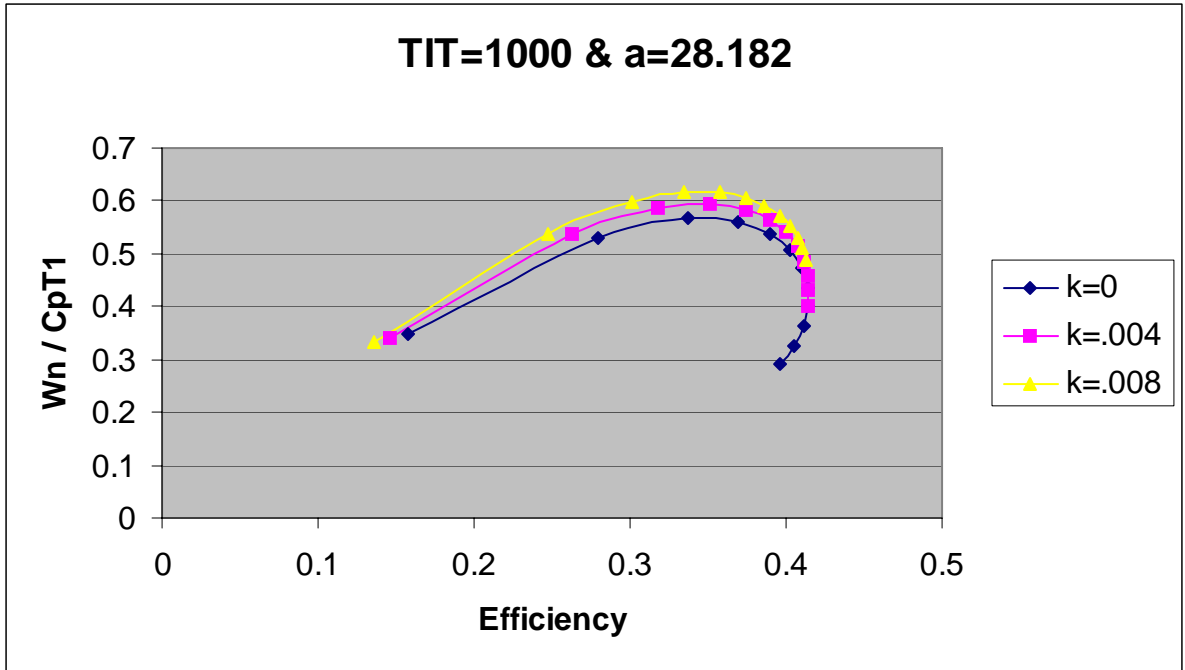


Fig 3.1.15 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine

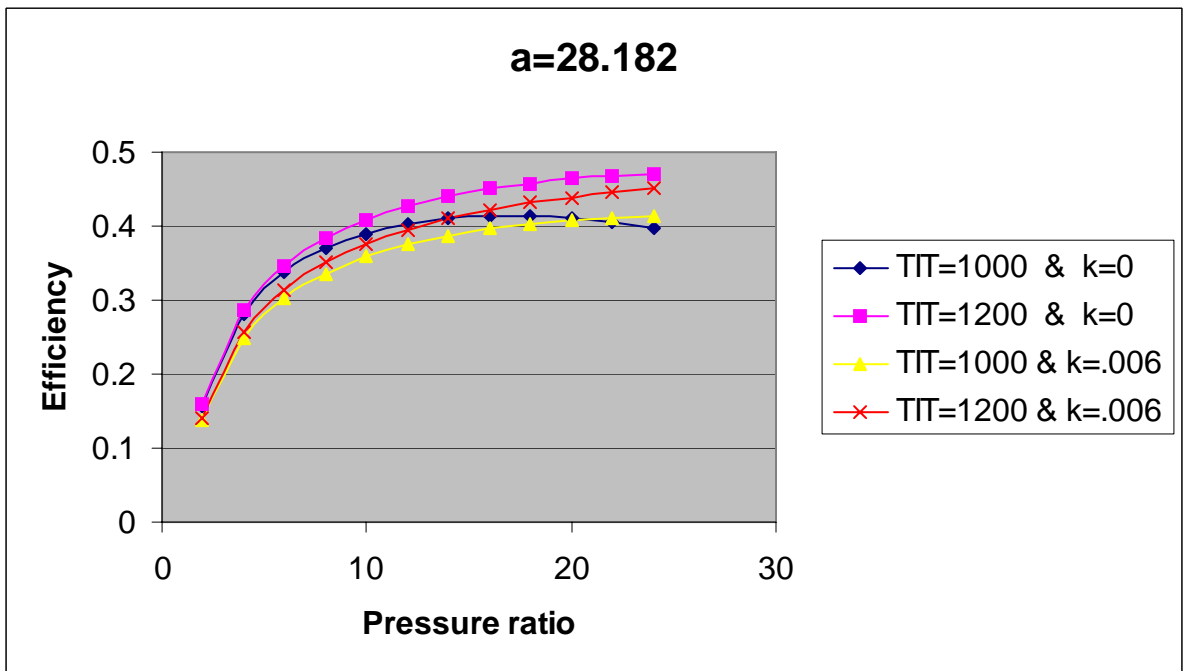


Fig 3.1.16 Variation of Efficiency of gas turbine Vs Pressure ratio

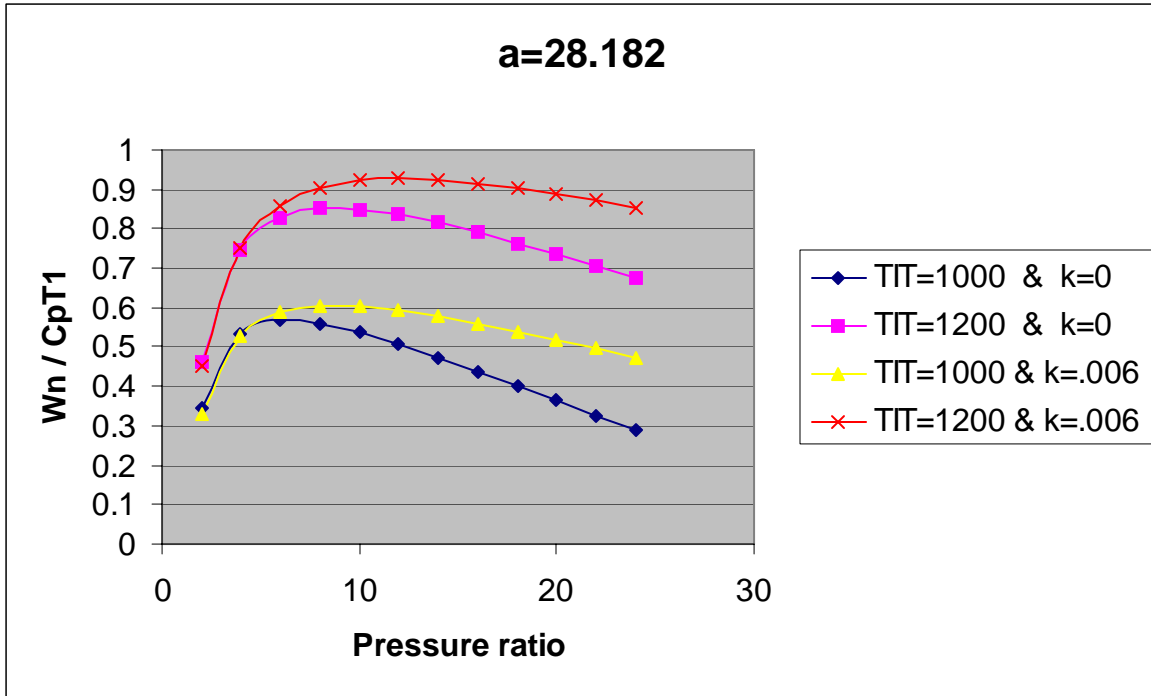


Fig 3.1.17 Variation of W_n/C_pT_1 Vs Pressure ratio

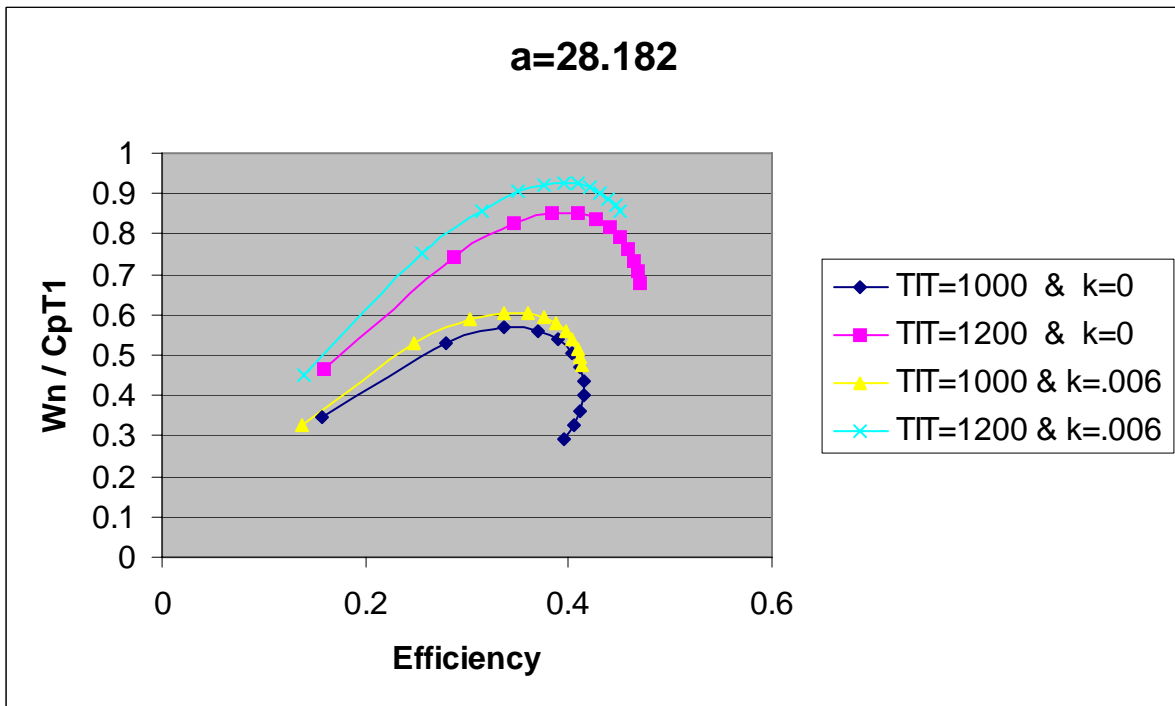


Fig 3.1.18 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine

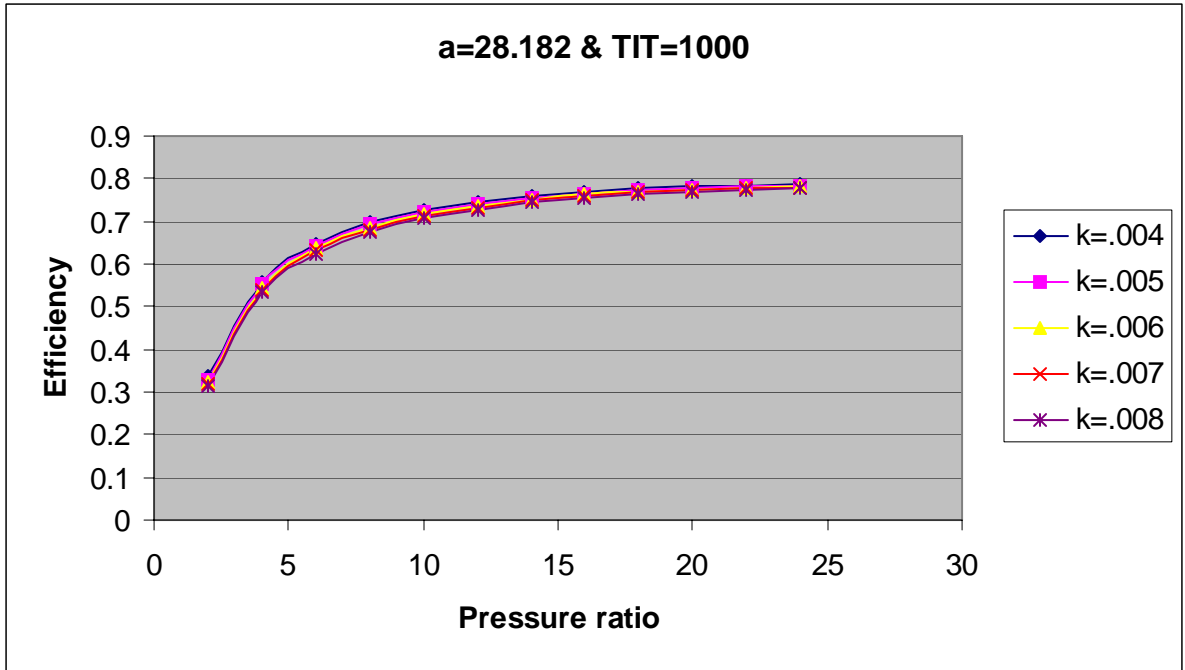


Fig 3.2.1 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler

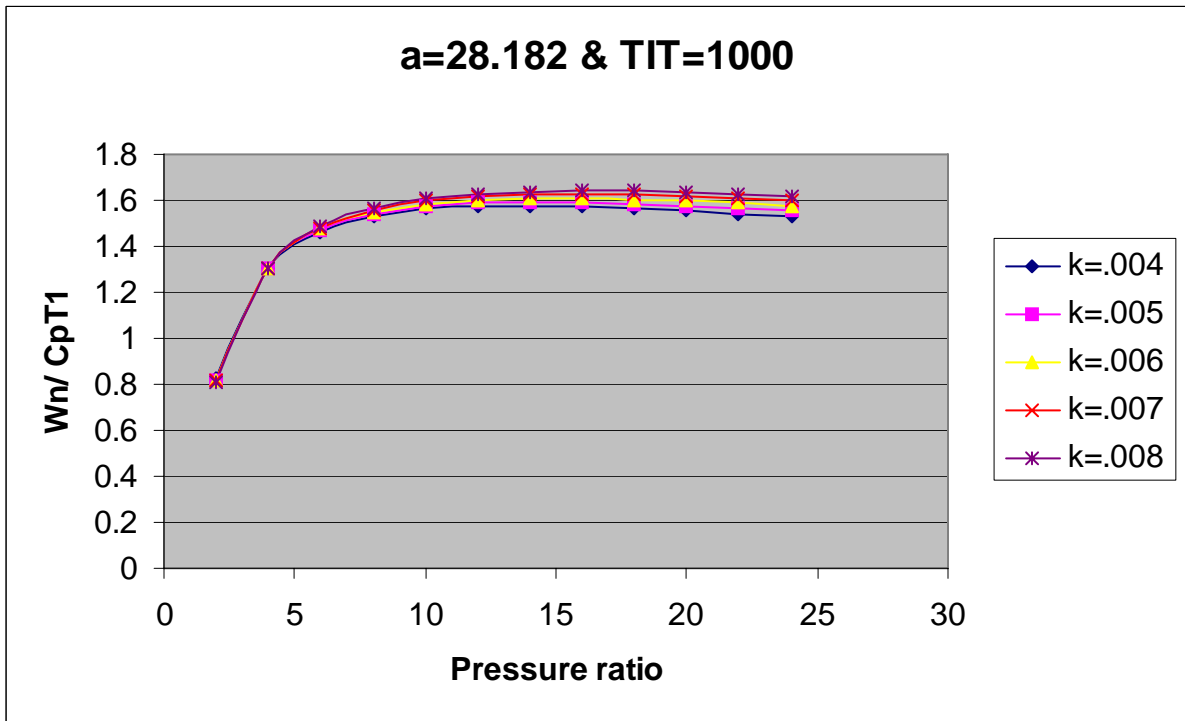


Fig 3.2.2 Variation of $W_n/C_p T_1$ Vs Pressure ratio with one intercooler

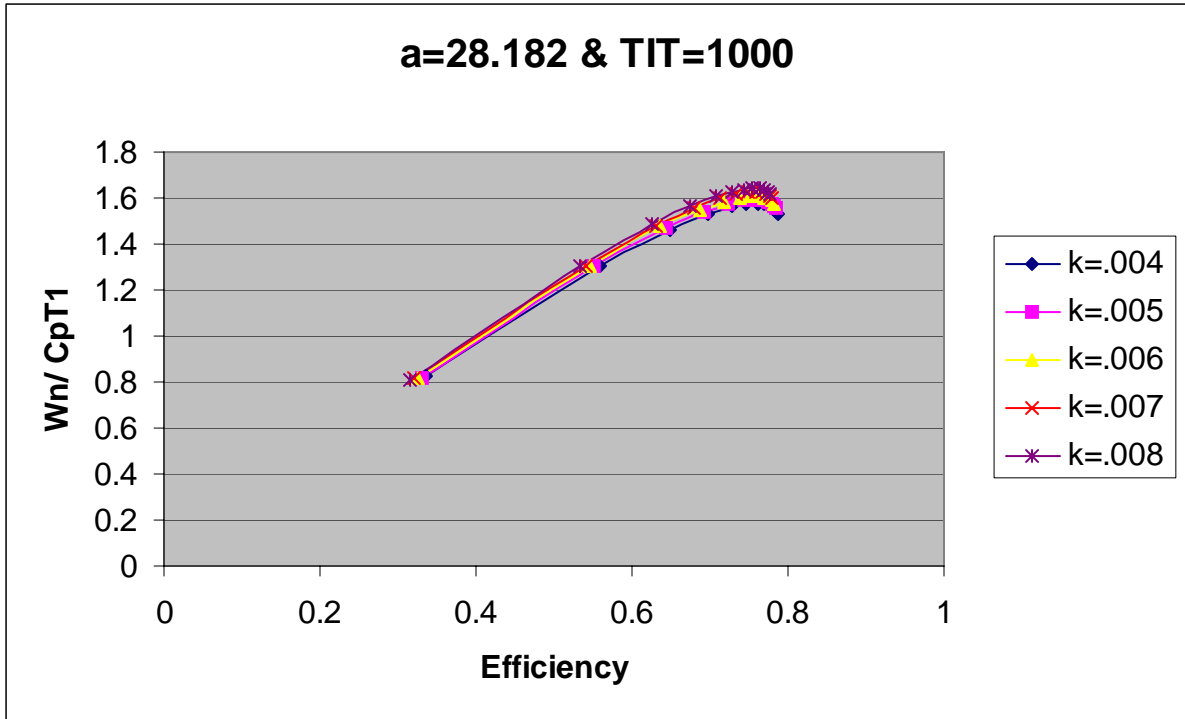


Fig 3.2.3 Variation of $W_n/C_p T_1$ Vs Efficiency of gas turbine with one intercooler

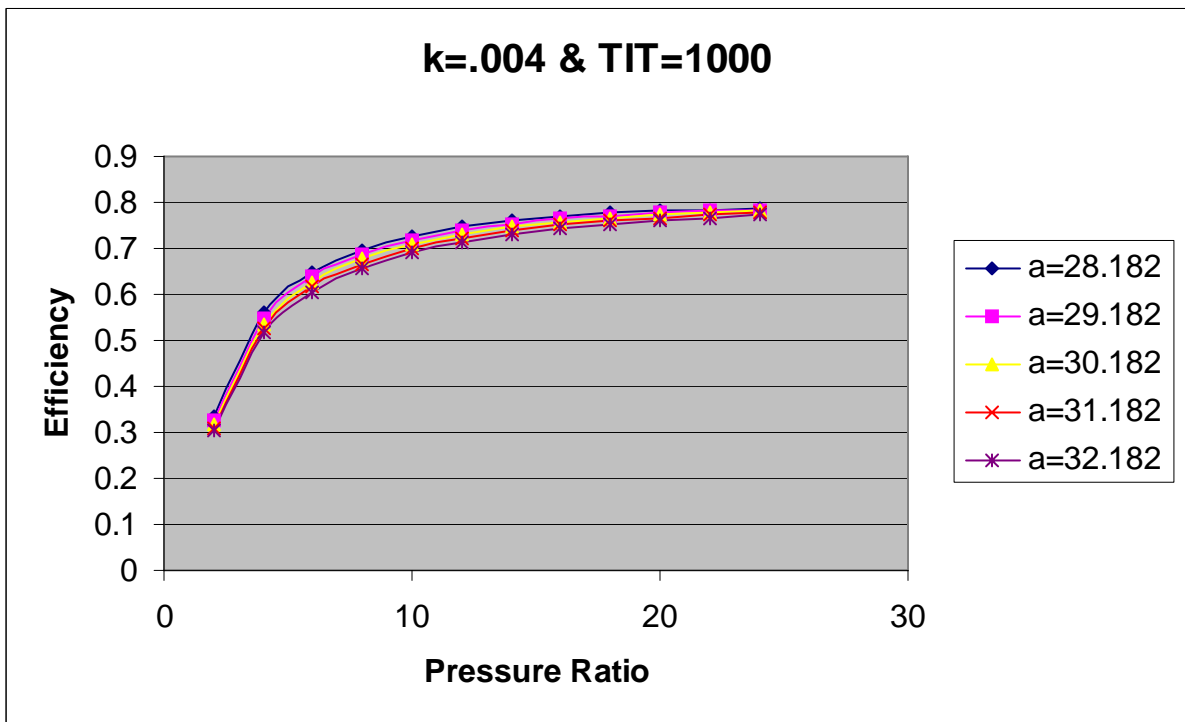


Fig 3.2.4 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler

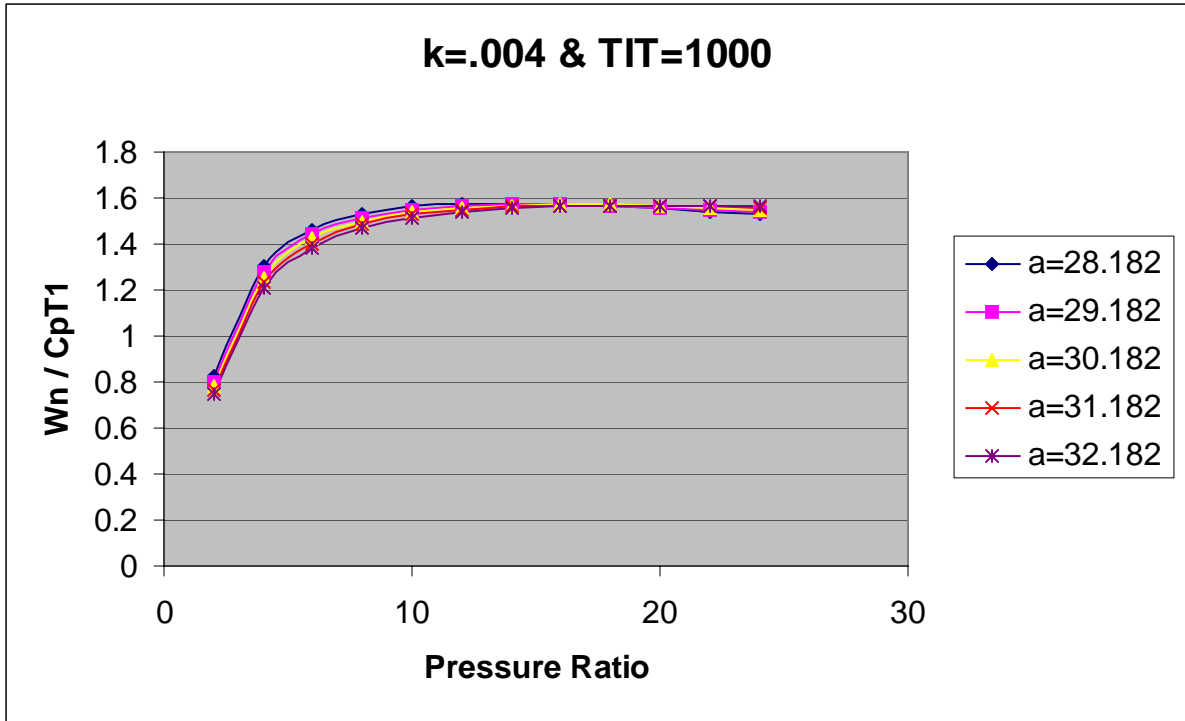


Fig 3.2.5 Variation of W_n/C_pT_1 Vs Pressure ratio with one intercooler

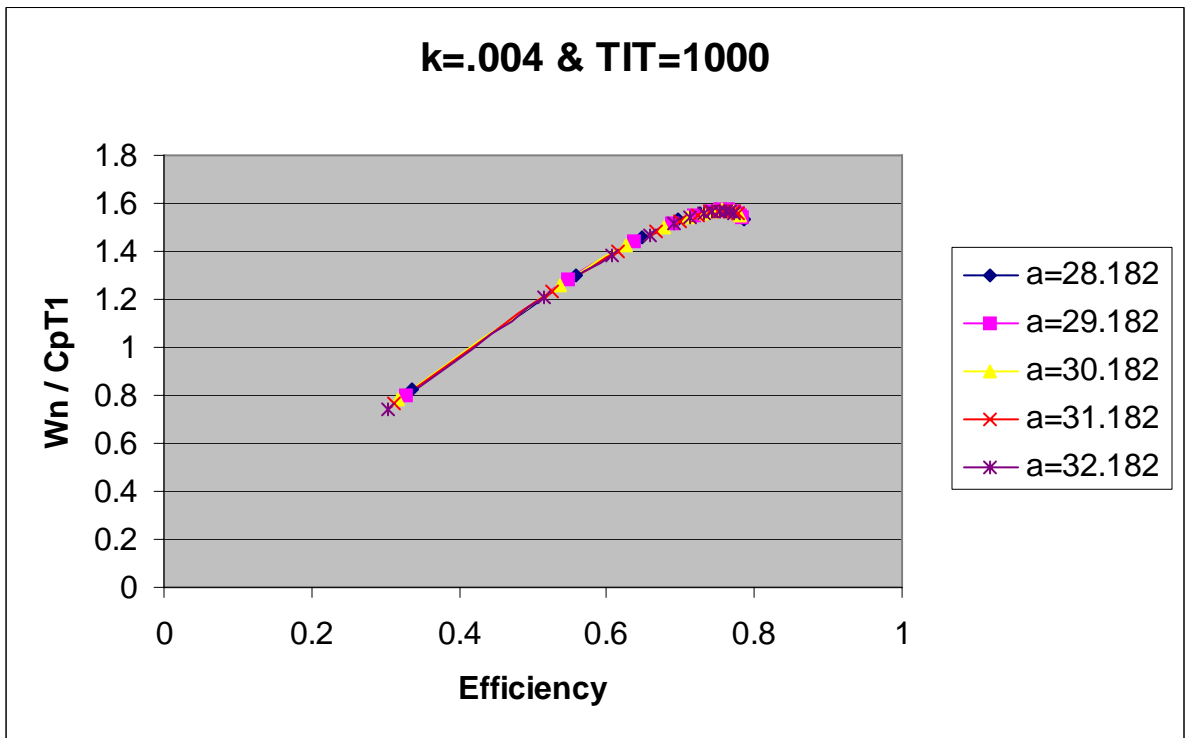


Fig 3.2.6 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one intercooler

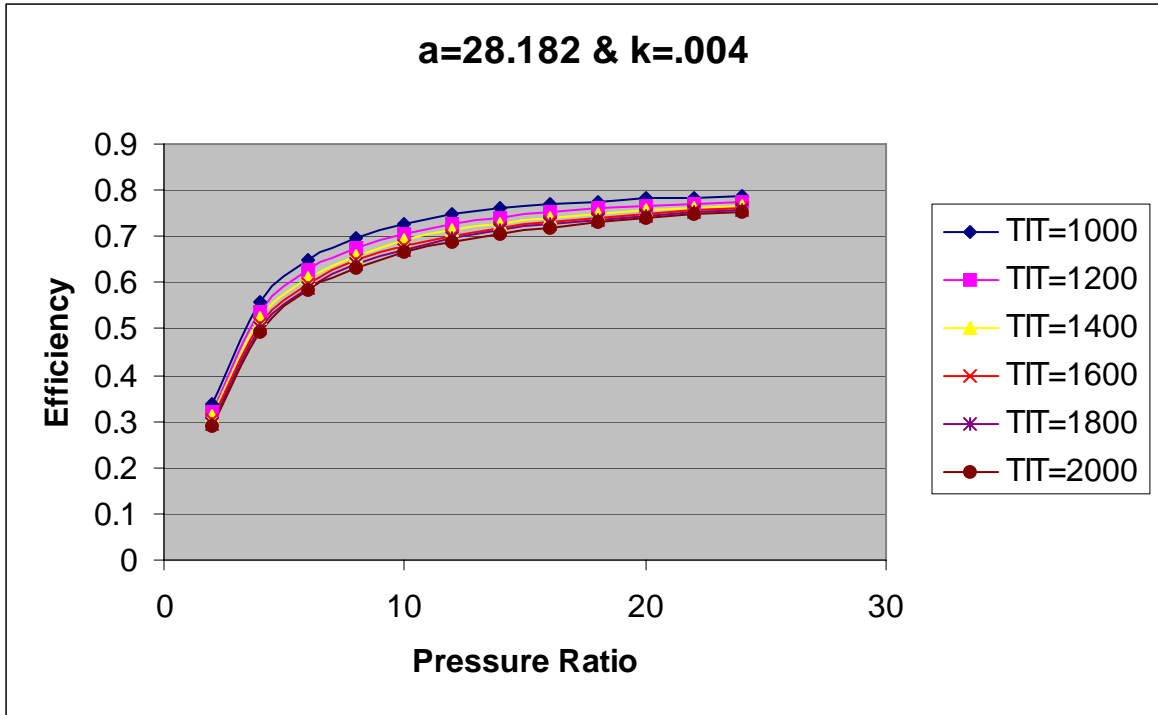


Fig 3.2.7 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler

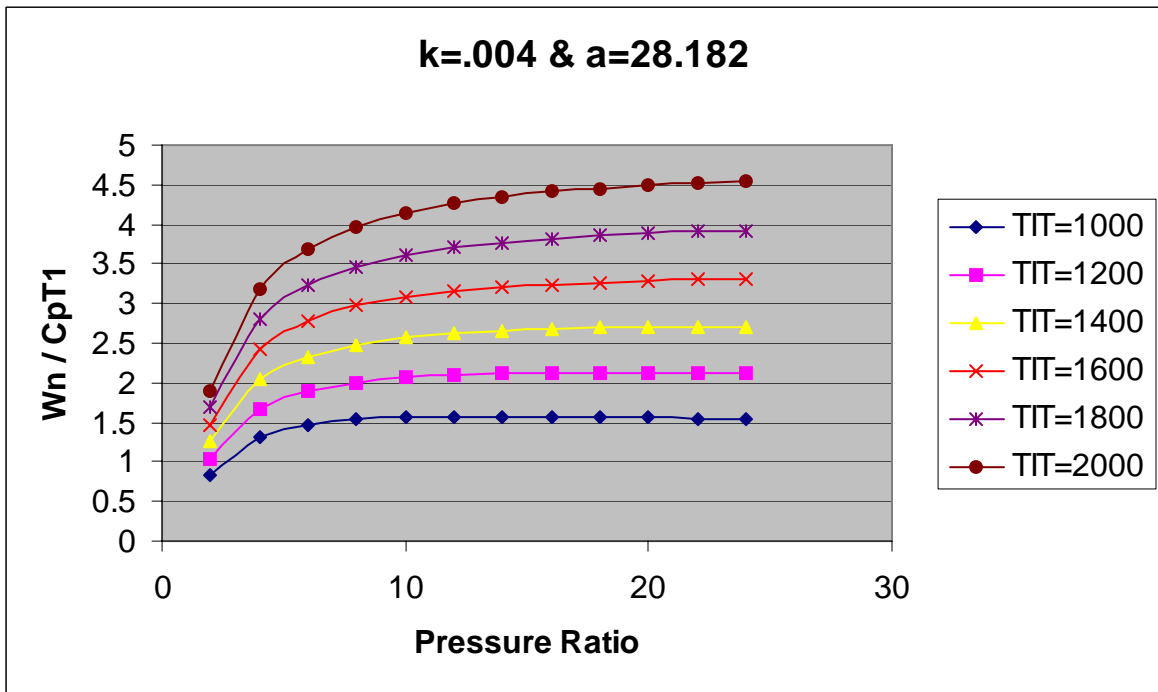


Fig 3.2.8 Variation of $W_n / C_p T_1$ Vs Pressure ratio with one intercooler

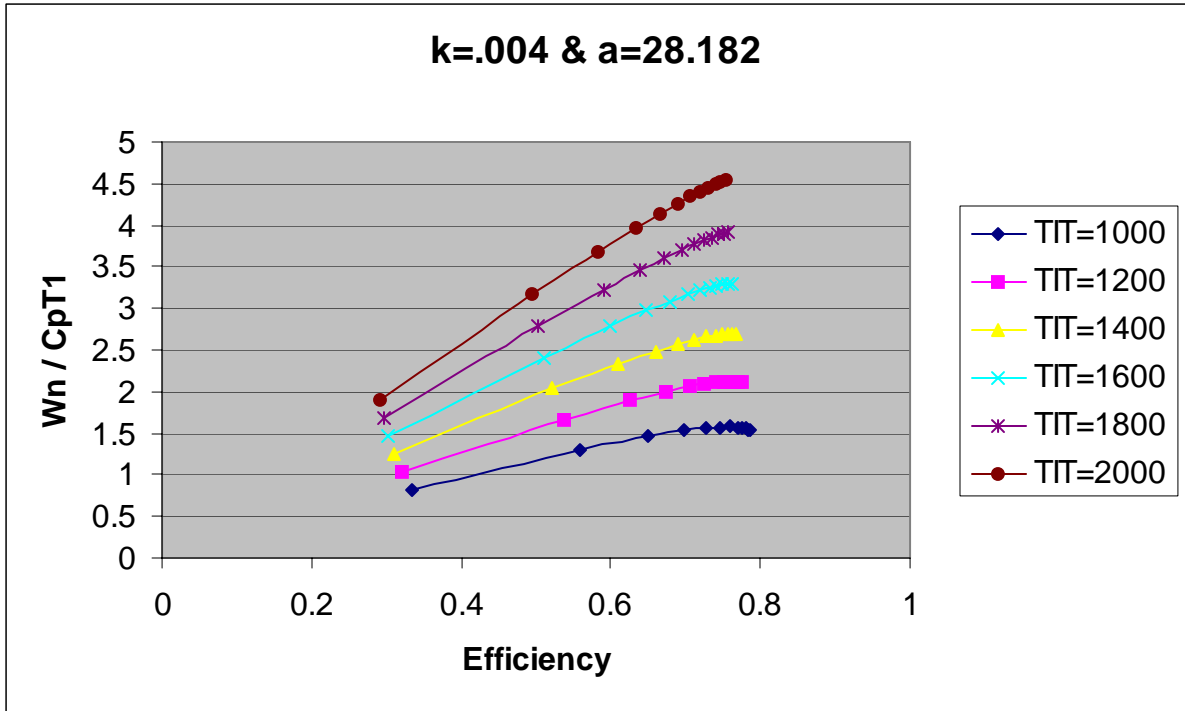


Fig 3.2.9 Variation of $W_n / C_p T_1$ Vs Efficiency of gas turbine with one intercooler

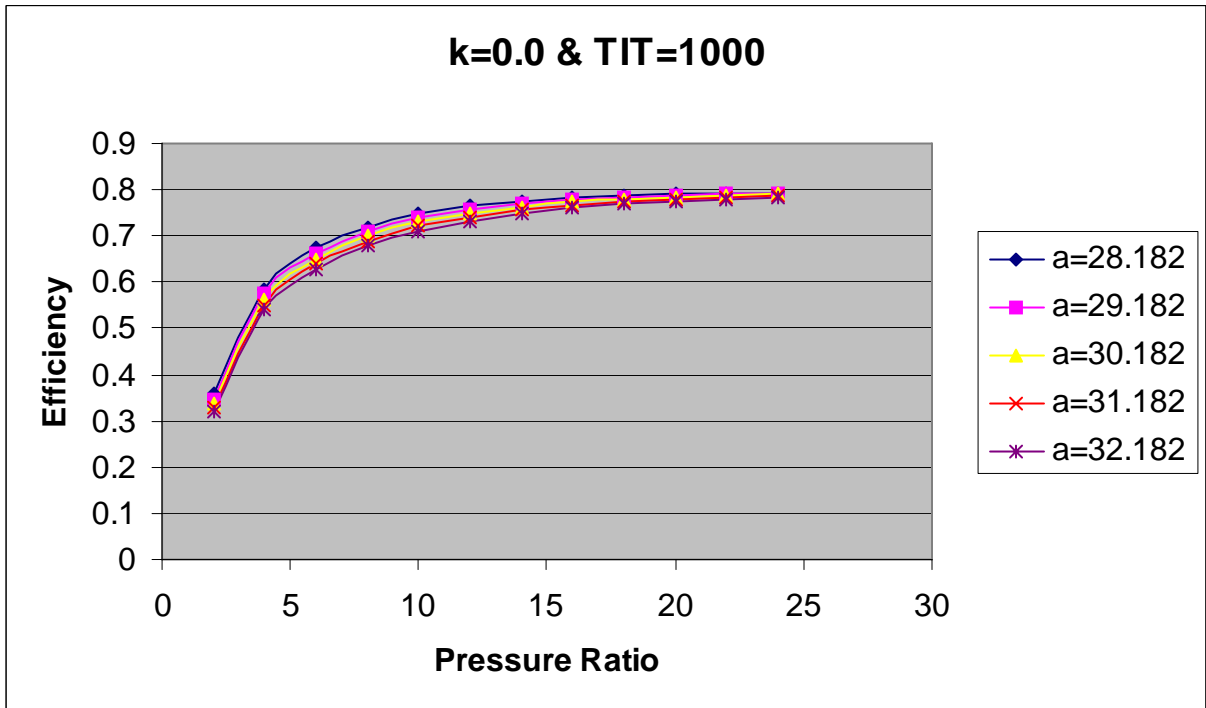


Fig 3.2.10 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler

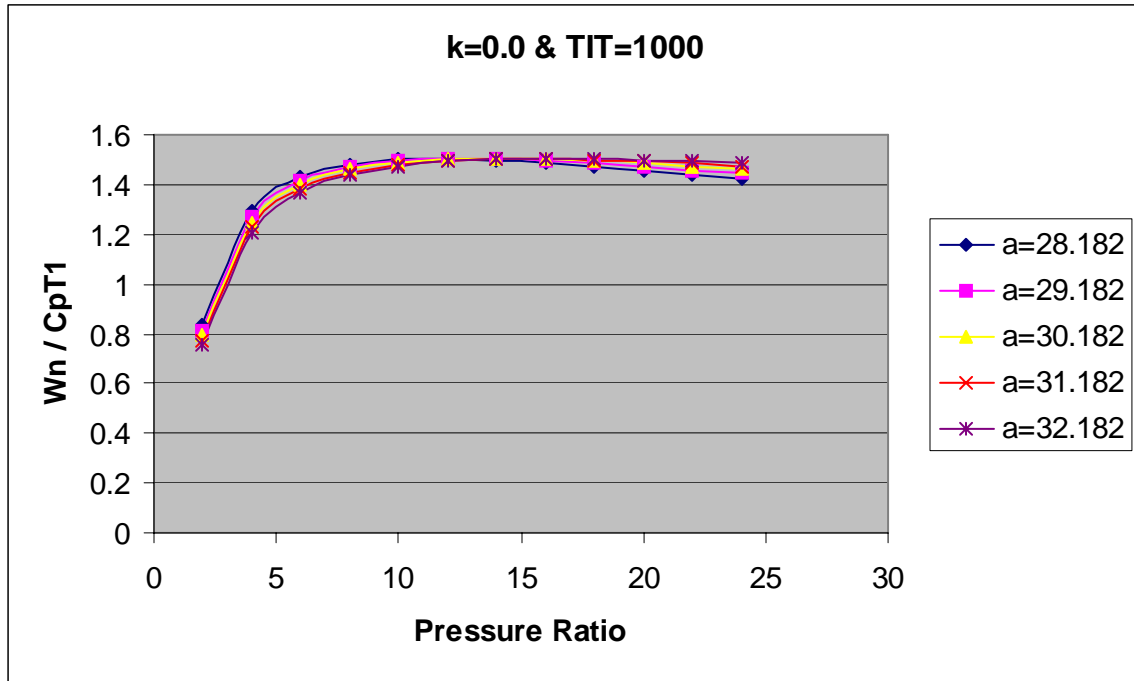


Fig 3.2.11 Variation of $W_n/C_p T_1$ Vs Pressure ratio with one intercooler

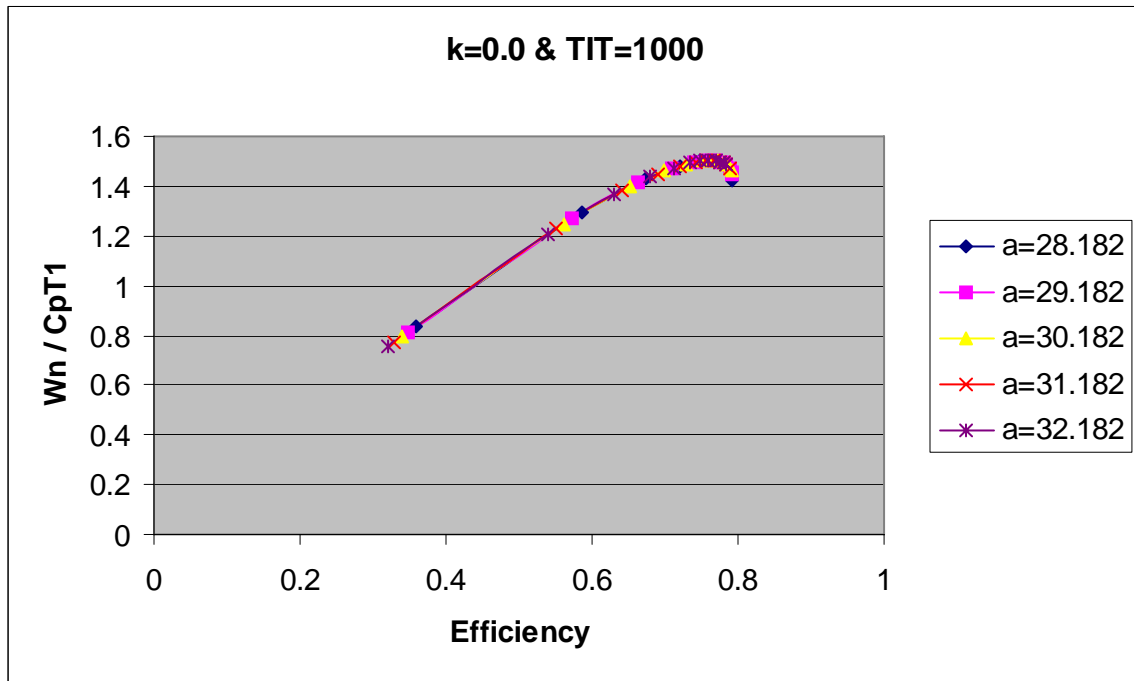


Fig 3.2.12 Variation of $W_n/C_p T_1$ Vs Efficiency of gas turbine with one intercooler

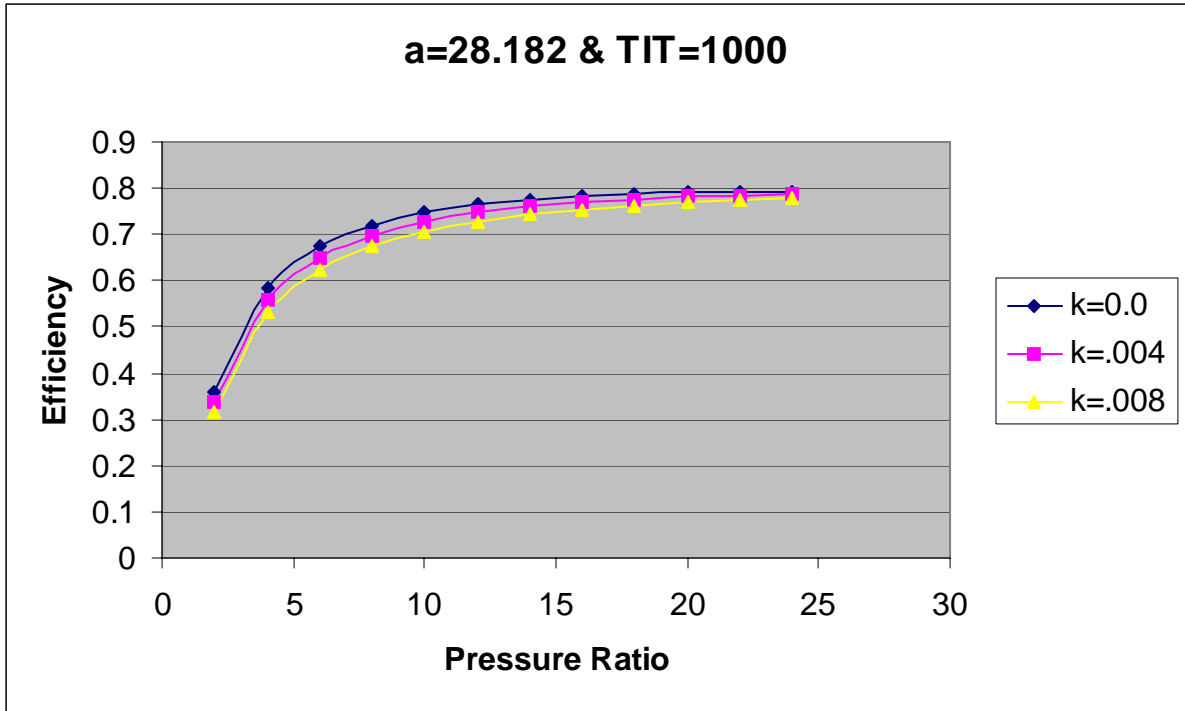


Fig 3.2.13 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler

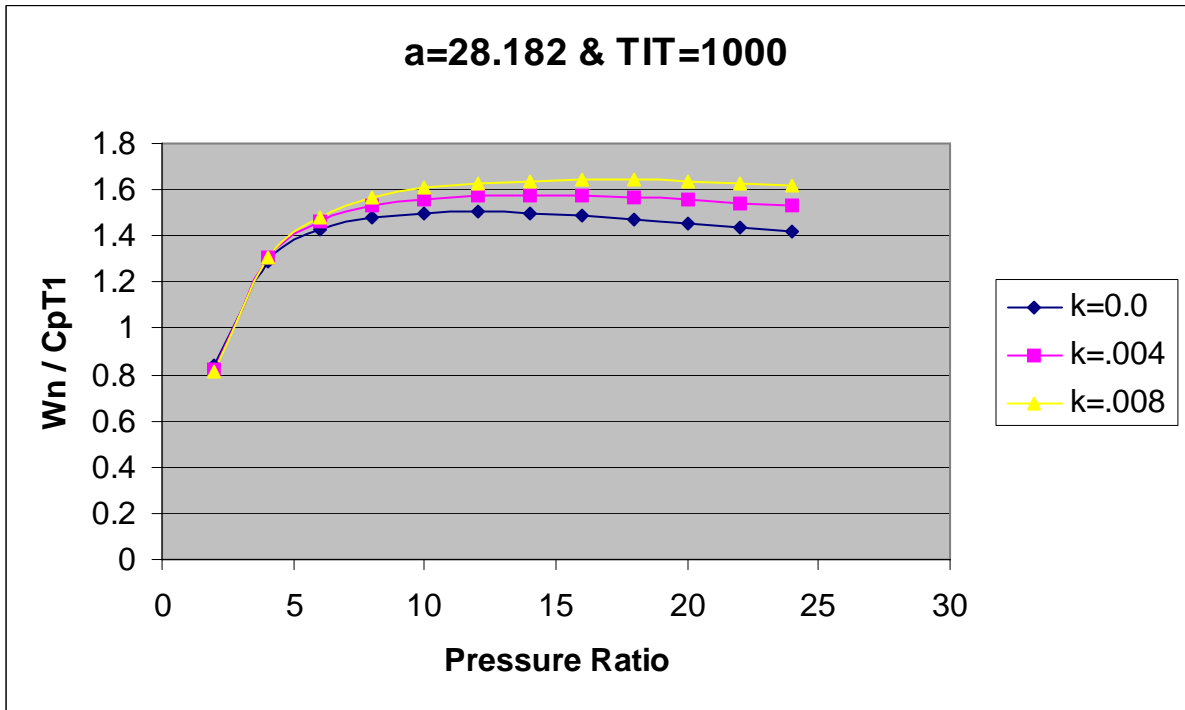


Fig 3.2.14 Variation of W_n/C_pT_1 Vs Pressure ratio with one intercooler



Fig 3.2.15 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one intercooler

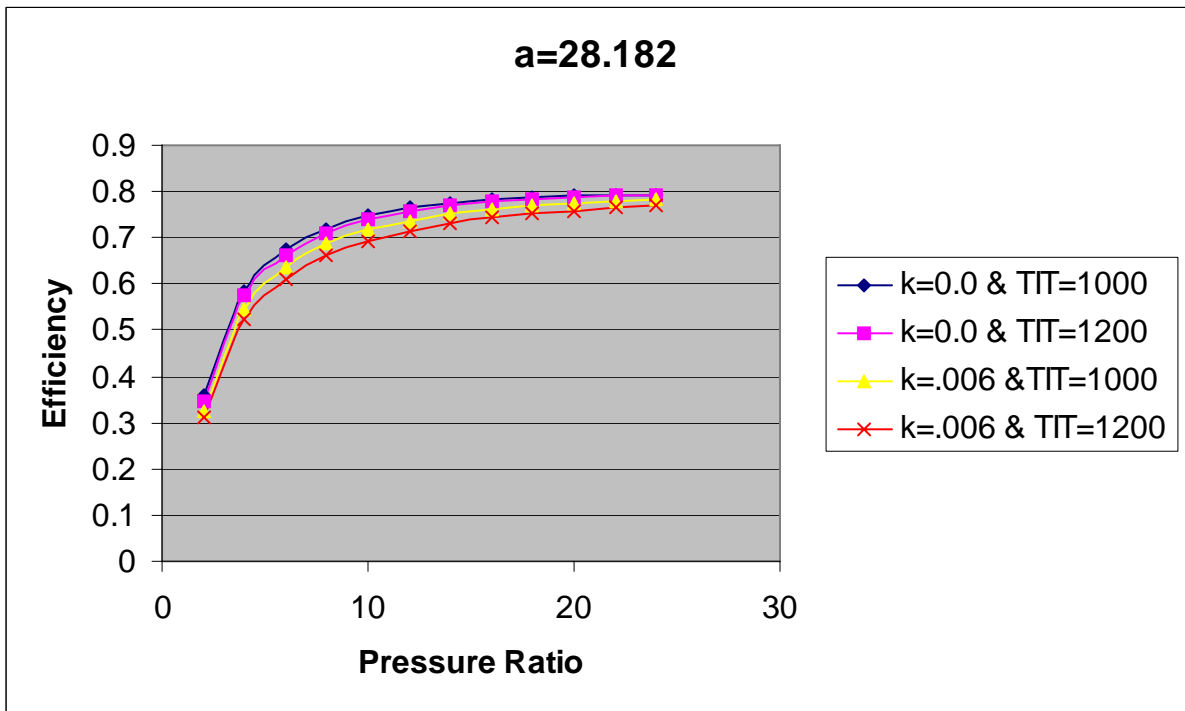


Fig 3.2.16 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler

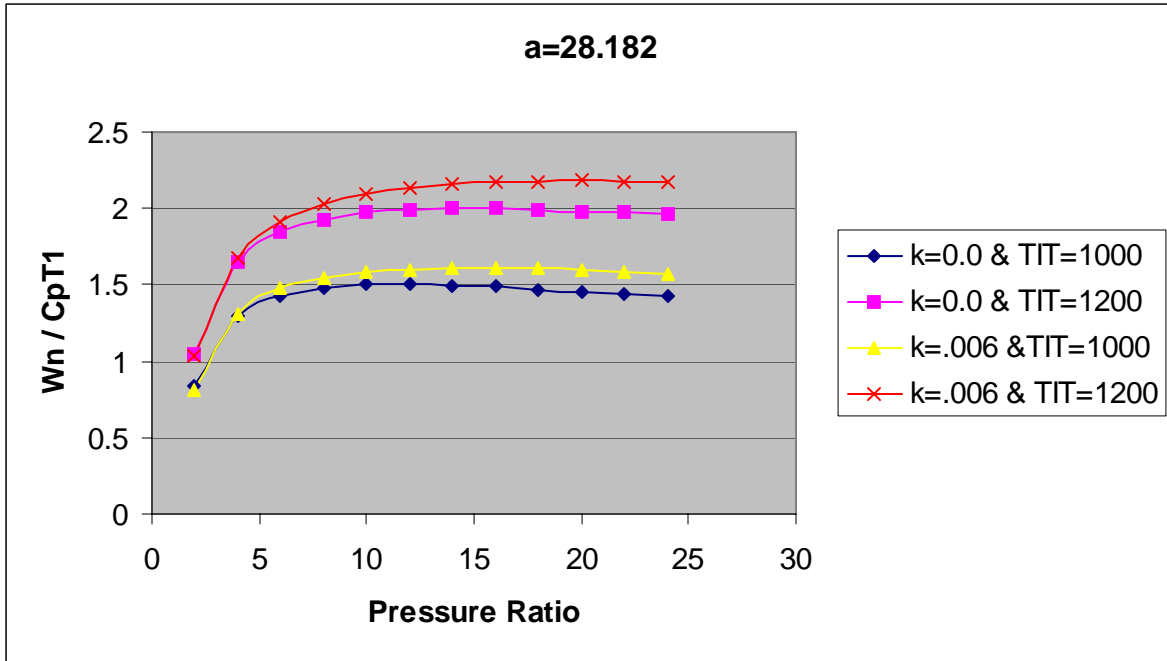


Fig 3.2.17 Variation of W_n/C_pT_1 Vs Pressure ratio with one intercooler

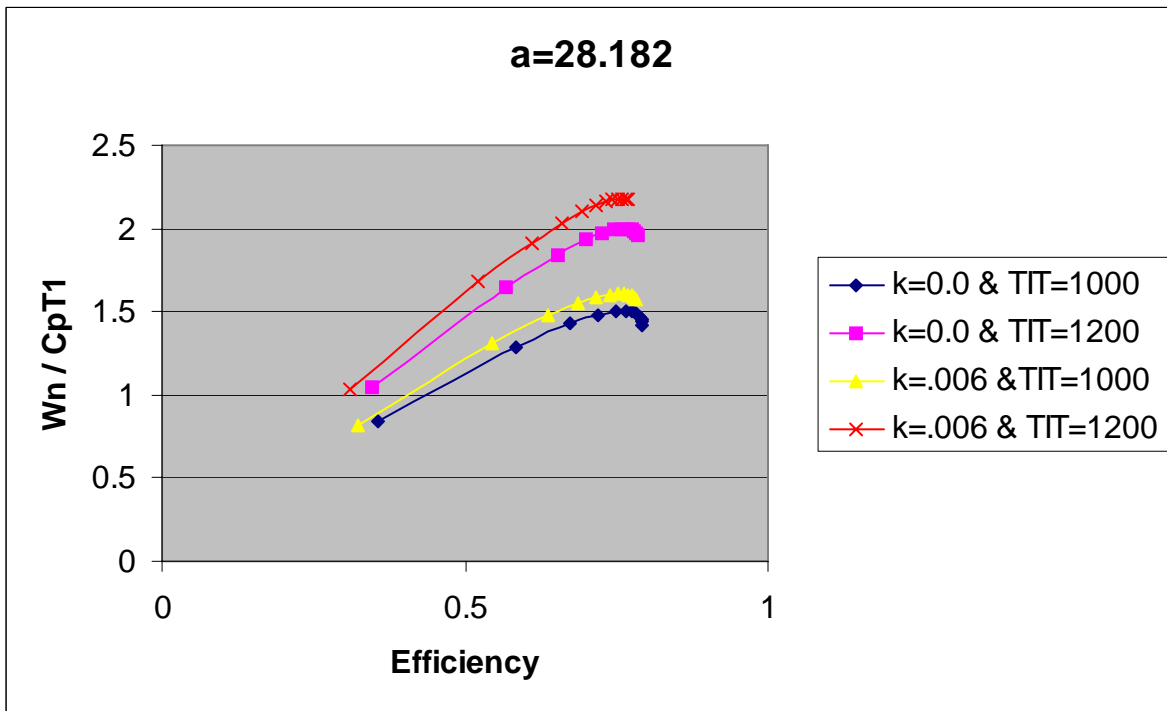


Fig 3.2.18 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one intercooler

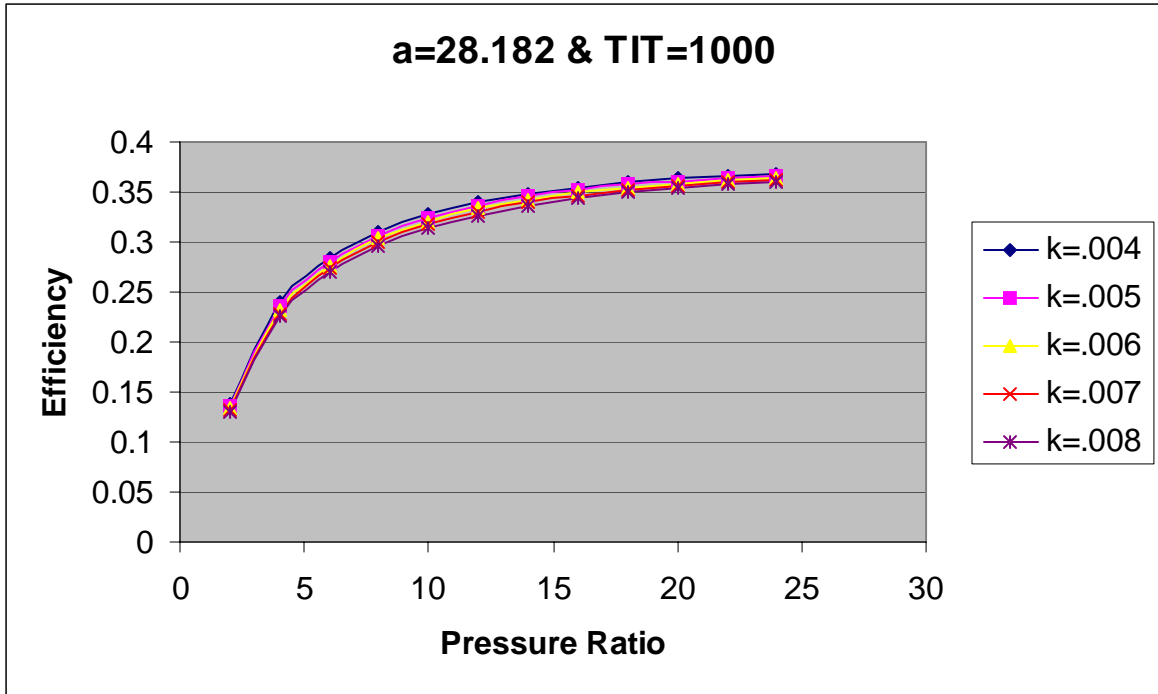


Fig 3.3.1 Variation of Efficiency of gas turbine Vs Pressure ratio with one Reheat

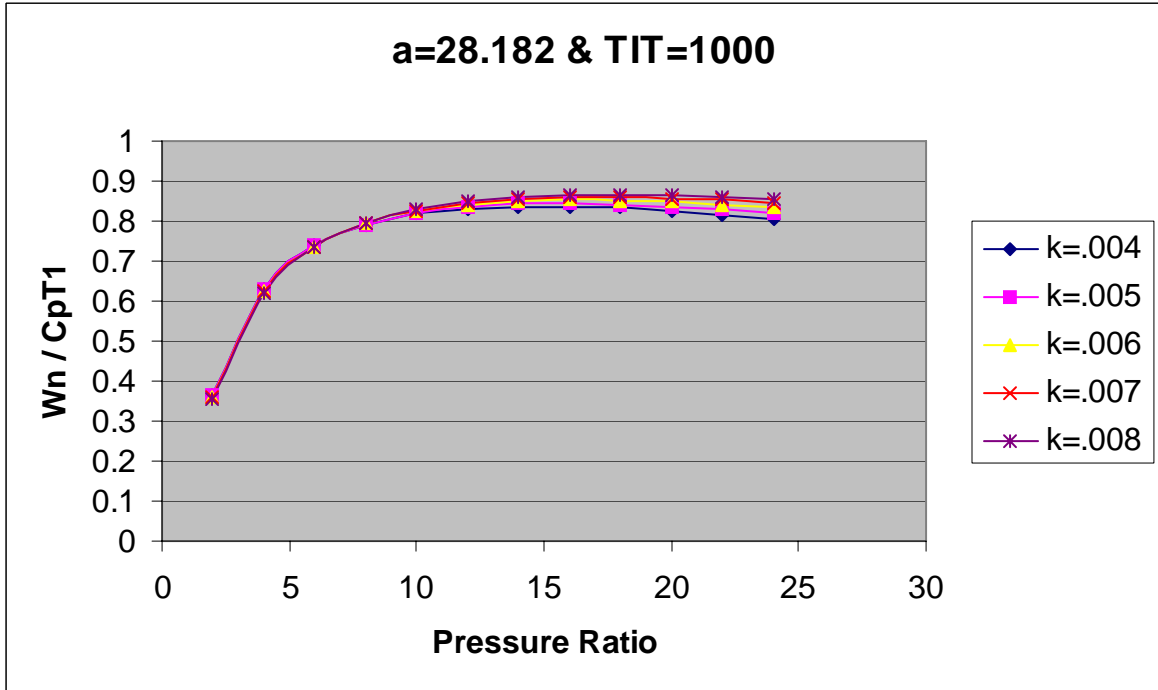


Fig 3.3.2 Variation of $W_n / C_p T_1$ Vs Pressure ratio with one Reheat

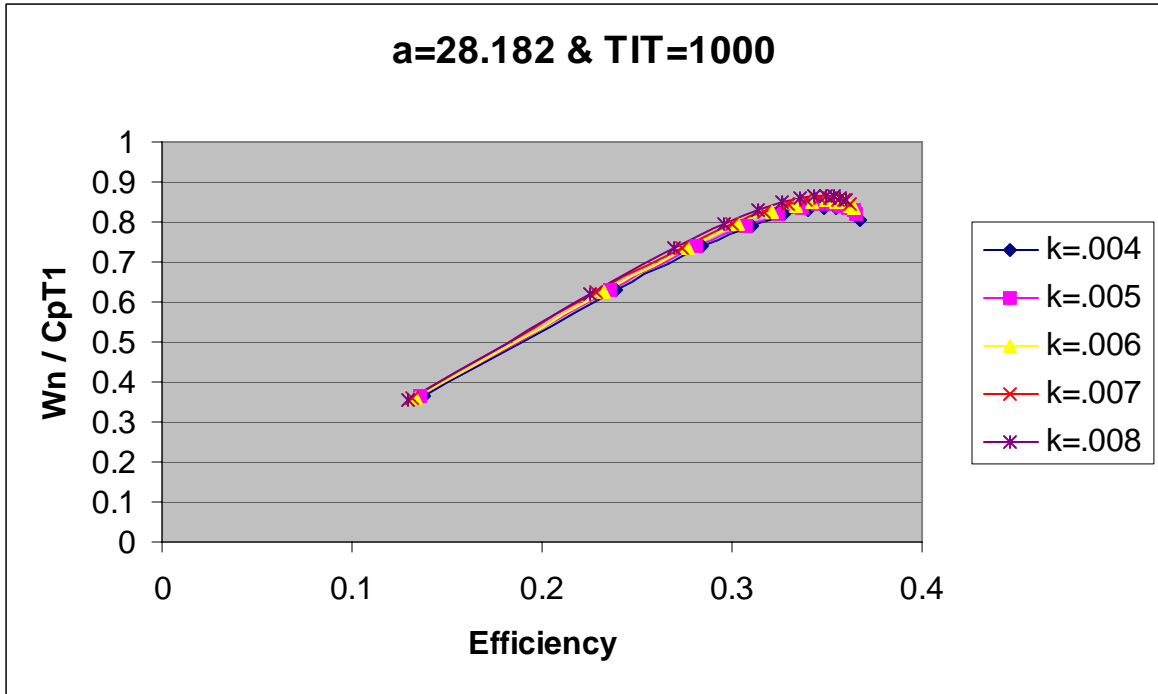


Fig 3.3.3 Variation of $W_n / C_p T_1$ Vs Efficiency of gas turbine with one Reheat

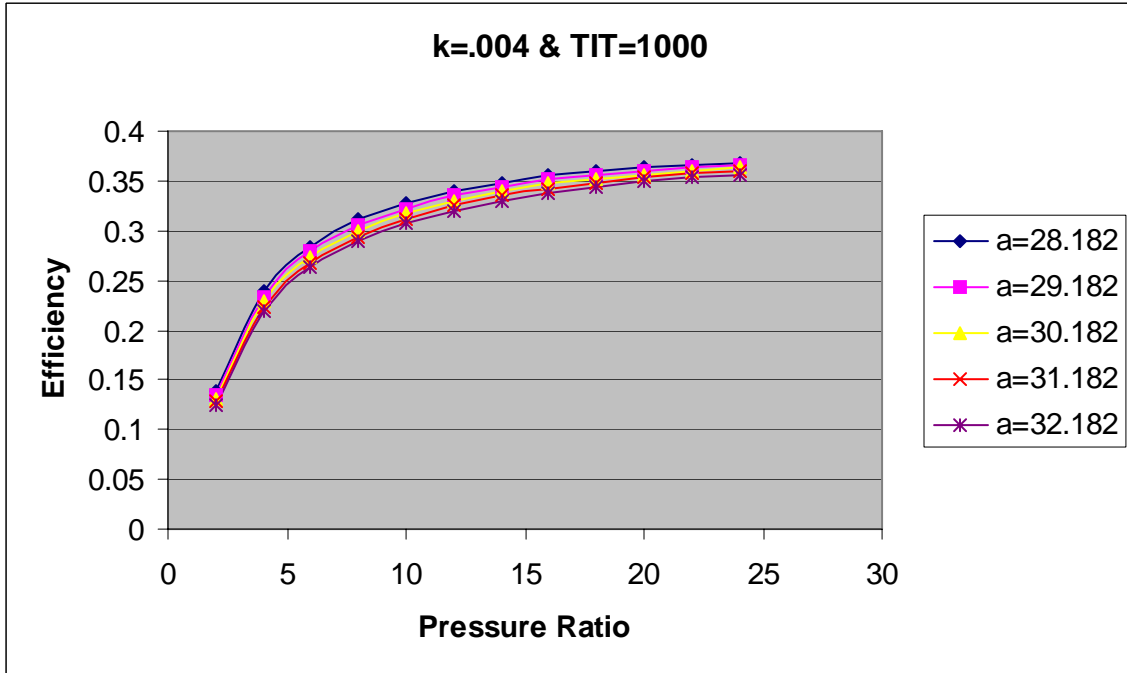


Fig 3.3.4 Variation of Efficiency of gas turbine Vs Pressure ratio with one Reheat

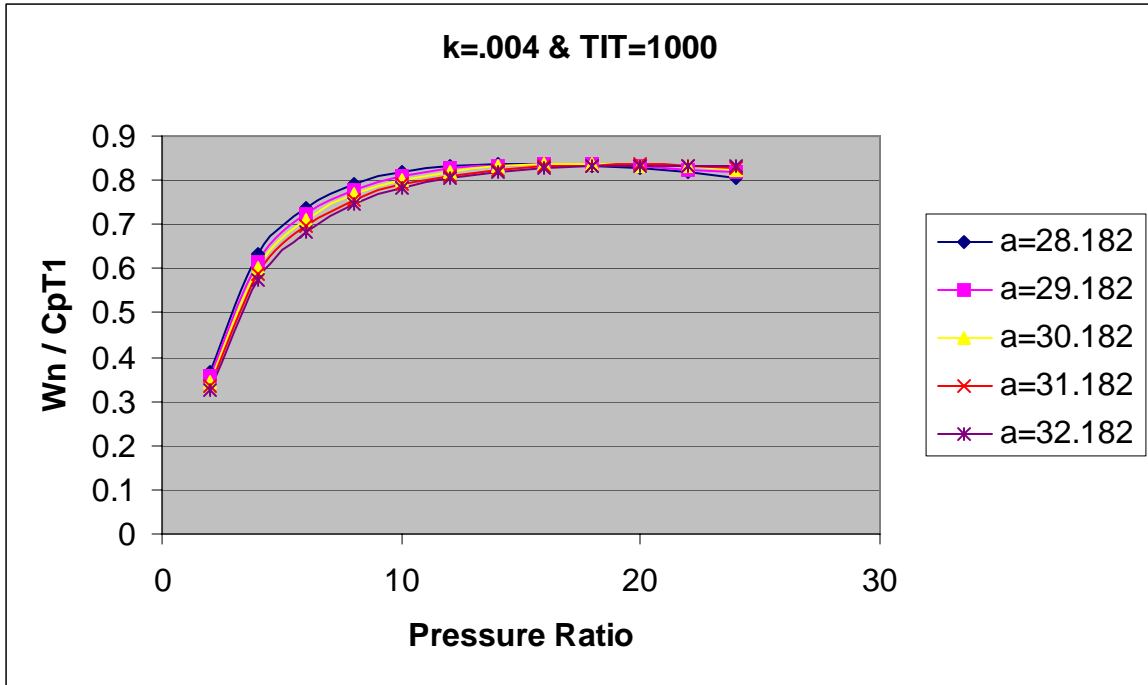


Fig 3.3.5 Variation of W_n/C_pT_1 Vs Pressure ratio with one Reheat

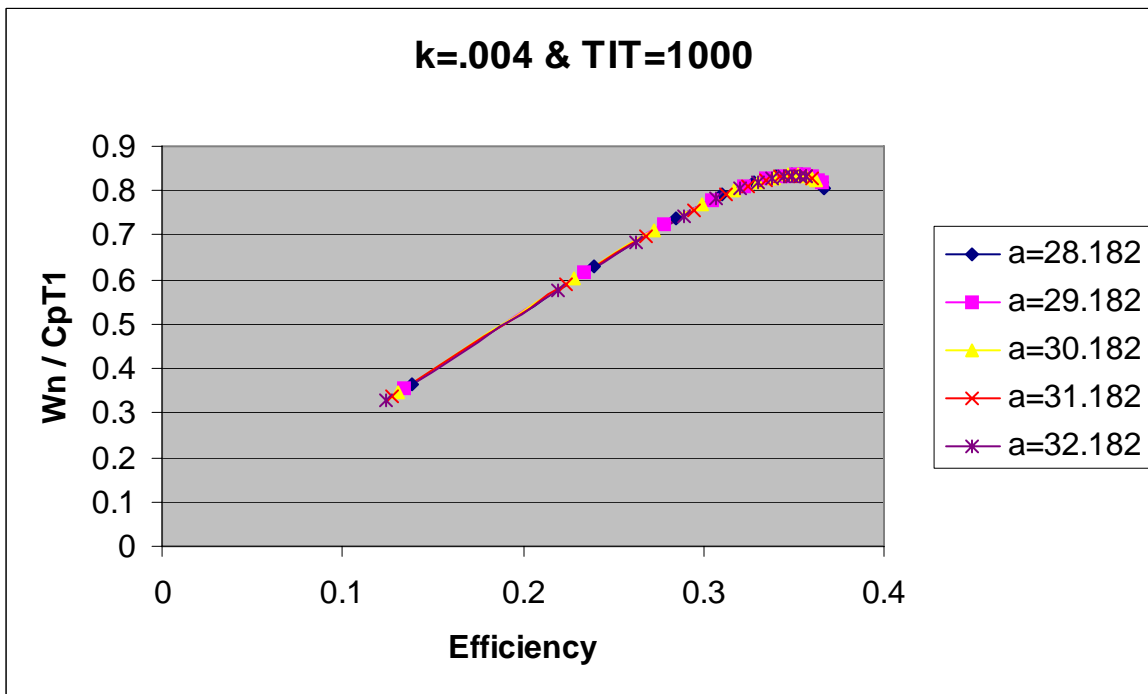


Fig 3.3.6 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one Reheat

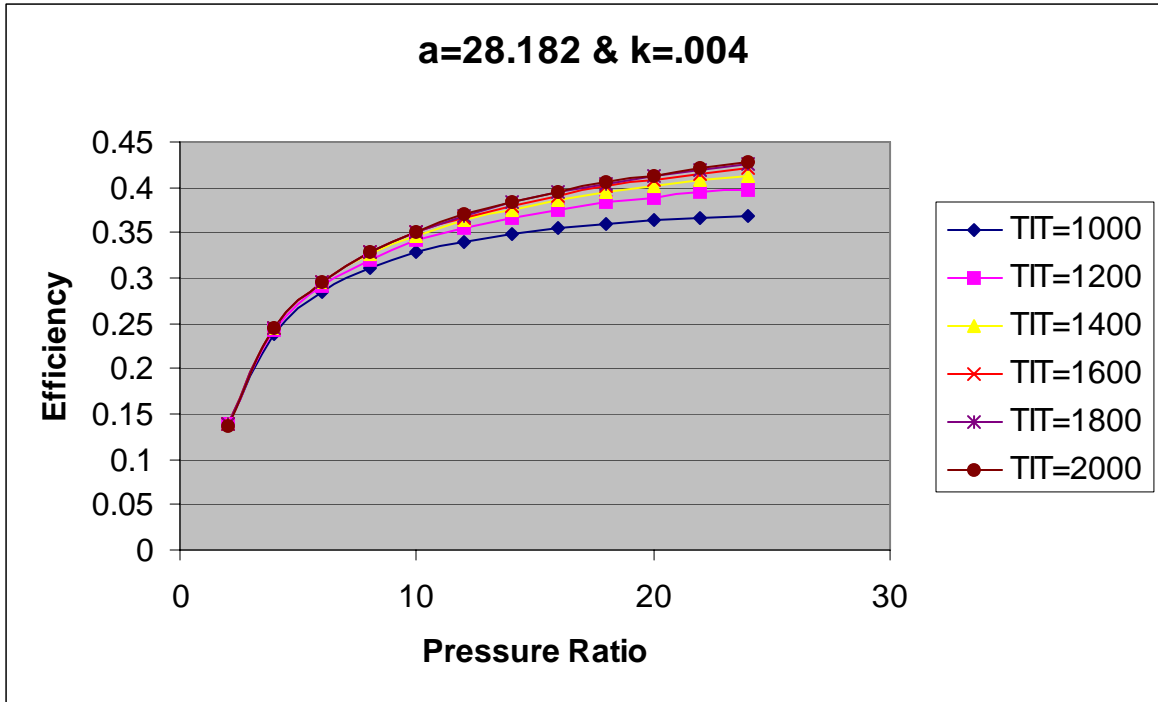


Fig 3.3.7 Variation of Efficiency of gas turbine Vs Pressure ratio with one Reheat

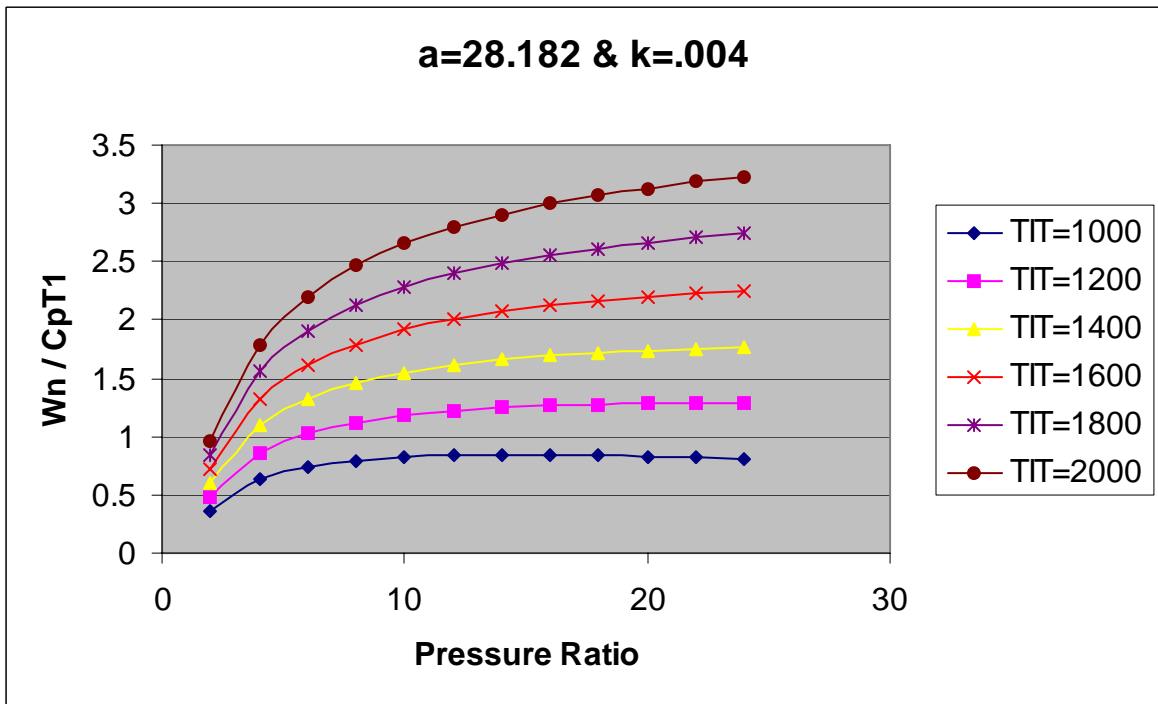


Fig 3.3.8 Variation of W_n/C_pT_1 Vs Pressure ratio with one Reheat

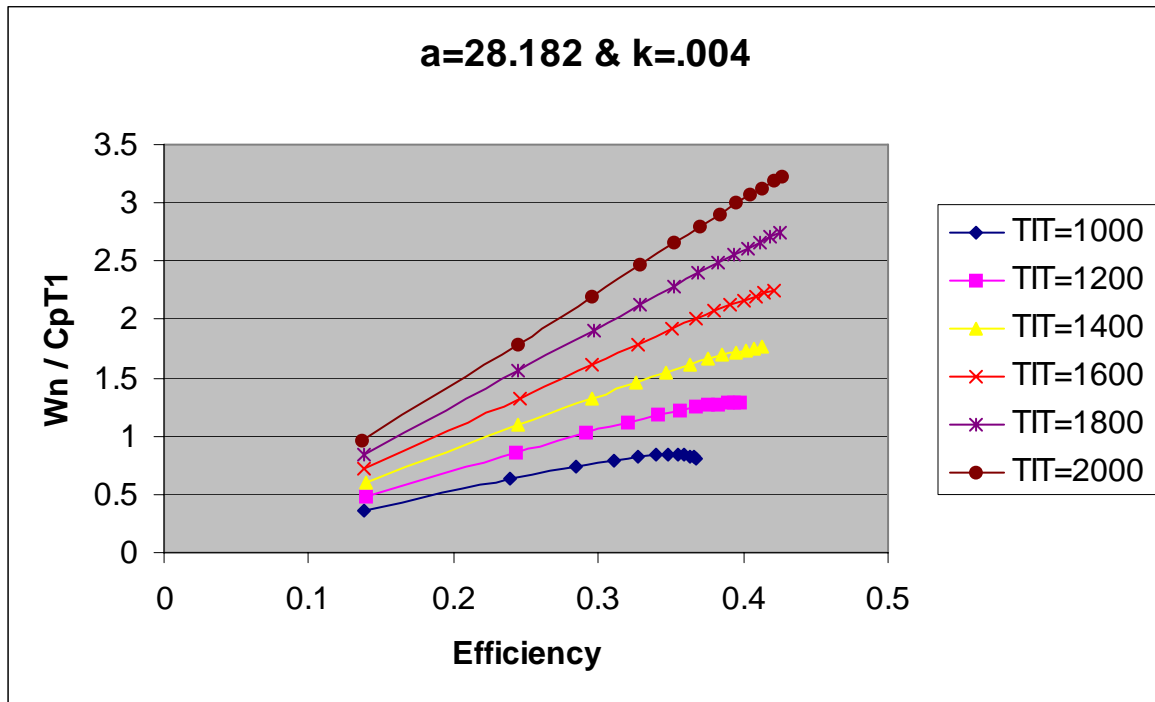


Fig 3.3.9 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one Reheat

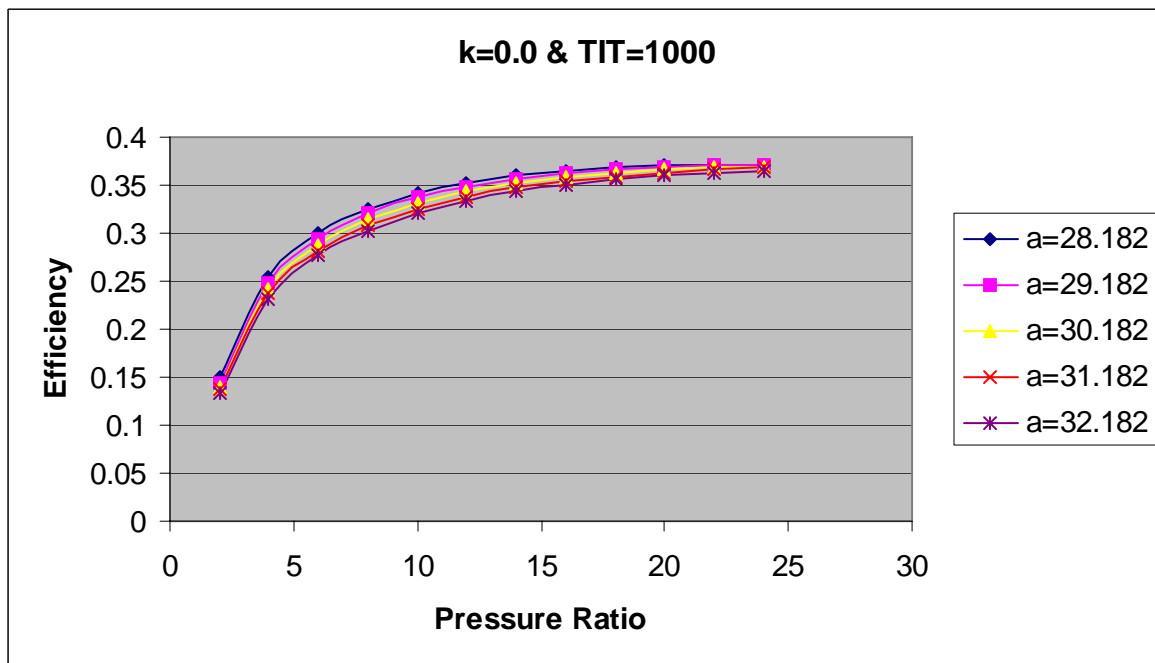


Fig 3.3.10 Variation of Efficiency of gas turbine Vs Pressure ratio with one Reheat

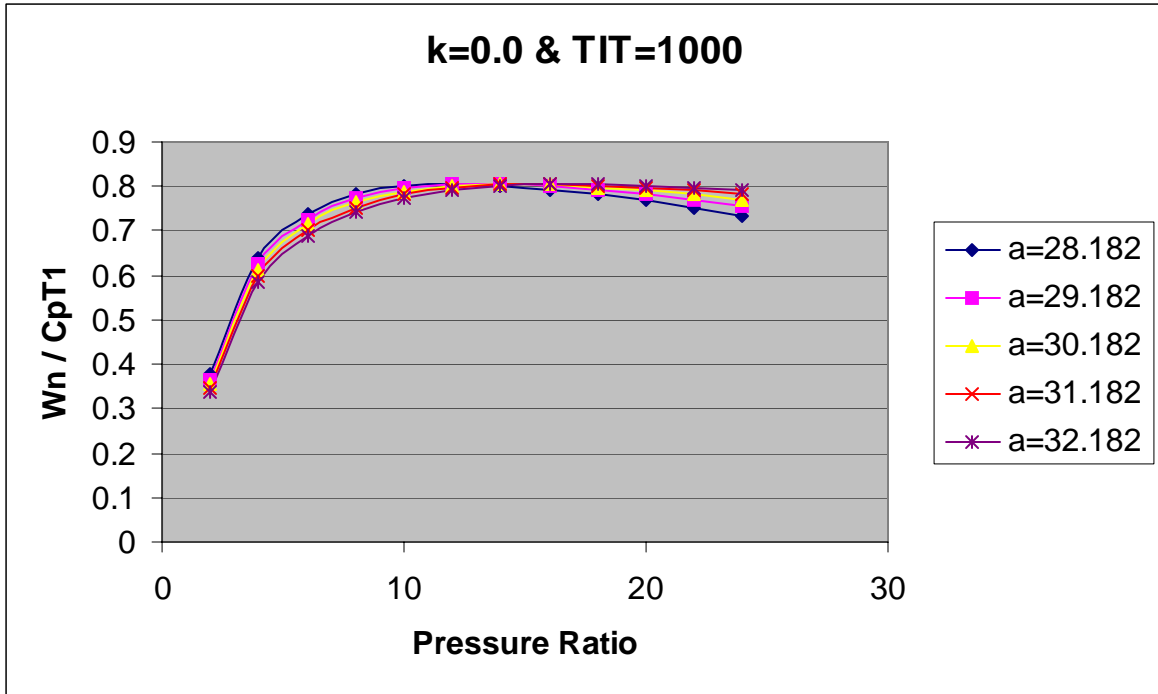


Fig 3.3.11 Variation of W_n/C_pT_1 Vs Pressure ratio with one Reheat

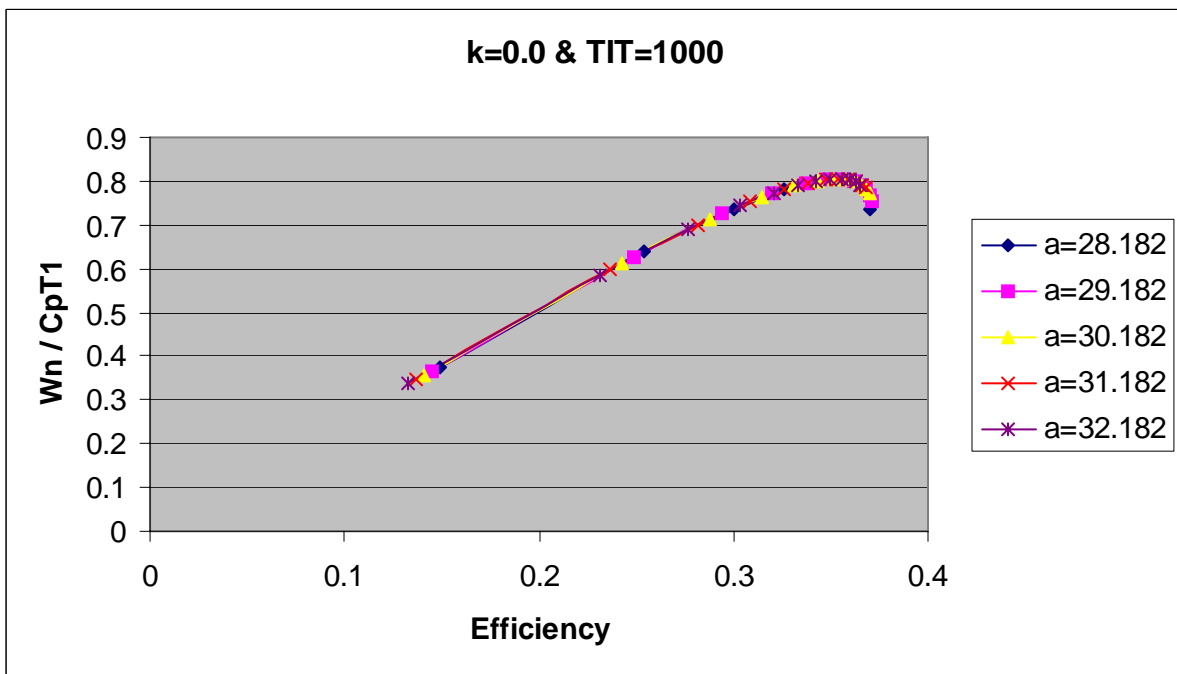


Fig 3.3.12 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one Reheat

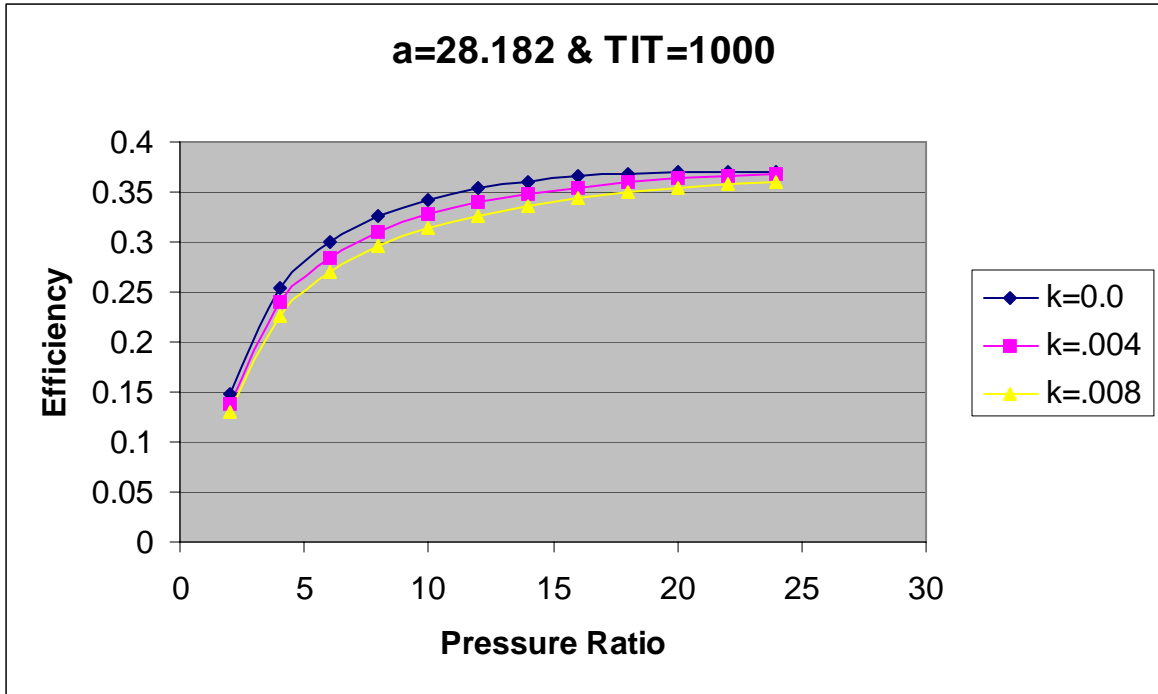


Fig 3.3.13 Variation of Efficiency of gas turbine Vs Pressure ratio with one Reheat

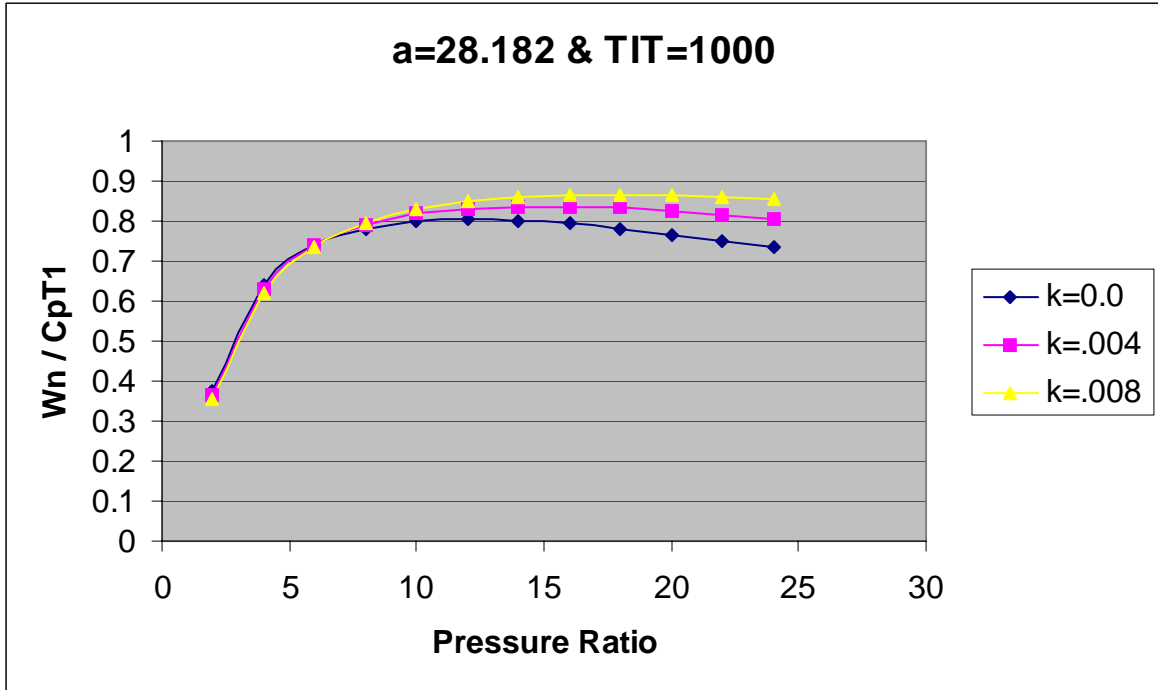


Fig 3.3.14 Variation of W_n/C_pT_1 Vs Pressure ratio with one Reheat

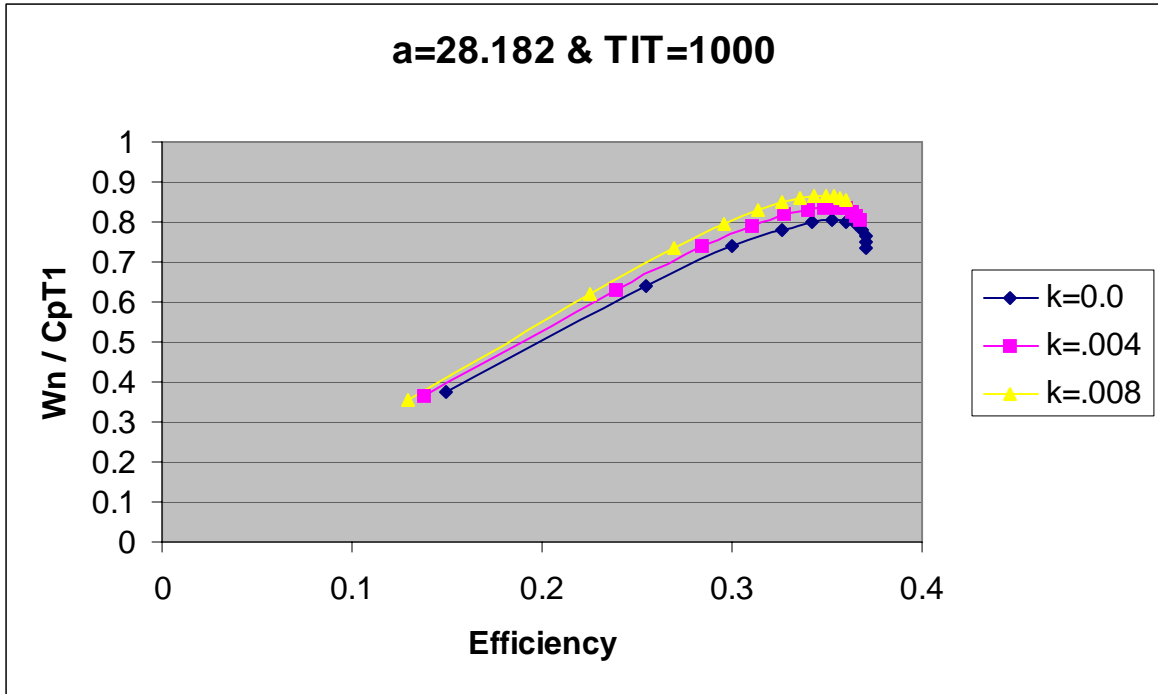


Fig 3.3.15 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one Reheat

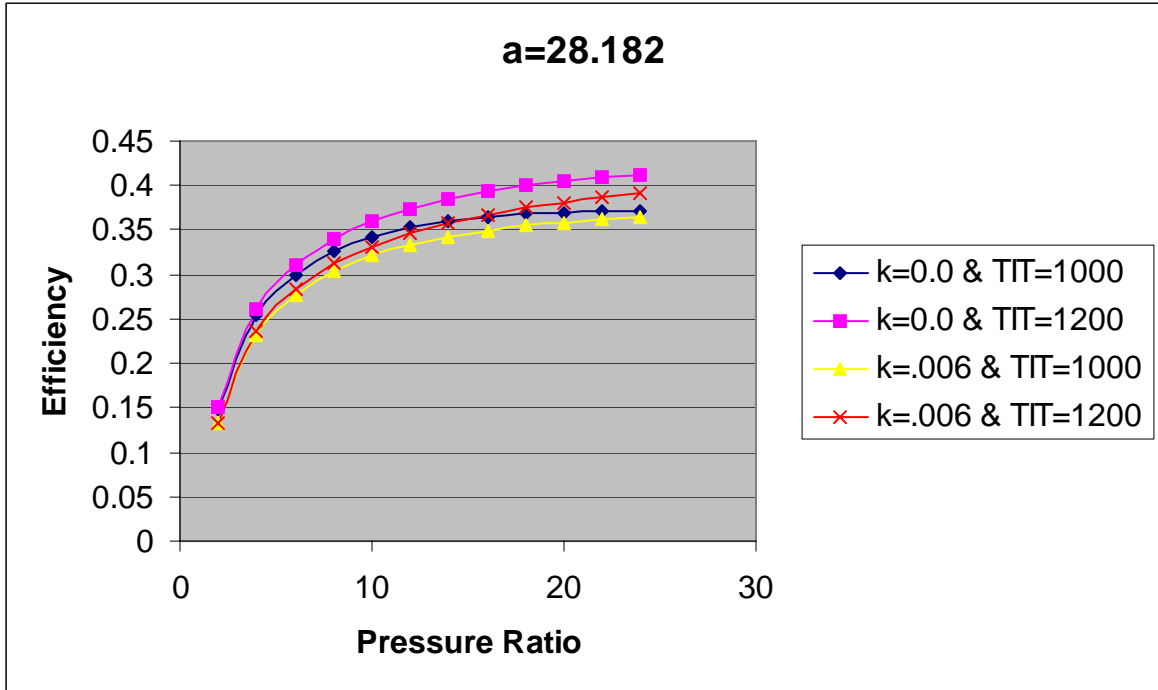


Fig 3.3.16 Variation of Efficiency of gas turbine Vs Pressure ratio with one Reheat

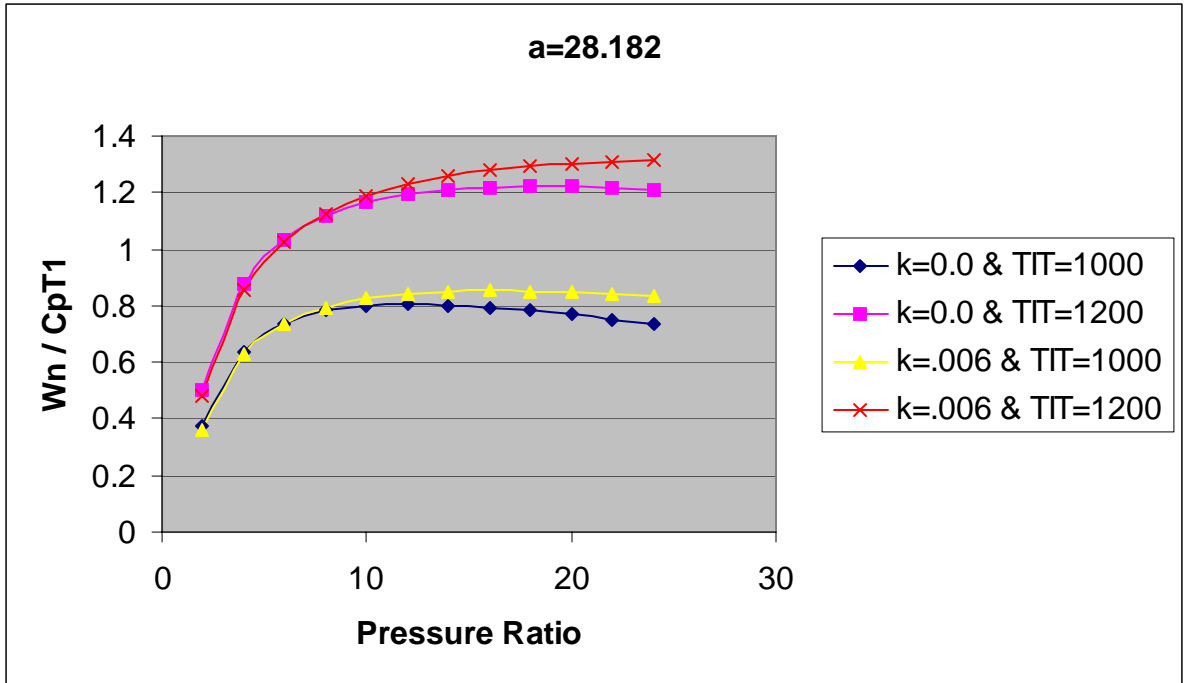


Fig 3.3.17 Variation of W_n/C_pT_1 Vs Pressure ratio with one Reheat

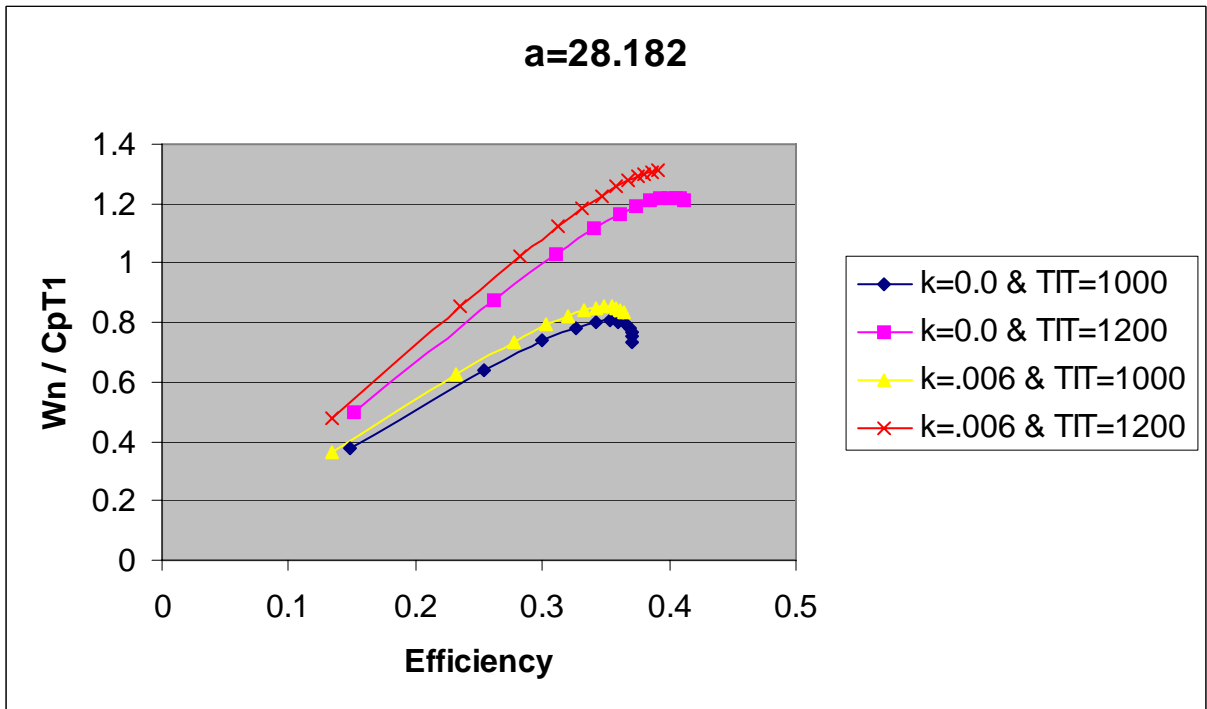


Fig 3.3.18 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one Reheat

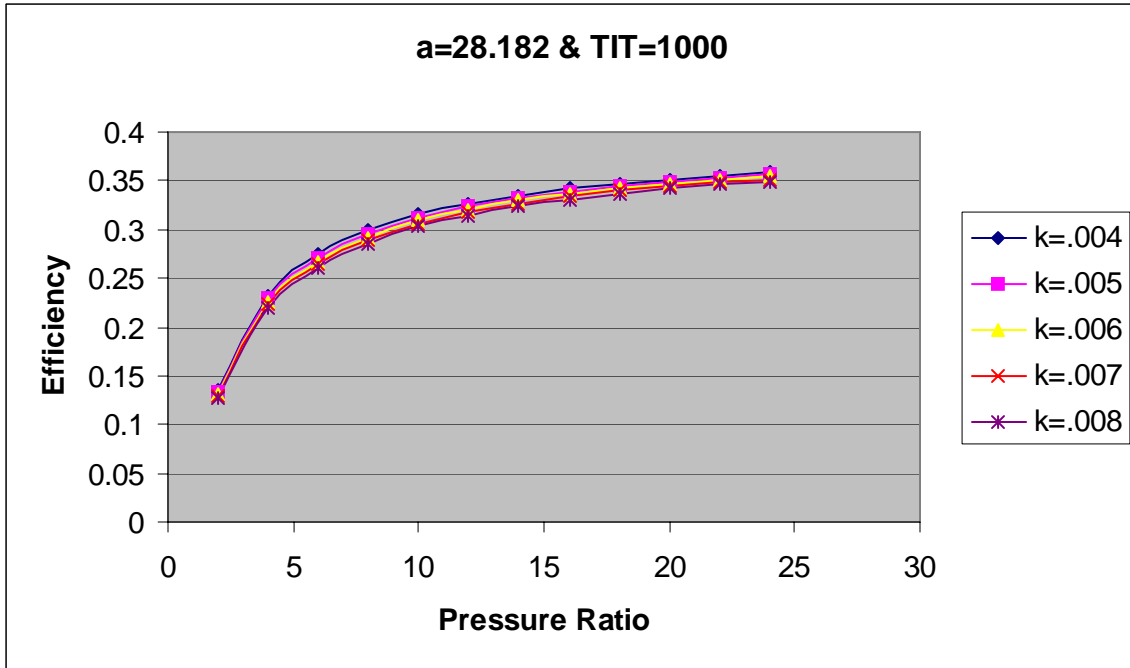


Fig 3.4.1 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler and one Reheat

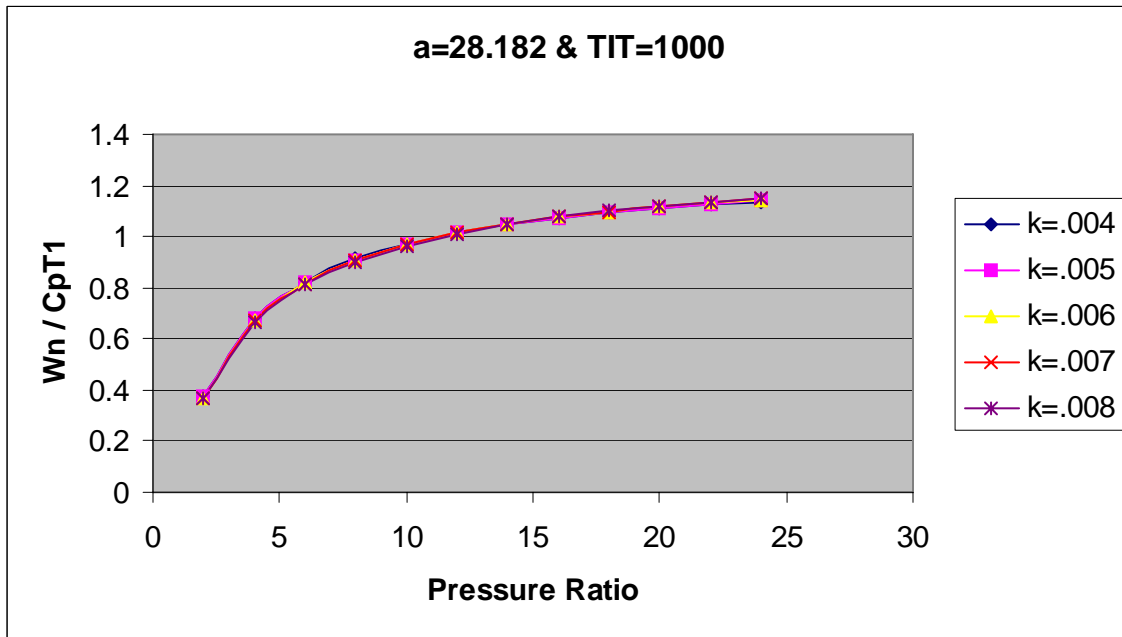


Fig 3.4.2 Variation of $W_n / C_p T_1$ Vs Pressure ratio with one intercooler and one Reheat

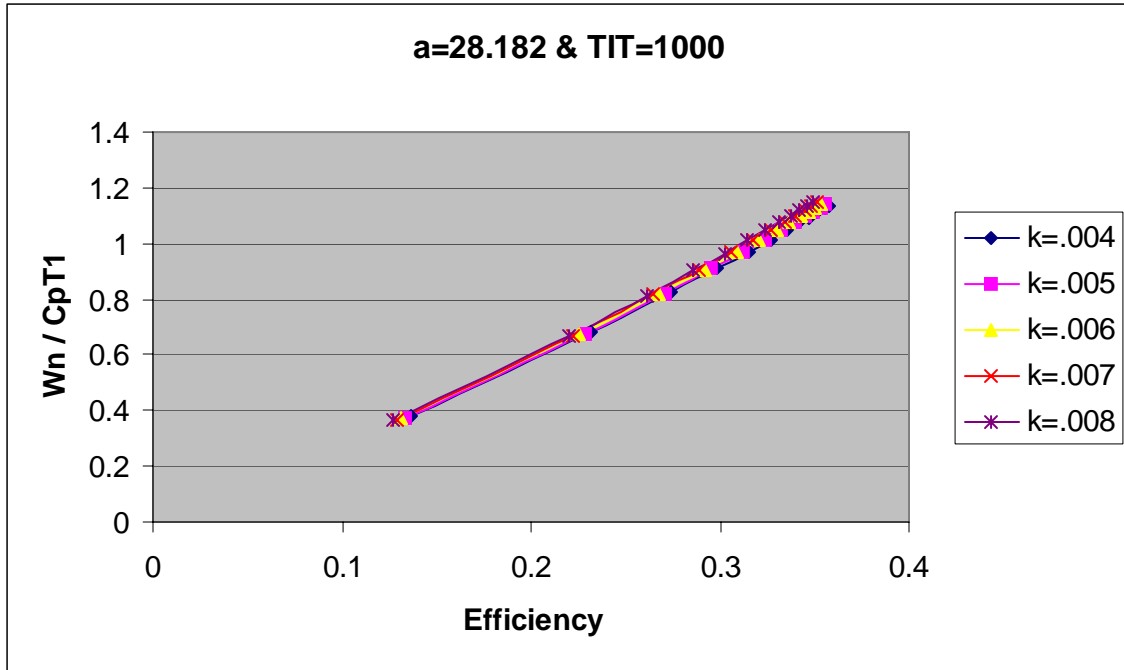


Fig 3.4.3 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one intercooler and one Reheat

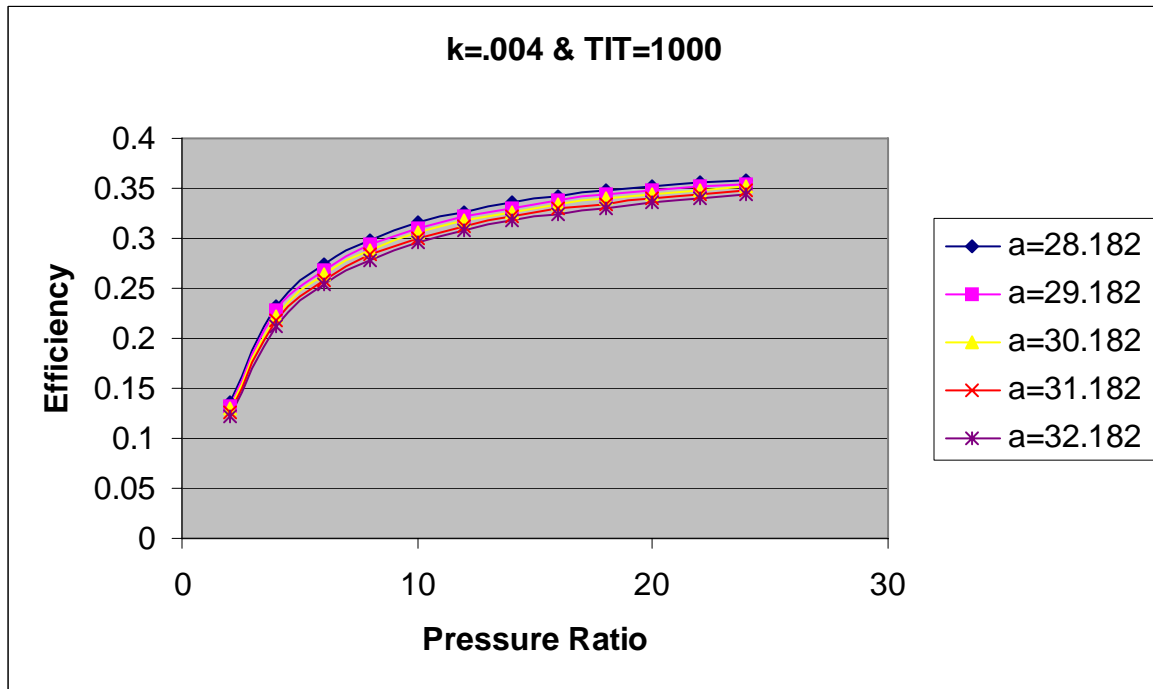


Fig 3.4.4 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler and one Reheat

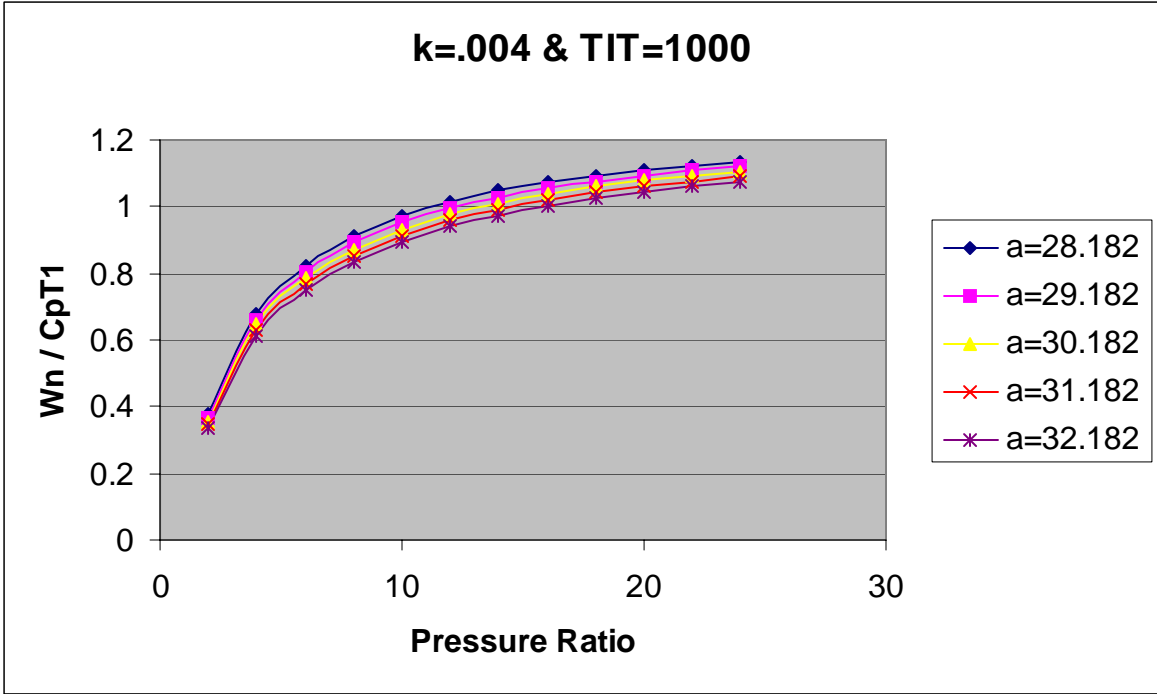


Fig 3.4.5 Variation of W_n/C_pT_1 Vs Pressure ratio with one intercooler and one Reheat

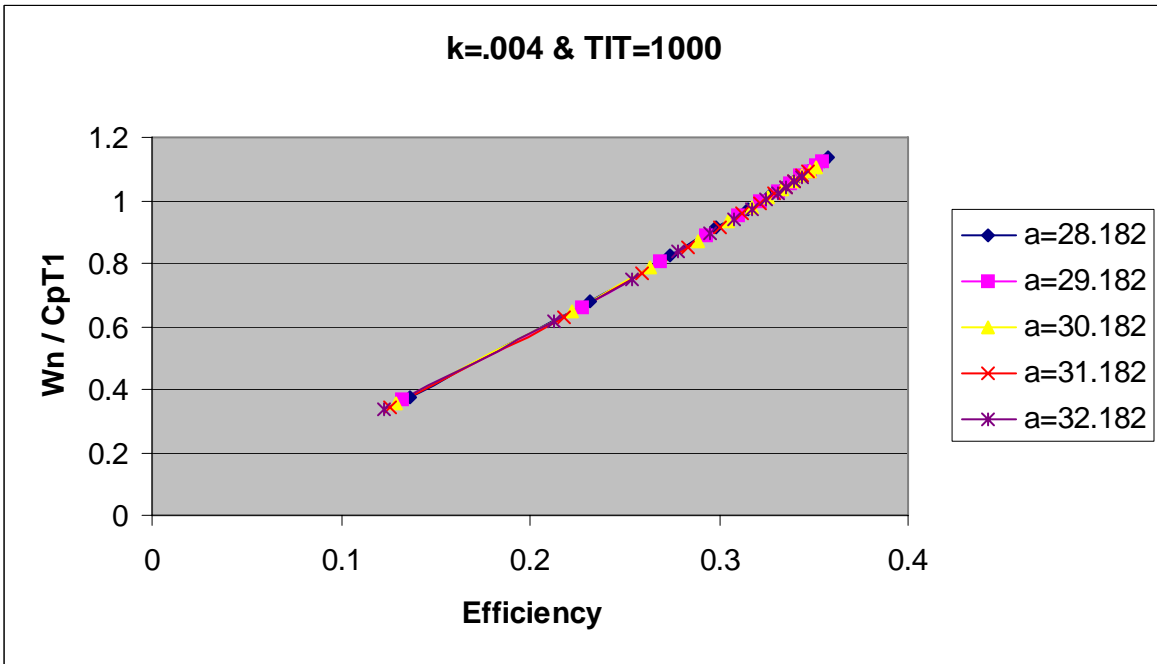


Fig 3.4.6 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one intercooler and one Reheat

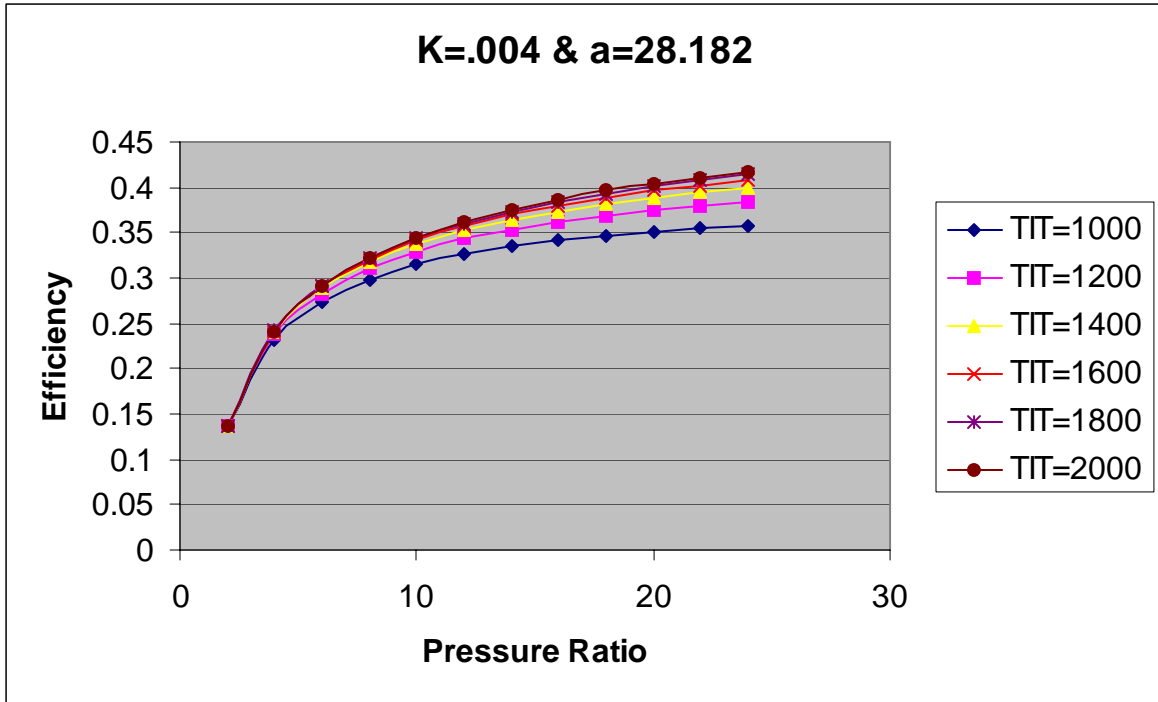


Fig 3.4.7 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler and one Reheat

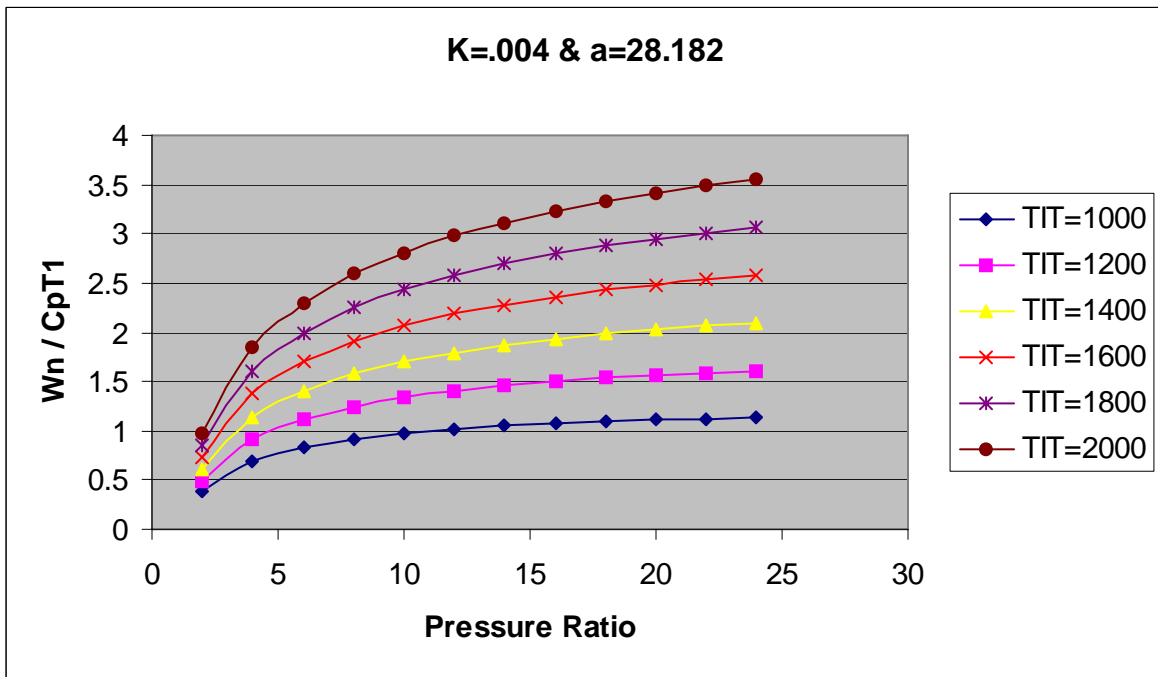


Fig 3.4.8 Variation of $W_n / C_p T_1$ Vs Pressure ratio with one intercooler and one Reheat

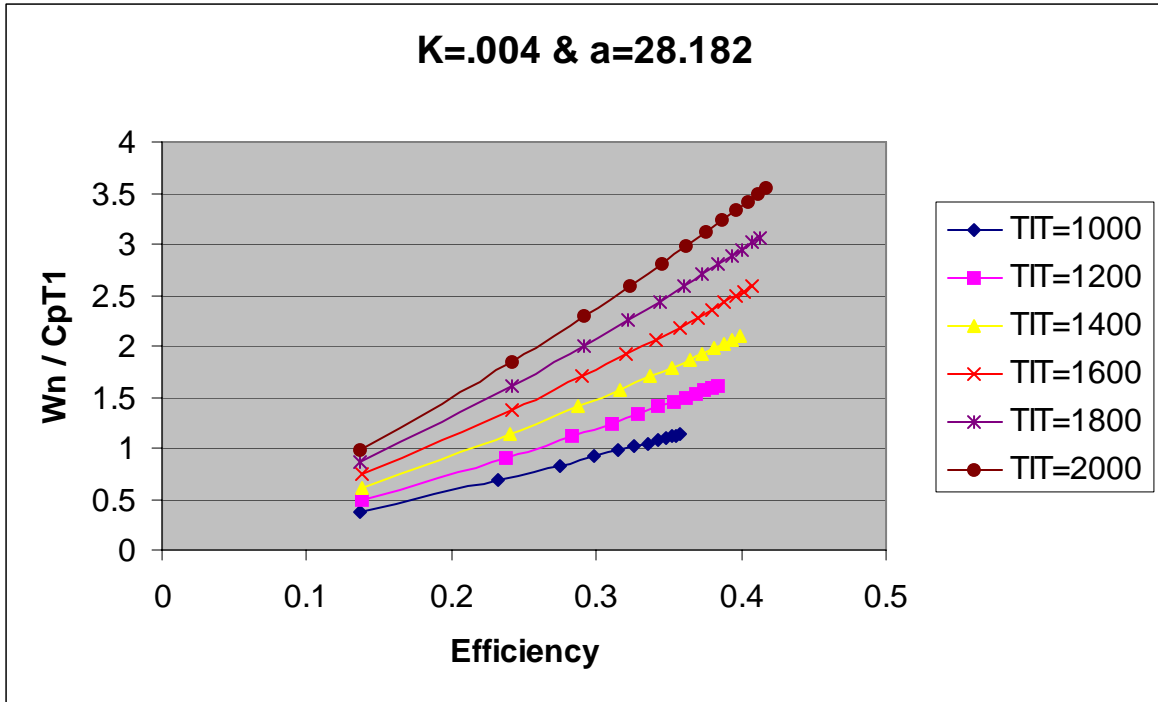


Fig 3.4.9 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one intercooler and one Reheat

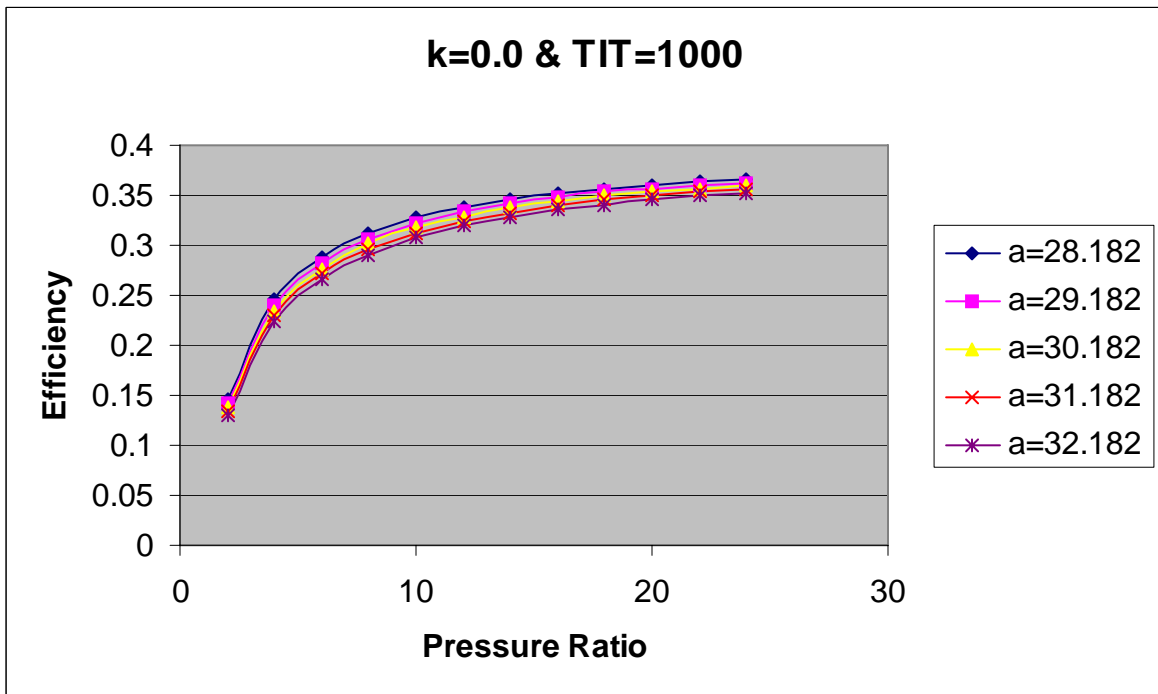


Fig 3.4.10 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler and one Reheat

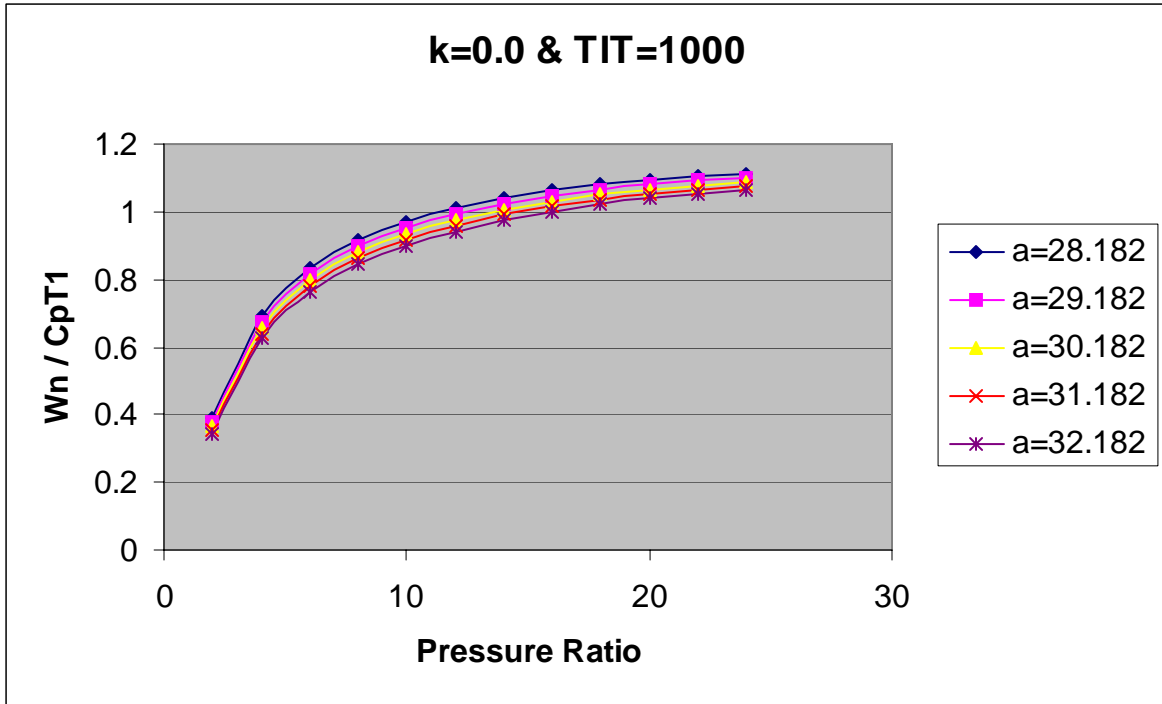


Fig 3.4.11 Variation of W_n/C_pT_1 Vs Pressure ratio with one intercooler and one Reheat

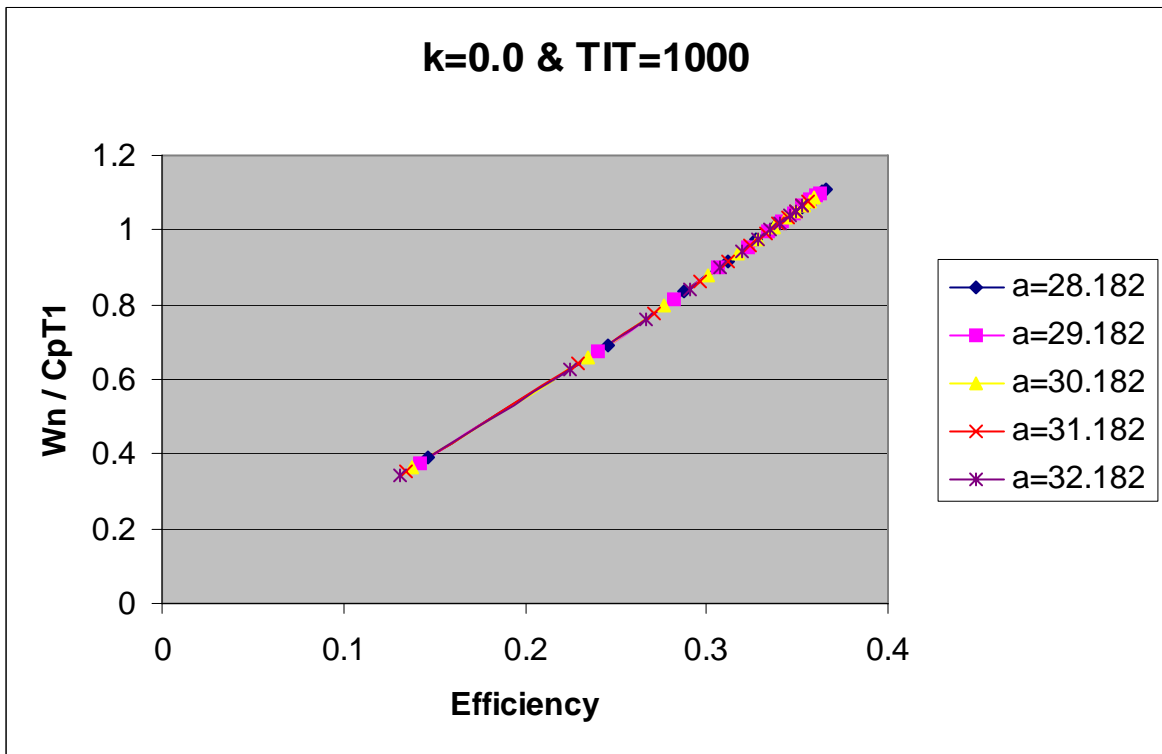


Fig 3.4.12 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one intercooler and one Reheat

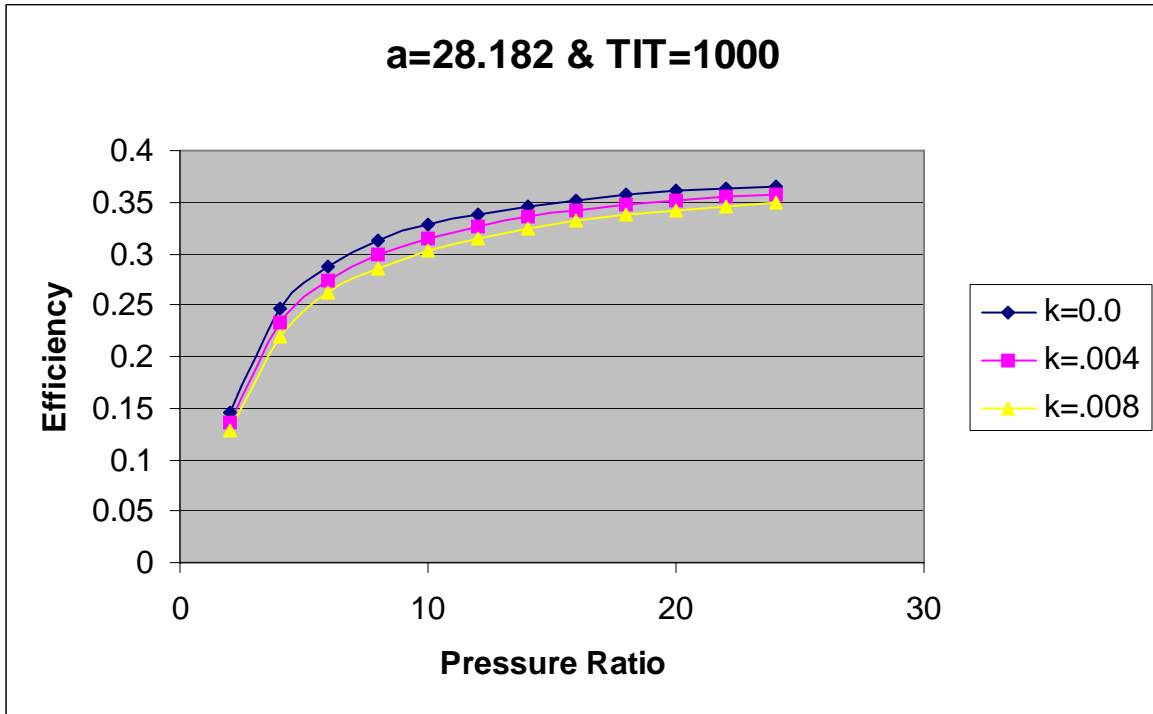


Fig 3.4.13 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler and one Reheat

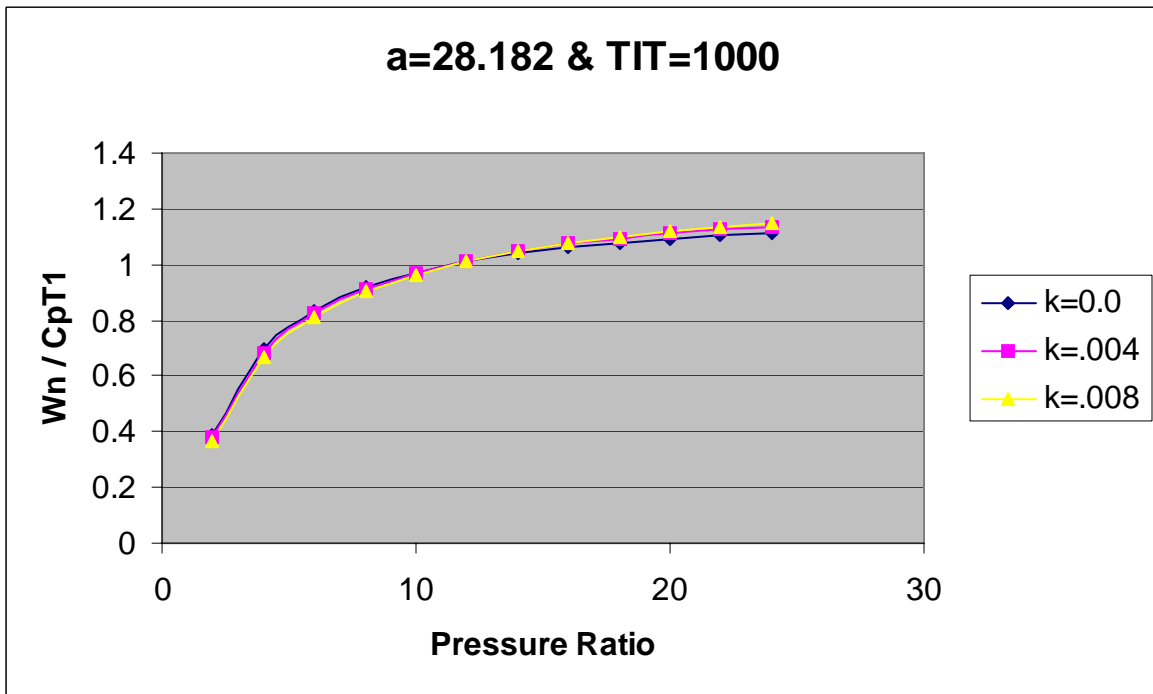


Fig 3.4.14 Variation of W_n/C_pT_1 Vs Pressure ratio with one intercooler and one Reheat

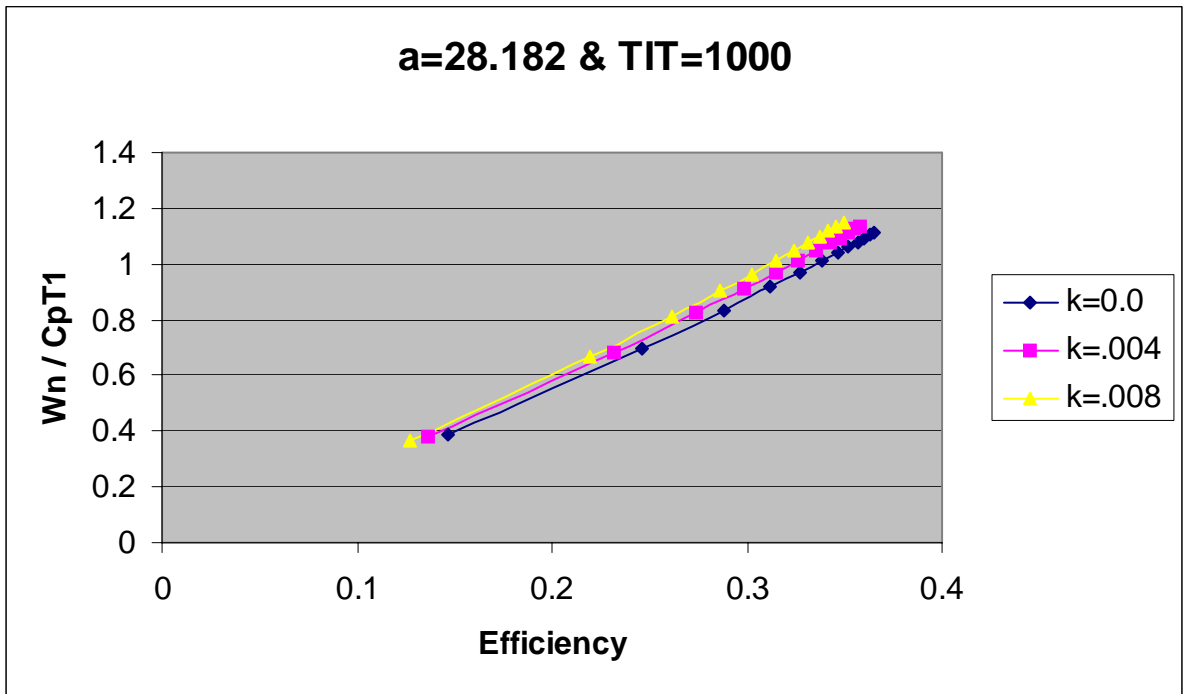


Fig 3.4.15 Variation of $W_n/C_p T_1$ Vs Efficiency of gas turbine with one intercooler and one Reheat

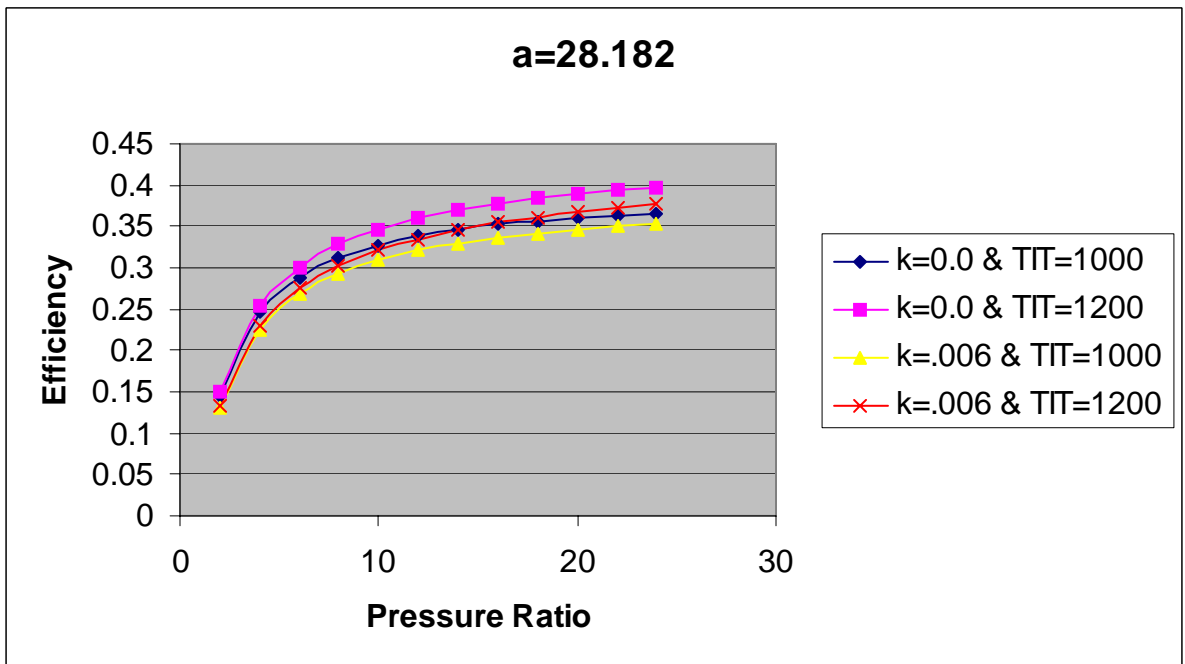


Fig 3.4.16 Variation of Efficiency of gas turbine Vs Pressure ratio with one intercooler and one Reheat

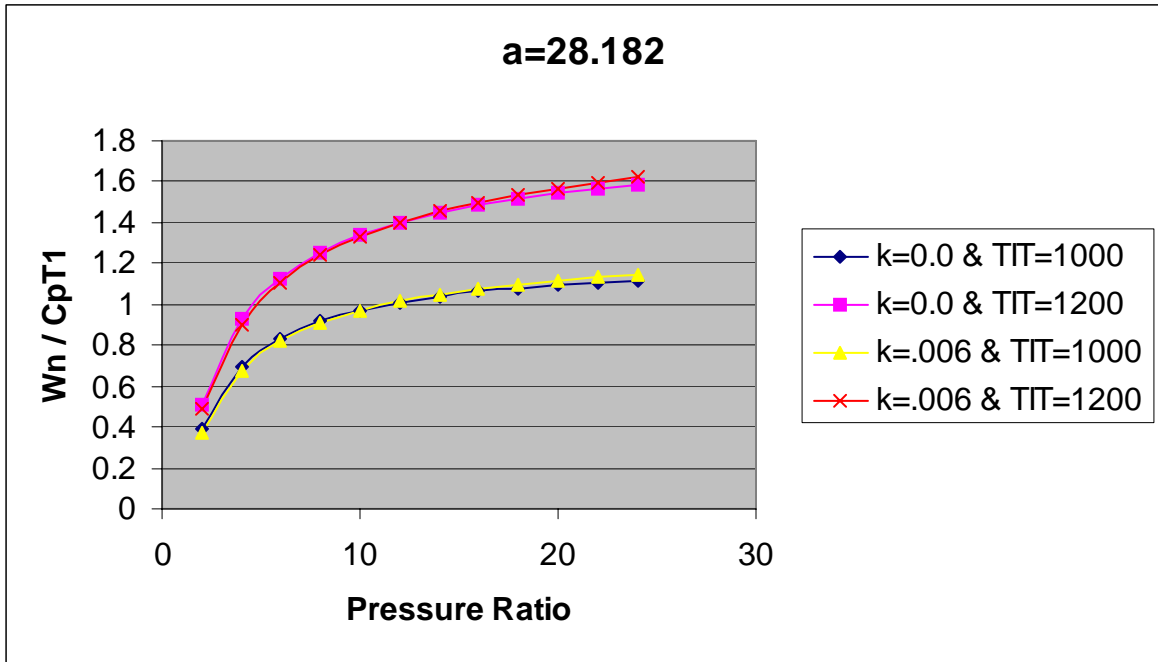


Fig 3.4.17 Variation of W_n/C_pT_1 Vs Pressure ratio with one intercooler and one Reheat

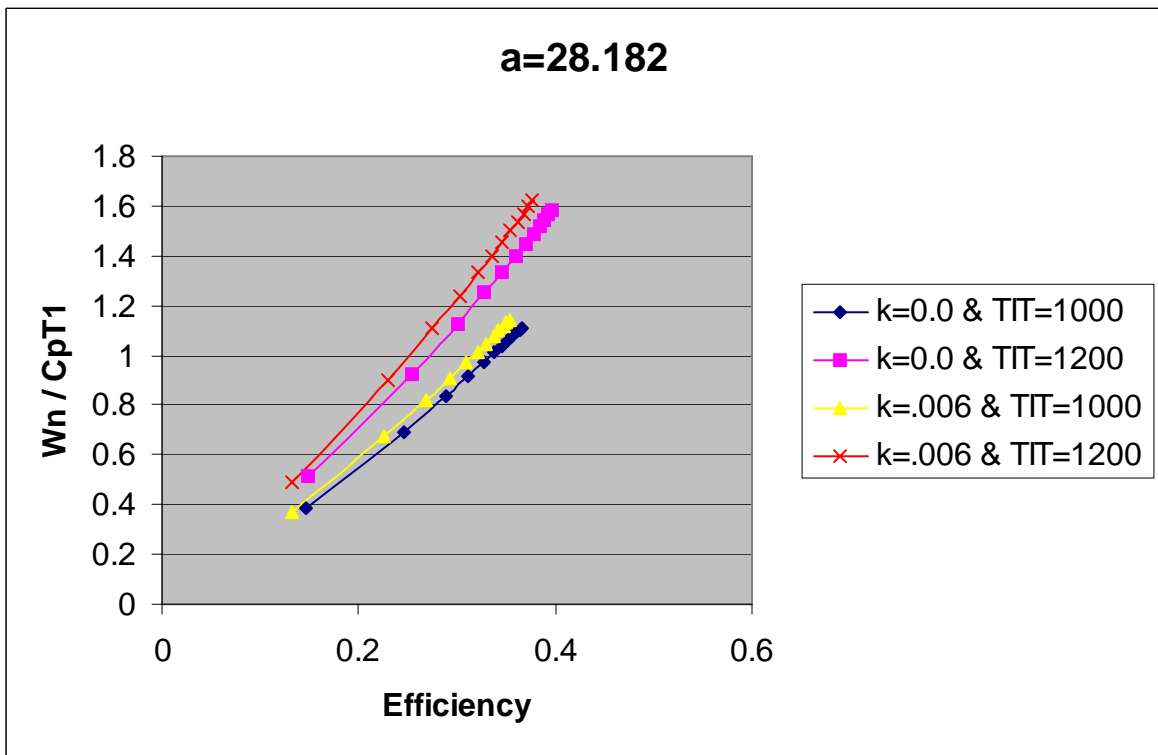


Fig 3.4.18 Variation of W_n/C_pT_1 Vs Efficiency of gas turbine with one intercooler and one Reheat

3.3DISCUSSION OF RESULTS

Graphs for simple gas turbine

FROM GRAPH 3.1.1

- For each value of k , the efficiency of the cycle increases with increase in pressure ratio of the cycle.
- For the increasing value of k , the efficiency of the cycle decreases for the same value of the pressure ratio.
- For the higher value of the pressure ratio, the difference between the efficiency of the cycle for two different values of k decreases.

FROM GRAPH 3.1.2

- For each value of k , the ratio of $W_n / C_p T_1$ first increases then decreases with the pressure ratio.
- For increasing value of k , ratio of $W_n / C_p T_1$ increases for the same pressure ratio.
- For the increasing value of k , the optimum pressure ratio for the maximum value of $W_n / C_p T_1$ shifts toward higher pressure ratio.

FROM GRAPH 3.1.3

- For the increasing value of k , the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of k , the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of k , the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.1.4

- For each value of 'a', the efficiency of the cycle increases with increase in pressure ratio of the cycle.
- For the increasing value of 'a', the efficiency of the cycle decreases for the same value of the pressure ratio.
- For the higher value of the pressure ratio, the difference between the efficiency of the cycle for two different values of 'a' decreases.

FROM GRAPH 3.1.5

- For each value of 'a', the ratio $W_n / C_p T_1$ first increases and then decreases.
- For an increasing value of 'a', the ratio $W_n / C_p T_1$ decreases upto a certain pressure ratio. After this pressure ratio the higher the value of 'a', higher the ratio $W_n / C_p T_1$.
- With the increasing value of 'a', for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.1.6

- For the increasing value of 'a', the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of 'a', the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of 'a', the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.1.7

- For each value of TIT, the efficiency of the cycle increases as the pressure ratio increases.

- For the increasing value of TIT, the efficiency of the cycle increases for the same pressure ratio.
- Increasing the pressure ratio, the difference between the efficiency of the cycle for two different values of 'TIT' increases.

FROM GRAPH 3.1.8

- For each value of TIT, the ratio $W_n / C_p T_1$ of the cycle increases as the pressure ratio increases.
- For the increasing value of TIT, the ratio $W_n / C_p T_1$ of the cycle increases for the same pressure ratio.
- With the increasing value of 'TIT' , for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.1.9

- For the increasing value of TIT, the maximum value of ratio $W_n / C_p T_1$ of the cycle gets at a higher efficiency.
- For each value of TIT , there is a maximum value of efficiency at any value of ratio $W_n / C_p T_1$.
- With the increasing value of TIT , the maximum efficiency increases for any value of ratio $W_n / C_p T_1$.

FROM GRAPH 3.1.10

- For each value of 'a', the efficiency of the cycle increases.
- For a increasing value of ' a', the efficiency of the cycle decreases upto a certain pressure ratio. After this pressure ratio the higher the value of ' a' , higher the efficiency of the cycle .

- With the increasing value of 'a', for the maximum value of the efficiency of the cycle, the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.1.11

- For each value of 'a' the ratio $W_n / C_p T_1$ first increases and then decreases.
- For a increasing value of 'a' the ratio $W_n / C_p T_1$ decreases upto a certain pressure ratio. After this pressure ratio the higher the value of 'a', higher the ratio $W_n / C_p T_1$.
- With the increasing value of 'a', for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.1.12

- For the increasing value of 'a', the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of 'a', the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of 'a', the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.1.13

- For each value of 'a', the efficiency of the cycle increases.
- For a increasing value of 'a', the efficiency of the cycle decreases upto a certain pressure ratio. After this pressure ratio the higher the value of 'a', higher the efficiency of the cycle.
- With the increasing value of 'a', for the maximum value of the efficiency of the cycle, the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.1.14

- For each value of k , the ratio of $W_n / C_p T_1$ first increases then decreases with the pressure ratio.
- For increasing value of k , ratio of $W_n / C_p T_1$ increases for the same pressure ratio.
- For the increasing value of k , the optimum pressure ratio for the maximum value of $W_n / C_p T_1$ shifts toward higher pressure ratio.

FROM GRAPH 3.1.15

- For the increasing value of k , the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of k , the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of k , the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.1.16

- At $TIT = 1000$, the efficiency first decreases with the pressure ratio as increasing the ' k ' but after a certain pressure ratio efficiency of the cycle increases as the ' k ' increases.
- At $TIT = 1200$, the efficiency first decreases with the pressure ratio as increasing the ' k ' and the difference between the efficiency at $k=0.0$ & $k=0.006$ decreases as the pressure ratio increases.

FROM GRAPH 3.1.17

- At TIT =1000, the ratio $W_n / C_p T_1$ first decreases with the pressure ratio as increasing the 'k' but after a certain pressure ratio, the ratio $W_n / C_p T_1$ of the cycle increases as the 'k' increases.
- At TIT =1200, the ratio $W_n / C_p T_1$ first decreases with the pressure ratio as increasing the 'k' but after a certain pressure ratio, the ratio $W_n / C_p T_1$ increases as the 'k' increases. But the pressure ratio after which ratio $W_n / C_p T_1$ increases with the 'k' increases, shifts toward high-pressure ratio as compare to TIT=1000.

FROM GRAPH 3.1.18

- At TIT =1000, the maximum value of ratio $W_n / C_p T_1$ gets at a higher efficiency for the increasing value of 'k'.
- At TIT =1200, the maximum value of ratio $W_n / C_p T_1$ gets at a higher efficiency for the increasing value of 'k'. But the value of efficiency for maximum value of ratio $W_n / C_p T_1$ shifts toward high value of efficiency as compare to TIT=1000.

Graphs for the one inter cooler used in compression process

FROM GRAPH 3.2.1

- For each value of k, the efficiency of the cycle increases with increase in pressure ratio of the cycle.
- For the increasing value of k, the efficiency of the cycle decreases for the same value of the pressure ratio.
- For the higher value of the pressure ratio, the difference between the efficiency of the cycle for two different values of k decreases.

FROM GRAPH 3.2.2

- For each value of k , the ratio of $W_n / C_p T_1$ first increases then decreases with the pressure ratio.
- For increasing value of k , ratio of $W_n / C_p T_1$ increases for the same pressure ratio.
- For the increasing value of k , the optimum pressure ratio for the maximum value of $W_n / C_p T_1$ shifts toward higher pressure ratio.

FROM GRAPH 3.2.3

- For the increasing value of k , the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of k , the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of k , the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.2.4

- For each value of 'a', the efficiency of the cycle increases with increase in pressure ratio of the cycle.
- For the increasing value of 'a', the efficiency of the cycle decreases for the same value of the pressure ratio.
- For the higher value of the pressure ratio, the difference between the efficiency of the cycle for two different values of 'a' decreases.

FROM GRAPH 3.2.5

- For each value of 'a', the ratio $W_n / C_p T_1$ first increases and then decreases.

- For a increasing value of ‘a’, the ratio $W_n / C_p T_1$ decreases upto a certain pressure ratio. After this pressure ratio the higher the value of ‘a’, higher the ratio $W_n / C_p T_1$.
- With the increasing value of ‘a’, for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.2.6

- For the increasing value of ‘a’, the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of ‘a’, the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of ‘a’, the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.2.7

- For each value of TIT, the efficiency of the cycle increases as the pressure ratio increases.
- For the increasing value of TIT, the efficiency of the cycle decreases for the same pressure ratio.
- Increasing the pressure ratio, the difference between the efficiency of the cycle for two different values of ‘TIT’ decreases.

FROM GRAPH 3.2.8

- For each value of TIT, the ratio $W_n / C_p T_1$ of the cycle increases as the pressure ratio increases.
- For the increasing value of TIT, the ratio $W_n / C_p T_1$ of the cycle increases for the same pressure ratio.

- With the increasing value of 'TIT' , for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.2.9

- For the increasing value of TIT, the maximum value of ratio $W_n / C_p T_1$ of the cycle gets at a higher efficiency.
- For each value of TIT , there is a maximum value of efficiency at any value of ratio $W_n / C_p T_1$.
- With the increasing value of TIT , the maximum efficiency decreases for any value of ratio $W_n / C_p T_1$.

FROM GRAPH 3.2.10

- For each value of 'a', the efficiency of the cycle increases.
- For a increasing value of ' a', the efficiency of the cycle decreases upto a certain pressure ratio. After this pressure ratio the higher the value of ' a' , higher the efficiency of the cycle .
- With the increasing value of 'a' , for the maximum value of the efficiency of the cycle, the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.2.11

- For each value of 'a' the ratio $W_n / C_p T_1$ first increases and then decreases.
- For a increasing value of ' a' the ratio $W_n / C_p T_1$ decreases upto a certain pressure ratio. After this pressure ratio the higher the value of ' a' , higher the ratio $W_n / C_p T_1$.
- With the increasing value of 'a' , for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.2.12

- For the increasing value of 'a', the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of 'a', the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of 'a', the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.2.13

- For each value of 'a', the efficiency of the cycle decreases.
- For an increasing value of 'a', the efficiency of the cycle decreases up to a certain pressure ratio. After this pressure ratio the higher the value of 'a', the higher the efficiency of the cycle.
- With the increasing value of 'a', for the maximum value of the efficiency of the cycle, the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.2.14

- For each value of k, the ratio of $W_n / C_p T_1$ first increases then decreases with the pressure ratio.
- For increasing value of k, ratio of $W_n / C_p T_1$ increases for the same pressure ratio.
- For the increasing value of k, the optimum pressure ratio for the maximum value of $W_n / C_p T_1$ shifts toward higher pressure ratio.

FROM GRAPH 3.2.15

- For the increasing value of k, the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.

- For the increasing value of k , the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of k , the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.2.16

- At TIT =1000, the efficiency first decreases with the pressure ratio as increasing the ‘ k ’ but after a certain pressure ratio efficiency of the cycle increases as the ‘ k ’ increases.
- At TIT =1200, the efficiency decreases with the pressure ratio as increasing the ‘ k ’ and the difference between the efficiency at $k=0.0$ & $k=0.006$ decreases as the pressure ratio increases.

FROM GRAPH 3.2.17

- At TIT =1000, the ratio $W_n / C_p T_1$ first decreases with the pressure ratio as increasing the ‘ k ’ but after a certain pressure ratio, the ratio $W_n / C_p T_1$ of the cycle increases as the ‘ k ’ increases.
- At TIT =1200, the ratio $W_n / C_p T_1$ first decreases with the pressure ratio as increasing the ‘ k ’ but after a certain pressure ratio, the ratio $W_n / C_p T_1$ increases as the ‘ k ’ increases. But the pressure ratio after which ratio $W_n / C_p T_1$ increases with the ‘ k ’ increases, shifts toward high-pressure ratio as compare to TIT=1000.

FROM GRAPH 3.2.18

- At TIT =1000, the maximum value of ratio $W_n / C_p T_1$ gets at a higher efficiency for the increasing value of ‘ k ’.

- At TIT =1200, the maximum value of ratio $W_n / C_p T_1$ gets at a higher efficiency for the increasing value of 'k'. But the value of efficiency for maximum value of ratio $W_n / C_p T_1$ shifts toward low value of efficiency as compare to TIT=1000.

Graphs for the one reheat in expansion process

FROM GRAPH 3.3.1

- For each value of k, the efficiency of the cycle increases with increase in pressure ratio of the cycle.
- For the increasing value of k, the efficiency of the cycle decreases for the same value of the pressure ratio.
- For the higher value of the pressure ratio, the difference between the efficiency of the cycle for two different values of k decreases.

FROM GRAPH 3.3.2

- For each value of k, the ratio of $W_n / C_p T_1$ first increases then decreases with the pressure ratio.
- For increasing value of k, ratio of $W_n / C_p T_1$ increases for the same pressure ratio.
- For the increasing value of k, the optimum pressure ratio for the maximum value of $W_n / C_p T_1$ shifts toward higher pressure ratio.

FROM GRAPH 3.3.3

- For the increasing value of k, the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of k, the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.

- For the increasing value of k , the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.3.4

- For each value of 'a', the efficiency of the cycle increases with increase in pressure ratio of the cycle.
- For the increasing value of 'a', the efficiency of the cycle decreases for the same value of the pressure ratio.
- For the higher value of the pressure ratio, the difference between the efficiency of the cycle for two different values of 'a' decreases.

FROM GRAPH 3.3.5

- For each value of 'a', the ratio $W_n / C_p T_1$ first increases and then decreases.
- For an increasing value of 'a', the ratio $W_n / C_p T_1$ decreases upto a certain pressure ratio. After this pressure ratio the higher the value of 'a', higher the ratio $W_n / C_p T_1$.
- With the increasing value of 'a', for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.3.6

- For the increasing value of 'a', the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of 'a', the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of 'a', the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.3.7

- For each value of TIT, the efficiency of the cycle increases as the pressure ratio increases.
- For the increasing value of TIT, the efficiency of the cycle increases for the same pressure ratio.
- Increasing the pressure ratio, the difference between the efficiency of the cycle for two different values of 'TIT' increases.

FROM GRAPH 3.3.8

- For each value of TIT, the ratio $W_n / C_p T_1$ of the cycle increases as the pressure ratio increases.
- For the increasing value of TIT, the ratio $W_n / C_p T_1$ of the cycle increases for the same pressure ratio.
- With the increasing value of 'TIT', for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.3.9

- For the increasing value of TIT, the maximum value of ratio $W_n / C_p T_1$ of the cycle gets at a higher efficiency.
- For each value of TIT, there is a maximum value of efficiency at any value of ratio $W_n / C_p T_1$.
- With the increasing value of TIT, the maximum efficiency increases for any value of ratio $W_n / C_p T_1$.

FROM GRAPH 3.3.10

- For each value of 'a', the efficiency of the cycle increases.
- For a increasing value of 'a', the efficiency of the cycle decreases upto a certain pressure ratio. After this pressure ratio the higher the value of 'a', higher the efficiency of the cycle .
- With the increasing value of 'a', for the maximum value of the efficiency of the cycle, the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.3.11

- For each value of 'a' the ratio $W_n / C_p T_1$ first increases and then decreases.
- For a increasing value of 'a' the ratio $W_n / C_p T_1$ decreases upto a certain pressure ratio. After this pressure ratio the higher the value of 'a', higher the ratio $W_n / C_p T_1$.
- With the increasing value of 'a', for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.3.12

- For the increasing value of 'a', the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of 'a', the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of 'a', the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.3.13

- For each value of 'a', the efficiency of the cycle increases and the difference between efficiency for $k=0.0$ & $k=.006$ decreases.
- For increasing value of 'a', the efficiency of the cycle decreases upto a certain pressure ratio. After this pressure ratio the higher the value of 'a', higher the efficiency of the cycle .
- With the increasing value of 'a', for the maximum value of the efficiency of the cycle, the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.3.14

- For each value of k, the ratio of $W_n / C_p T_1$ first increases with the pressure ratio.
- For increasing value of k, ratio of $W_n / C_p T_1$ increases for the same pressure ratio.
- For the increasing value of k, the optimum pressure ratio for the maximum value of $W_n / C_p T_1$ shifts toward higher pressure ratio.

FROM GRAPH 3.3.15

- For the increasing value of k, the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of k, the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of k, the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.1.16

- At TIT =1000, the efficiency decreases with the pressure ratio as increasing the 'k' and the difference between efficiency decreases for $k=0.0$ & $k=0.006$ with increasing pressure ratio.
- At TIT =1200, the efficiency first decreases with the pressure ratio as increasing the 'k' and the difference between the efficiency at $k=0.0$ & $k=0.006$ decreases as the pressure ratio increases.

FROM GRAPH 3.3.17

- At TIT =1000, the ratio $W_n / C_p T_1$ first decreases with the pressure ratio as increasing the 'k' but after a certain pressure ratio, the ratio $W_n / C_p T_1$ of the cycle increases as the 'k' increases.
- At TIT =1200, the ratio $W_n / C_p T_1$ first decreases with the pressure ratio as increasing the 'k' but after a certain pressure ratio, the ratio $W_n / C_p T_1$ increases as the 'k' increases. But the pressure ratio after which ratio $W_n / C_p T_1$ increases with the 'k' increases, shifts toward high-pressure ratio as compare to TIT=1000.

FROM GRAPH 3.3.18

- At TIT =1000, the maximum value of ratio $W_n / C_p T_1$ gets at a higher efficiency for the increasing value of 'k'.
- At TIT =1200, the maximum value of ratio $W_n / C_p T_1$ gets at a higher efficiency for the increasing value of 'k'. But the value of efficiency for maximum value of ratio $W_n / C_p T_1$ shifts toward high value of efficiency as compare to TIT=1000.

Graphs for one inter cooler used in compression process and one reheat in expansion

FROM GRAPH 3.4.1

- For each value of k , the efficiency of the cycle increases with increase in pressure ratio of the cycle.
- For the increasing value of k , the efficiency of the cycle decreases for the same value of the pressure ratio.
- For the higher value of the pressure ratio, the difference between the efficiency of the cycle for two different values of k decreases.

FROM GRAPH 3.4.2

- For each value of k , the ratio of $W_n / C_p T_1$ first increases then decreases with the pressure ratio.
- For increasing value of k , ratio of $W_n / C_p T_1$ increases for the same pressure ratio.
- For the increasing value of k , the optimum pressure ratio for the maximum value of $W_n / C_p T_1$ shifts toward higher pressure ratio.

FROM GRAPH 3.4.3

- For the increasing value of k , the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of k , the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of k , the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.4.4

- For each value of 'a', the efficiency of the cycle increases with increase in pressure ratio of the cycle.
- For the increasing value of 'a', the efficiency of the cycle decreases for the same value of the pressure ratio.
- For the higher value of the pressure ratio, the difference between the efficiency of the cycle for two different values of 'a' decreases.

FROM GRAPH 3.4.5

- For each value of 'a', the ratio $W_n / C_p T_1$ first increases and then decreases and the difference between the value of $W_n / C_p T_1$ decreases with pressure ratio increases.
- For an increasing value of 'a', the ratio $W_n / C_p T_1$ decreases.

FROM GRAPH 3.4.6

- For the increasing value of 'a', the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of 'a', the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of 'a', the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.4.7

- For each value of TIT, the efficiency of the cycle increases as the pressure ratio increases.
- For the increasing value of TIT, the efficiency of the cycle increases for the same pressure ratio.

- Increasing the pressure ratio, the difference between the efficiency of the cycle for two different values of 'TIT' increases.

FROM GRAPH 3.4.8

- For each value of TIT, the ratio $W_n / C_p T_1$ of the cycle increases as the pressure ratio increases.
- For the increasing value of TIT, the ratio $W_n / C_p T_1$ of the cycle increases for the same pressure ratio.
- With the increasing value of 'TIT', for the maximum value of the ratio $W_n / C_p T_1$ the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.4.9

- For the increasing value of TIT, the maximum value of ratio $W_n / C_p T_1$ of the cycle gets at a higher efficiency.
- For each value of TIT, there is a maximum value of efficiency at any value of ratio $W_n / C_p T_1$.
- With the increasing value of TIT, the maximum efficiency increases for any value of ratio $W_n / C_p T_1$.

FROM GRAPH 3.4.10

- For each value of 'a', the efficiency of the cycle increases.
- For a increasing value of 'a', the efficiency of the cycle decreases and the difference between efficiency decreases with increasing pressure ratio.
- With the increasing value of 'a', for the maximum value of the efficiency of the cycle, the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.4.11

- For each value of 'a' the ratio $W_n / C_p T_1$ first increases and then decreases.

- For an increasing value of 'a' the ratio $W_n / C_p T_1$ decreases and the difference between the value of ratio $W_n / C_p T_1$ decreases with increasing pressure ratio.

FROM GRAPH 3.4.12

- For the increasing value of 'a', the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.
- For the increasing value of 'a', the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.

FROM GRAPH 3.4.13

- For each value of 'a', the efficiency of the cycle increases and the difference between efficiency for $k=0.0$ & $k=.006$ decreases.
- For an increasing value of 'a', the efficiency of the cycle decreases up to a certain pressure ratio. After this pressure ratio the higher the value of 'a', the higher the efficiency of the cycle.
- With the increasing value of 'a', for the maximum value of the efficiency of the cycle, the optimum value of pressure ratio shifts toward high pressure ratio.

FROM GRAPH 3.4.14

- For each value of k, the ratio of $W_n / C_p T_1$ increases with the pressure ratio.
- For increasing value of k, ratio of $W_n / C_p T_1$ increases for the same pressure ratio.
- For the increasing value of k, the optimum pressure ratio for the maximum value of $W_n / C_p T_1$ shifts toward higher pressure ratio.

FROM GRAPH 3.4.15

- For the increasing value of k, the value of the ratio $W_n / C_p T_1$ increases at the same efficiency.

- For the increasing value of k , the maximum value of the efficiency for any value of the ratio $W_n / C_p T_1$ decreases.
- For the increasing value of k , the maximum value of the ratio $W_n / C_p T_1$ shifts toward low efficiency.

FROM GRAPH 3.4.16

- At TIT =1000, the efficiency decreases with the pressure ratio as increasing the ' k ' and the difference between efficiency decreases for $k=0.0$ & $k=0.006$ with increasing pressure ratio.
- At TIT =1200, the efficiency first decreases with the pressure ratio as increasing the ' k ' and the difference between the efficiency at $k=0.0$ & $k=0.006$ decreases as the pressure ratio increases.

FROM GRAPH 3.4.17

- At TIT =1000, the ratio $W_n / C_p T_1$ first decreases with the pressure ratio as increasing the ' k ' but after a certain pressure ratio, the ratio $W_n / C_p T_1$ of the cycle increases as the ' k ' increases.
- At TIT =1200, the ratio $W_n / C_p T_1$ first decreases with the pressure ratio as increasing the ' k ' but after a certain pressure ratio, the ratio $W_n / C_p T_1$ increases as the ' k ' increases. But the pressure ratio after which ratio $W_n / C_p T_1$ increases with the ' k ' increases, shifts toward high-pressure ratio as compare to TIT=1000.

FROM GRAPH 3.4.18

- At TIT =1000, the maximum value of ratio $W_n / C_p T_1$ gets at a higher efficiency for the increasing value of ' k '.

- At $TIT = 1200$, the maximum value of ratio $W_n / Cp T_1$ gets at a higher efficiency for the increasing value of 'k'. But the value of efficiency for maximum value of ratio $W_n / Cp T_1$ shifts toward high value of efficiency as compare to $TIT = 1000$.

CHAPTER 4

CONCLUSION

The effect of variable specific heat is discussed. The specific heat of air varies considerably with temperature. At 300 K the constant pressure specific heat of air is 1.005 kJ /kg K but at 1000K, it is 1.140 kJ/kg K.

In ideal cycle calculations the specific heat has been taken to be constant throughout the cycle, with a value of 1.005 kJ /kg K. Thus, this assumption would seem to introduce considerable error.

The cycle model, assuming temperature-dependent specific heats of the working fluid has been investigated numerically. In this study temperature dependent specific heat ratio functions were derived. The performance characteristics of the cycle were obtained by numerical examples using these derived relations. Along with the analysis of simple gas turbine , gas turbine with one intercooler alone, one reheat alone , and with one intercooler and one reheat cycles have been analyzed. During this analysis it is revealed that simple gas turbine performance most affected by the consideration of variable specific heat. The results show that there are significant effects of the temperature dependence of the specific-heats heat of the working fluid on the performance of the cycles, and this should be considered in practical-cycle analysis. The results obtained from this research are compatible with those in the open literature, but for other cycles, and may be used with assurance to provide guidance for the analysis of the behavior and design of practical engines. It would be more meaningful if one considers experimental results. This will be a next work in the near future.

Future studies should discuss the possible effects of fuel additives in order to achieve a less temperature-dependent specific heat of the working fluid.

ANNEXURE

// programme for analysis of gas turbine with and without intercooler and reheat to find out compressor work input, turbine work output , net work output, specific work ratio and efficiency of the cycle at various pressure ratio for variable specific heat.

```
#include <conio.h>
#include <stdio.h>
#include <iostream.h>
#include <math.h>
#include <ctype.h>
#include <graphics.h>

main()
{
clrscr();
char ch='Y';
char outline[500];
double T1,P1,N1,Ma,m,a,k1, bv, ecc,Q1,ec,Rc,P2,G,Tcooler,work_total,
        tc_actual, Wci, tc_ideal, Wn,Q,T3,Ws,S,T,cv;
int i,choice;
double T0, z, h1, h2,x, y ,x1,y1 ,h11,k2;
FILE *fp;
fp=fopen("C:\\project.xls","w");
fprintf(fp,"\n\n\t\tTIT\t\t\tk1\t\t\tbv\t\t\ttrp\t\t\tWc\t\t\tWt\t\t\teth\t\t\tWs\t\t\tWn\n\n");

cout << "Please Enter T1 P1 N1 Ma a and b";
cout << "\nPlease Enter ambient temperatureT1\n";
    cin >> T1;
cout << "\nPlease Enter ambient presure P1\n ";
    cin >> P1;
cout << "\nPlease Enter the no of intercoolers N1\n ";
    cin >> N1;
cout << "\nPlease Enter the mass of the air Ma\n ";
    cin >> Ma;
    m=Ma;
cout << "\nPlease Enter the coefficent a of the 'cp= a + k1 T\n";
    cin >> a;
cout << "\nPlease Enter The coefficent k1 of the 'cp= a + k1 T\n";
    cin >> k1;
```

```

cout << "\nPlease Enter coefficent bv of the 'cv= bv + k1 T'\n";
    cin >> bv;

    bv=a-8.314;
    k2=k1/2;
for(i=0;i<(N1+1);i++)
{
    cout<<"\nEnter choice\n";
    cin >> choice;

        if(choice==1)
            {
                cout << "\nEnter pressure after compression of P2\n";
                cin >> P2;
                Rc = P2 / P1;
                P1 =P2;
            }
        if(choice==2)
            {
                cout << "\nEnter Pr Ratio Rc \n";
                cin >> Rc;
            }
    cout << " \nEnter efficiency of the compressor(ec)\n";
        cin >> ec;
    if (i > 0)
        {
        cout << " \nEnter temperature after the cooling (Tcooler)\n";
            cin >> Tcooler;
        T1 = Tcooler;
        }
    double p, q, r, s, t;
    p=a-bv;
    q=p*log(Rc);
    r=q+k1*T1+a*log(T1);
    x=r/a;
    y=k1/a;
    cout<< " \nEnter initial guess of the temperature of air T2(non zero)\n";
        cin >> T0;
        z=.0001;
        h1=log(T0) - x +y*T0;
        do
            {
                h1=log(T0) - x +y*T0;
                h2= 1/T0 + y;
                T0=T0-h1/h2;
                h1=log(T0) - x +y*T0;
            }

```

```

        h1=h1*h1;
        h1=sqrt (h1);
    }while(h1>z);
    tc_ideal= T0;

double x22,x11,c,D;
    c = (tc_ideal - T1) * ( a + k2 * ( tc_ideal + T1));
    c /=  ec;
    c += a * T1 + k2 * T1 * T1 ;
    c = - c;

    D = sqrt(a*a - 4*k2*c);
    x11= (-a + D) / (2 *k2);
    x22= (-a - D) / (2 *k2);

    tc_actual=x11;

    Wci = Ma * ( a * tc_actual + k2 * tc_actual * tc_actual- a * T1 - k2 * T1 * T1);
    work_total = work_total + Wci;

    cout << "\nWc"<<i<<" = " <<Wci<<"\n\n";
}
    cout << "\nWork Total= " << work_total<<"\n\n";
    cout << "\nT2 = " << tc_actual<<"\n\n";

//*****
// Turbine Calculation

double T3,Rt,et,T2 = tc_actual,tt_ideal=0,tt_actual=0;
int N2;
cout << "\nEnter No. of Reheat Cycles N2 \n" ;
    cin >> N2;

double work_ttotal=0,Wti;
for( i=0; i < (N2+1);i++)

{
    cout << "\nEnter expansion ratio in the turbine(Rt)\n";
        cin >> Rt;
    cout << "\nEnter the efficiency of the turbine(et)\n";
        cin >> et;

if (i > 0)
    {
        T2=tt_actual;
    }
}

```

```

double T00,x1,y1;
double p1, q1, r1, s1, t1;
    p1=a-bv;
    q1=-p1*log(Rt);
    r1=q1+k1*T3+a*log(T3);
    x1=r1/a;
    y1=k1/a;

cout<< " \nEnter initial guess of the temperature of Te(non zero)\n";
    cin >> T00;
    z=.0001;
    h1=log(T00) - x1 + y1 *T00;
    h1=h1*h1;
    h1=sqrt (h1);
    do
    {
        h1=log(T00) - x1 + y1 *T00;
        h2= 1/T00 + y1;
        T00=T00-h1/h2;
        h1=log(T00) - x1 + y1 *T00;
        h1=h1*h1;
        h1=sqrt (h1);
    }
    while(h1>z);
    tt_ideal = T00;

double c1,x111,x222,D;

    c1 = (T3-tt_ideal) * ( a + k2 * ( T3 + tt_ideal));
    c1 *= et;
    c1 -= a * T3 + k2 * T3 * T3 ;

    D = sqrt(a*a - 4*k2*c1);
    x111= (-a + D) / (2 *k2);
    x222= (-a - D) / (2 *k2);

    tt_actual =x111;
    cout<<"\nT4= "<<tt_actual<<"\n\n";

    Wti = Ma * ( a * T3 + k2 * T3 * T3 - a * tt_actual - k2 *tt_actual * tt_actual);
    work_ttotal = work_ttotal + Wti;
    cout << "\nWt"<<i<< " = " <<Wti<<"\n\n";

    Q= (1/ecc)*(Ma*(a*T3+k2*T3*T3)-m*(a* T2+k2*T2*T2));
    Q1=Q1+Q;

```

```

        cout<<"Q"<<Q1;
        cout << "Wti"<< Wti;
    }
    cout << "\nWork Total= " << work_tttotal<<"\n\n";
    cout << "\nT4 = " << tt_actual;
double eth;
    cout<<"\nEnter the combustion efficiency(ecc)\n ";
        cin>>ecc;

        eth=(work_tttotal-work_total)/Q1;
        Wn=(work_tttotal-work_total);
        cout<<"Wn"<<Wn<<"\n";
        Ws=Wn/(a*T1+k1*T1*T1);

        fprintf(fp,"\\t\\t%f\\t%f\\t%f\\t%f\\t%f\\t%f\\t%f\\t%f\\t%f\\n",T3,a,k1,bv,Rc,work_to
tal,work_tttotal,eth,Ws,Wn);

        cout<<"\nthermal efficiency= " <<eth<<"\n\n";

fclose(fp);

fp=fopen("c:\\project.xls","r");
fscanf(fp,"\\n\\n\\t\\t %[ 1A-Za-z\\t]s\\n",outline);
cout<<outline<<"\n";
while (!feof(fp))
{
    if (!feof(fp))
    {
        fscanf(fp,"%f%f%f%f%f%f%f%f
%f\\n",&T3,&a,&k1,&bv,&Rc,&work_total,&work_tttotal,&eth,&Ws,&Wn);
        printf("%4.0f %5.3f %4.3f %6.3f %2.0f %5.2f %5.2f %6.5f %6.4f
%6.4f\\n",T3,a,k1,bv,Rc,work_total,work_tttotal,eth,Ws,Wn);
    }
}

    getch();
    return 0;
}

```

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